

MANUAL OF PETROLEUM MEASUREMENT STANDARDS

CHAPTER 12 - CALCULATION OF PETROLEUM QUANTITIES

Section 4 - Determination of Base Prover Volume

Part 2 - Master Meter Method

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Chapter 12 - Calculation of Petroleum Quantities

Section 4 - Base Prover Volume Determination

Part 2 - Master Meter Volumetric Method

1. Scope

This document provides standardized calculation methods for the quantification of liquids and the determination of base prover volumes (BPVs) under defined conditions by '**master meter volumetric method**', regardless of the point of origin or destination or units of measure required by governmental organizations. The criteria contained in this document allow different individuals, using various computer languages on different computer hardware (or manual calculations), to arrive at identical results using the same standardized input data.

This publication rigorously specifies the equations for computing correction factors, rules for rounding, the sequence of the calculations, and the discrimination levels of all numbers to be used in these calculations. No deviations from these specifications are permitted since the intent of this document is to serve as a rigorous standard.

1.1 Application

1.1.1. General

The BPV of a prover (displacement or open tank) may be determined by one of three methods: waterdraw, master meter, or gravimetric.

This document specifies the equations, rules for rounding, sequence of the calculations, and discrimination levels for the '**master meter volumetric method**'.

The operational procedures and acceptance criteria employed to calibrate a displacement prover by the master meter volumetric method are specified in API *MPMS* Chapter 4.9.3. The master prover may be a displacement prover or open tank prover.

1.1.2. Applicable Fluids

For displacement provers (free or captive displacer design), the application of this standard shall be limited to hydrocarbon liquids which are assumed to be clean, air/gas free, low vapor pressure, homogeneous, single-phase, and Newtonian at operating conditions.

To properly implement the procedures to correct measured quantities at flowing temperatures and pressures to corresponding quantities at base (reference or standard) conditions, the liquid density correlations specified in API *MPMS* Chapter 11.1 shall be utilized to perform the complex calculations.

For open tank provers as a master prover, the application of this standard shall be limited to potable water, which is assumed to be clean, air/gas free, low vapor pressure, homogeneous, single-phase, and Newtonian at operating conditions.

1.1.3. Base Conditions

Historically, the measurement of hydrocarbon liquids for custody transfer and process control have been stated in volume units at base (reference or standard) conditions.

The base conditions for the measurement of liquids, such as crude petroleum and its liquid products, having a vapor pressure equal to or less than atmospheric pressure at the base temperature are as follows.

- International System (SI) of Units.
 - Pressure: 101.325 kPa (14.696 psia).
 - Temperature: 15.00 °C (59.0 °F).
- U.S. Customary (USC) units.
 - Pressure: 14.696 psia (101.325 kPa).
 - Temperature: 60.0 °F (15.556 °C).

Base conditions may change based on contractual, regulatory, or national requirements. Therefore, it is necessary that the base conditions be identified and specified in all standardized volumetric flow measurements by all the parties involved in the measurement.

2. Normative References

The following referenced documents are indispensable for the application of this document. For dated references, only the edition cited applies. For undated references, the latest edition of the following referenced documents (including any addenda) applies.

API Manual of Petroleum Measurement Standards (MPMS) Chapter 4.8, Operation of Proving Systems

API Manual of Petroleum Measurement Standards (MPMS) Chapter 4.9.1, Introduction to the Determination of the Volume of Displacement and Tank Provers

API Manual of Petroleum Measurement Standards (MPMS) Chapter 4.9.2, Determination of the Volume of Displacement and Tank Provers by the Waterdraw Method of Calibration

API Manual of Petroleum Measurement Standards (MPMS) Chapter 4.9.3, Determination of the Volume of Displacement Provers by the Master Meter Method of Calibration

API Manual of Petroleum Measurement Standards (MPMS) Chapter 11.1, Temperature and Pressure Volume Correction Factors for Generalized Crude Oils, Refined Products, and Lubricating Oils

API Manual of Petroleum Measurement Standards (MPMS) Chapter 11.4.1, Density of Water and Water Volumetric correction Factors for Water Calibration of Volumetric Provers

API Manual of Petroleum Measurement Standards (MPMS) Chapter 12.4.1, Calculation of Petroleum Quantities Determination of Base Prover Volume Using Waterdraw Volumetric Method

3. Terms, Definitions, Acronyms, Abbreviations, and Symbols

3.1 Terms and Definitions

For the purposes of this document, the following terms and definitions apply. Terms of more general use may be found in API *MPMS* Chapter 1, *Online Terms and Definitions Database*.

3.1.1

base conditions

Reference pressure and temperature conditions, as defined by standards, regulations, or contracts, used in custody transfer measurement calculations of fluid volumes and other calculations.

3.1.2

base prover volume

BPV

The volume of the prover at base conditions as shown on the calibration certificate.

3.1.3

calibrated prover volume

CPV

The volume of the prover at base conditions is determined from a prover calibration run (or roundtrip).

3.1.4

calibration certificate

A report documenting the calibration of a measurement device such as a flowmeter prover, a thermometer, or pressure gauge and its traceability to a national metrological institute [e.g., National Institute of Standards and Technology (NIST)].

3.1.5

calibration set (or set)

A calibration set consists of three (3) to six (6) consecutive CPV determinations at a defined stable flowrate.

3.1.6

correction for temperature on liquid

CTL

Compensates for the effect of temperature on a liquid.

3.1.7

correction for pressure on liquid

CPL

Compensates for the effect of pressure on a liquid.

3.1.8

correction for temperature and pressure on liquid

CTPL

Compensates for the combined effect of temperature and pressure on a liquid.

3.1.9

correction for pressure on steel

CPS

Correction for changes in volume of a steel container - prover, tank, tank car, or other vessel - due to changes in the internal pressure between its reference pressure and its operating pressure.

3.1.10

correction for temperature on steel

CTS

Correction for changes in length, area, or volume of a steel container - prover, tank, tank car, or other vessel - due to changes in the steel temperature between its reference temperature and its operating temperature.

3.1.11

densitometer meter factor

DMF

A dimensionless term equal to the ratio of the density as determined by a reference device to the corresponding density of the density meter.

NOTE The densitometer's reading (ρ_{ind}) is multiplied by a DMF to obtain the observed density (ρ_{obs}) at the temperature (T_{dm}) and pressure (P_{dm}) conditions of the densitometer.

3.1.12

displacement prover

Displacement provers operate on the principle of the repeatable displacement of a known volume of liquid from a calibrated section of pipe between two detectors. Displacement of the volume of liquid is achieved by a sphere or a piston traveling through the pipe. A corresponding volume of liquid is simultaneously measured by a flowmeter installed in series with the displacement prover.

3.1.13

displacement prover – free displacer design

A displacement prover that employs a free displacer design, employs a sphere or piston that moves freely with the flow when the displacer is launched. This design employs integrally installed displacer detectors.

3.1.14

displacement prover – captive displacer design

A displacement prover that employs a captive displacer design, employs a piston that is attached to a rod that moves freely with the flow when the displacer is launched. This design employs externally installed displacer detectors mounted on a rod that is in the atmosphere.

3.1.15

flowrate

Q

The rate of flow as measured by a flowmeter.

3.1.16

gauge pressure

Pressure measured relative to atmospheric pressure with one atmosphere taken as zero.

3.1.17

low vapor pressure liquid

A liquid with a vapor pressure less than or equal to atmospheric pressure at operating conditions ($P_E \leq 0.0$ kPag or 0.0 psig).

3.1.18

NIST traceability

A property of a measurement result whereby the result can be traced back to the National Institute of Standards and Technology (NIST) by an unbroken chain of calibrations.

3.1.19

open tank prover

An open tank prover is an atmospheric volumetric vessel that has a reduced cross section or neck located at both the top and bottom or, in some cases, at the top only. The necks are equipped with gauge glasses and graduated scales.

3.1.20

pass

A single movement of the displacer in a displacement prover that activates the start-stop detectors.

3.1.21

primary standard

A measurement standard whose value is determined by NIST or appropriate national metrological institute.

3.1.22

prover calibration certificate

A document package stating the BPV, which includes the physical and run data used to calculate the BPV, and the traceability documentation.

3.1.23

prover with external detectors

Captive displacer prover designs employ a piston attached to a shaft. The displacement of the shaft is constant except that it moves into and out of the calibrated section during a calibration run. Usually, there is one or two externally mounted detectors and/or guide rods attached to the captive piston displacer. Since provers have externally mounted detectors, the thermal effect on the steel may not be the same for the area aspect as for the linear aspect. In a prover calibration, as well as a flowmeter calibration, it is necessary to obtain both a prover barrel temperature and a detector shaft temperature.

3.1.24

prover with integral detectors

Free displacer prover designs, both unidirectional and bidirectional applications, employ a sphere or piston displacer in a circular conduit or pipe. The detectors are integral to the pipe. In other words, the detectors are mounted directly to the pipe through which the free displacer passes.

3.1.25

reference conditions

The base conditions of temperature and pressure (e.g., 60.0 °F and 0 psig, 60.0 °F and equilibrium vapor pressure, 15.00 °C and 101.325 kPa, or 15.00 °C and equilibrium vapor pressure) to which measured volumes are to be corrected.

3.1.26 reference pressure

P_B

The base conditions of pressure (e.g., 0 psig, 14.696 psia, 101.325 kPa, and equilibrium vapor pressure) to which measured volumes are to be corrected.

3.1.27 reference temperature

T_B

The base conditions of temperature (e.g., 60.0 °F, 15.00 °C, 20.00 °C) to which measured volumes are to be corrected.

3.1.28 run

For a bidirectional displacement prover, the combination of a single pass of the displacer in one direction (e.g., forward) followed by a single pass of the displacer in the opposite direction (e.g., back).

For a unidirectional prover, one pass of the displacer between detectors.

For an open tank prover, one filling (or emptying) between the upper neck scale level reading and the lower neck scale level reading or zero reference on an open tank prover.

3.1.29 trips per run

The number of runs of a displacer in a pipe prover for calculating a single calibration run.

3.2 Acronyms, Abbreviations, and Symbols

3.2.1 General

Symbols have been defined to aid in clarity of the mathematical treatments. Notations at the end of a symbol such as “P” refers to a prover, “M” refers to a flowmeter, “MM” refers to a master meter, “MP” refers to a master prover, “FP” refers to a field prover (prover to be calibrated), “dm” refers to a densitometer, and “B” refers to base conditions.

3.2.2 Units

SI International System of Units (kPa, cubic meter, kilogram, °C)

USC U.S. customary units (psi, cubic inch, gallon, barrel, pound, °F)

3.2.3 Steel Pipe Dimensions and Properties

ID_P inside diameter of displacement prover

WT_P wall thickness of displacement prover

E modulus of elasticity of steel

GL linear coefficient of thermal expansion of steel

| | |
|--------|---|
| E_P | modulus of elasticity of prover wall material |
| GL_D | GL for detector mounting shaft (external detectors) |
| GL_P | GL for prover wall material |

3.2.4 Flowmeter Terms, Flowrate, Pulses, Repeatability, and Reproducibility

| | |
|---------------------------|--|
| T_{F_Comp} | Temperature Compensated Flowmeter |
| T_{P_Comp} | Pressure Compensated (CMF) Flowmeter |
| NKF | Nominal K-Factor (pulses per Bbl, pulses per M^3) |
| Q | flowrate (prover report, prover calibration) |
| Q_{MM_SET} | average flowrate for the Selected Runs (CPV_{RUN}) in a Set (prover calibration) |
| NKF | Nominal K-Factor (e.g., pulses per M^3 , pulses per Bbl) of the flowmeter |
| IMF | Intermediate Meter Factor (proving report) |
| MMF | Master Meter Factor (prover report, prover calibration) |
| MMF_{SET} | Master Meter Factor for a Set (prover calibration) |
| ΔMMF | Master Meter Factor Deviation (prover report, prover calibration) |
| N | whole pulses |
| N_{AVG} | the average of the whole pulses for the selected runs |
| N_i | interpolated pulses |
| N_{I_AVG} | the average of the interpolated pulses for the selected runs |
| r | repeatability (or range) of flowmeter in % of the Selected Runs (proving report) |
| $(r)_{CPV_{RUN} Set}$ | repeatability (or range) in % of three (3) Consecutive CPV_{RUN} values in a Calibration Set |
| $R_{CPV_{SET} flowrates}$ | reproducibility (or range) in % of three (3) Consecutive CPV_{SET} values over three (3) flowrates |

3.2.5 Temperature

| | |
|-------------|------------------------------|
| $^{\circ}C$ | Celsius temperature scale |
| $^{\circ}F$ | Fahrenheit temperature scale |

| | |
|-----------------------|--|
| T | temperature (°C or °F) |
| T _B | base temperature (15.00 °C, 20.00 °C, or 60.0 °F) |
| T _{obs} | observed temperature of atmospheric hydrometer (proving report, prover calibration) |
| T _{dm} | temperature in densitometer (proving report, prover calibration) |
| T _D | temperature of detector shaft in prover (proving report, prover calibration) |
| T _M | temperature in meter (proving report, prover calibration) |
| T _{P_INLET} | inlet temperature in prover (proving report, prover calibration) |
| T _{P_OUTLET} | outlet temperature prover (proving report, prover calibration) |
| T _{P_RUN} | average of the inlet and outlet temperature in prover (proving report, prover calibration) |
| T _{P_SET} | average temperature in field prover for a Set (prover calibration) |

3.2.6 Pressure

| | |
|------------------------------------|---|
| kPag | kilopascals in gauge pressure units |
| psig | pounds per square inch in gauge pressure units |
| P | pressure |
| P _B | base pressure in gauge pressure units |
| P _E | equilibrium vapor pressure of liquid (set at 0.0 psig, 0.0 kPag) |
| P _{obs} | observed pressure of atmospheric hydrometer (proving report, prover calibration) |
| P _{dm} | pressure in densitometer (proving report, prover calibration) |
| P _M | pressure in flowmeter (proving report, prover calibration) |
| P _{P_INLET} | inlet pressure in prover (proving report, prover calibration) |
| P _{P_OUTLET} | outlet pressure in prover (proving report, prover calibration) |
| P _{P_RUN} calibration) | average of the inlet and outlet pressure in prover for a Run (proving report, prover calibration) |
| P _{P_SET} | average pressure in field prover for a Set (prover calibration) |

3.2.7 Fluid Properties

| | |
|-----|----------------|
| API | density (°API) |
|-----|----------------|

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| | |
|-------------------|--|
| API_{ind} | indicated density of atmospheric hydrometer or thermohydrometer ($^{\circ}API$) |
| API_{obs} | observed density of atmospheric hydrometer or thermohydrometer ($^{\circ}API$) |
| API_B | base density ($^{\circ}API$) |
| API_{B_RUN} | average density at base conditions for a Run (prover calibration, $^{\circ}API$) |
| API_{B_SET} | average density at base conditions for a Set (prover calibration, $^{\circ}API$) |
| ρ | mass density (kg/m^3) |
| ρ_B | base mass density (kg/m^3) |
| ρ_{ind} | indicated mass density (kg/m^3) |
| ρ_{obs} | observed mass density (proving report, prover calibration, kg/m^3) |
| ρ_{B_RUN} | base mass density for a Run (proving report, prover calibration, kg/m^3) |
| ρ_{B_START} | opening base mass density for a Set from the Proving Report (Spot Sampling, kg/m^3) |
| ρ_{B_STOP} | closing base mass density for a Set from the Proving Report (Spot Sampling, kg/m^3) |
| ρ_{B_SET} | average base mass density for selected Runs in a Set (Spot Sampling, kg/m^3) |

3.2.8 Correction Factors

| | |
|-----------------------|--|
| CTS | Correction for Temperature on Steel Container |
| CPS | Correction for Pressure on Steel Container |
| CTL | Correction for Temperature on Liquid |
| CPL | Correction for Pressure (compressibility) on Liquid |
| CTPL | Correction for Temperature and Pressure on Liquid |
| CTSp | Correction for Temperature on Steel Prover (proving report, prover calibration) |
| CPSp | Correction for Pressure on Steel Prover (proving report, prover calibration) |
| CTLp | Correction for Temperature on Liquid in Prover (proving report, prover calibration) |
| CPLp | Correction for Pressure on Liquid in Prover (proving report, prover calibration) |
| CTPLp calibration) | Correction for Temperature and Pressure on Liquid in Prover ((proving report, prover |

| | |
|-------------|---|
| CTL_M | Correction for Temperature on Liquid in Flowmeter (proving report, prover calibration) |
| CPL_M | Correction for Pressure on Liquid in Flowmeter (proving report, prover calibration) |
| $CTPL_M$ | Correction for Temperature and Pressure on Liquid in Flowmeter (proving report, prover calibration) |
| $CTSp_{15}$ | Correction for Temperature on Steel Prover to convert BPV_{usc_60} to BPV_{si_15} |
| $CTSp_{20}$ | Correction for Temperature on Steel Prover to convert BPV_{usc_60} to BPV_{si_20} |
| $CTSp_{60}$ | Correction for Temperature on Steel Prover to convert BPV_{si_15} to BPV_{usc_60} |
| DMF | Densitometer Meter Factor (proving report, prover calibration) |
| F | Compressibility Factor of fluid (proving report, prover calibration) |
| HYC | Hydrometer Correction Factor |
| IMF | Intermediate Meter Factor (proving report) |
| MMF | Master Meter Factor (proving report, prover calibration) |

3.2.9 Calibration Set - Acceptance Criteria

| | |
|-------------------------|--|
| r | repeatability (or range) in % - pulse train, or IMF (proving report) |
| $\Delta ICPV_{RUN}$ | ICPV variation over Selected 3 Consecutive Runs in a Set |
| $r_{\Delta ICPV_{RUN}}$ | ICPV variation (or repeatability) in % for Selected 3 Consecutive Runs in a Set |
| ΔMMF_{SET} | ΔMMF_{SET} in % for Selected 3 Consecutive Runs in a Set |
| $(R) CPV_{RUN}$ | ΔCPV variation (or reproducibility) in % over Selected 3 Consecutive Runs in a Set |
| $(r) CPV_{RUN}$ | CPV variation (or repeatability) in % for Selected 3 Consecutive Runs in a Set |

3.2.10 Prover Calibration - Set Stability Parameters

| | |
|------------------------|--|
| ΔMMF_{SET} | ΔMMF_{SET} in % in a Calibration Set |
| $\Delta \rho_{B_SET}$ | base density variation (or range) in a Calibration Set |
| ΔT_{FP_SET} | temperature variation (or range) in a Calibration Set |
| ΔP_{FP_SET} | pressure variation (or range) in a Calibration Set |
| ΔQ_{MM_SET} | flowrate variation (or range) in a Calibration Set |

3.2.11 Prover Calibration - Acceptance Criteria

| | |
|-------------------------------------|--|
| $\Delta\text{CPV}_{\text{SET}}$ | ΔCPV variation over three (3) Selected Consecutive Runs in a Calibration Set |
| $R_{\Delta\text{CPV}_{\text{SET}}}$ | CPV reproducibility in % for three (3) Consecutive Calibration Sets (All Methods) |
| ΔQ_{set} | flowrate variation (or range) in % between Consecutive Calibration Sets (All Methods) |

3.2.12 Volumes

| | |
|-------------------------------|---|
| BPV | Base Prover Volume |
| BPV_{USC} | Base Prover Volume at 60 °F and 0.0 psig (cubic inches, Bbl, gal, cubic feet) |
| BPV_{15} | Base Prover Volume at 15 °C and 0.0 kPag (mL, M ³ , L) |
| BPV_{20} | Base Prover Volume at 20 °C and 0.0 kPag (mL, M ³ , L) |
| BPV_{OLD} | Previous (old or targeted) Base Prover Volume |
| BPV_{NEW} | New Base Prover Volume |
| CPV | Calibrated Prover Volume at base conditions (prover calibration) |
| CPV_{RUN} | CPV for a Run (prover calibration) |
| CPV_{SET} | CPV for three (3) Consecutive Runs in a Set at a constant flowrate (prover calibration) |
| Avg CPV_{SET} | Average of three (3) Consecutive Sets at three different flowrates (prover calibration) |
| GSV_{P} | Gross Standard Volume of Prover (proving report) |
| IV_{M} | Indicated Volume of Flowmeter (proving report, prover calibration) |
| ISV_{M} | Indicated Standard Volume of Flowmeter (proving report) |
| GSV_{M} | Gross Standard Volume of Meter (proving report, prover calibration) |
| ICPV_{RUN} | Initial CPV for a Run (prover calibration) |

4. Precision and Rounding

The minimum precision of the computing hardware shall be 32bit IEEE floating point precision to obtain the same answer in all calculations.

When a number is to be rounded to a specific number of decimals, it shall always be rounded off in one step to the number of figures that are to be recorded and shall not be rounded in two or more steps of successive rounding. The rounding procedure shall be in accordance with the following.

When the figure to the right of last place to be retained is five (5) or greater, the figure in the last place to be retained should be increased by one (1).

If the figure to the right of the last place to be retained is less than five (5), the figure in the last place retained should be unchanged.

5. Discrimination and Reporting Levels

Discrimination and reporting levels ***different than those specified are not permitted.***

The discrimination and reporting levels are stated in tabular format below for clarity (Tables 1 through 9).

In these tables, the number of digits shown as (X) in front of the decimal point are for illustrative purposes only and may have several digits more or less than the number of (Xs) illustrated. The number of digits shown as (x) after the decimal point are very specific, as they define the required discrimination level for each value described.

The objective of this standard is to record the readings, then perform the calculations.

The discrimination levels specified in this section, in many circumstances are greater than the uncertainty of the field measurements.

The discrimination levels outlined in this section do not imply measurement accuracy of a device or field measurement.

For example, it is not reasonable for a dynamic temperature measurement to be accurate to less than ± 0.1 °F (± 0.05 °C) in a field or laboratory environments. This limitation is due to thermowell heat transfer, transfer medium, temperature lagging, temperature device limitations (design, sensor type, certification limitations), ambient effects, and so forth.

API MPMS Chapter 4.9.1 requires a minimum resolution of ± 0.1 °F (± 0.05 °C) and ± 1.0 psig (± 0.069 bar, ± 6.895 kPa) for the temperature and pressure devices involved in the determination of a BPV.

All required data and equation results shall be recorded and rounded (reporting) in accordance with the discrimination and reporting levels specified in the section. For detailed guidance, the user should reference the process maps and examples contained in this standard.

This prover calibration method employs a master flowmeter as a transfer standard between the master prover and the field displacement prover.

This method of prover calibration utilizes the Law of Conservation of Mass, a law of physics, which states that 'assuming no leaks in the system, the mass of the master flowmeter equals the mass of the master prover' and, the 'assuming no leaks in the system, mass of the field displacement prover equals the mass of the master flowmeter'.

5.1 Expanded Discrimination of Master Prover's BPV

The challenge of the methodology is to maintain the calculation discrimination and precision to achieve a six (6) digit base prover volume (BPV) determination of the field displacement prover. This

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is accomplished by an approach that is commonly utilized in experimental research -

- increasing the discrimination and precision of the standard (master prover's BPV)
- rigorous and complex calculational specifications (sequence, equations, discrimination, rounding, etcetera)

This prover calibration method necessitates the increased discrimination of the waterdrawn master prover's Base Prover Volume (BPV) as shown below in Table 9.

Atmospheric Hydrometer or Thermohydrometer

| Decimal Place Color Designation |
|---------------------------------|
| Device Measured Variable |
| Fixed Parameter |
| Calculated Variable |
| Iteration Output Variable |
| Correlation Output Variable |
| Rounded Correlation Value |
| X digits |

| Acronyms | USC Units | Units | SI Units | Units | Parameter | Reference Standards |
|--------------------|-----------|-------|----------|-------|--------------------------|---------------------------------|
| 12.4.2 | 11.1 | kg/m3 | 12.4.2 | 11.1 | kg/m3 | Chapters 9.1, 9.3, 12.4.2 |
| P _{Ind} | 2 | NA | 2 | NA | Device Measured Variable | Chapters 9.1, 9.3, 12.4.2 |
| API _{Ind} | 1 | NA | 1 | NA | Device Measured Variable | Chapters 9.1, 9.3, 12.4.2 |
| RD _{Ind} | NA | NA | NA | NA | Device Measured Variable | Chapters 9.1, 9.3, 12.4.2 |
| T _{Obs} | 2 | 12 | 3 | 12 | Device Measured Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| P _{Obs} | NA | NA | NA | NA | Fixed Parameter | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| T _B | 0 | 0 | 0 | 0 | Fixed Parameter | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| P _B | 0 | 0 | 0 | 0 | Fixed Parameter | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| HYC | 12 | NA | 12 | NA | Calculated Variable | Chapters 9.1, 9.3, 12.4.2 |
| ρ _{Obs} | 12 | 12 | 12 | 12 | Calculated Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| API _{Obs} | NA | 12 | NA | 12 | Calculated Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| RD _{Obs} | NA | 12 | NA | 12 | Calculated Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |

For thermohydrometer or hydrometer in opaque fluids, $\rho_{Ind} = (\rho_{Osg} - \text{meniscus correction for opaque fluids})$

For thermohydrometer or hydrometer in non-opaque fluids, $\rho_{Ind} = \rho_{Osg}$ (at bottom of meniscus)

For thermohydrometer or hydrometer, $\rho_{Obs} = \rho_{Ind} \times HYC$

$$\rho_{Ind} = [(141.5 \times \rho_{Water}) / (API_{Ind} + 131.5)]$$

$$\rho_{Ind} = RD_{Obs} \times \rho_{Water}$$

$$\rho_{Obs} = \rho_{Ind} \times HYC$$

| Chapter 11.1 Iteration Routine INPUTS to determine ρ_{60} , CTL _{60_obs1} , CPL _{60_obs1} , CTPL _{60_obs} | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Units | Parameter | Reference Standards |
|---|--------|------|-------|--------|------|-------|--------------------------|---------------------------------|
| P _{Obs} | 12 | 12 | kg/m3 | NA | NA | kg/m3 | Iteration Input Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| API _{Obs} | NA | NA | *API | NA | NA | *API | Calculated Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| RD _{Obs} | NA | NA | - | NA | NA | - | Calculated Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| T _{Obs} | 2 | 12 | *F | NA | NA | *C | Iteration Input Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| P _{Obs} | 0 | 12 | psig | NA | NA | kPag | Fixed Parameter | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| T _B | 0 | 0 | *F | NA | NA | *C | Fixed Parameter | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| P _B | 0 | 0 | psig | NA | NA | kPag | Fixed Parameter | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| P _c | NA | NA | psig | NA | NA | kPag | Fixed Parameter | Chapters 9.1, 9.3, 12.4.2, 11.1 |

Note: The Chapter 11.1 Iteration Routine is based on a specific set of USC Input units (kg/m³, °F, and psig) since the empirical data set is recorded in these units of measurement. Therefore, the API_{Obs}, RD_{Obs}, T_{Obs}, P_{Obs}, T_B, and P_B values MUST be converted to these specified set of USC units prior to entering the Chapter 11.1 Iteration Routine (very complex and rigid in the sequence of steps).

| Chapter 11.1 Iteration Routine OUTPUTS - ρ_{60} , CTL _{60_obs1} , CPL _{60_obs1} , CTPL _{60_obs} | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Units | Parameter | Reference Standards |
|---|--------|------|-------|--------|------|-------|---------------------------|---------------------------------|
| ρ ₆₀ | 12 | 12 | kg/m3 | NA | 12 | kg/m3 | Iteration Output Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| API ₆₀ | 12 | 12 | *API | NA | 12 | *API | Calculated Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| RD ₆₀ | 12 | 12 | - | NA | 12 | - | Calculated Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| CTL _{60_obs1} , CPL _{60_obs1} , CTPL _{60_obs} | 12 | 12 | - | NA | 12 | - | Iteration Output Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |

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| Densitometer - Online or Handheld | USC Units | | | SI Units | | | Parameter | Reference Standards |
|-----------------------------------|--|--------|------|-------------------|--------|------|---------------------------|----------------------------|
| | Acronyms | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | | |
| | | | | | | | | |
| | | | | | | | | |
| | ρ_{ind} | 3 | NA | kg/m ³ | 3 | NA | Device Measured Variable | Chapters 9.4, 12.4.2 |
| | API _{ind} | NA | NA | °API | NA | NA | Device Measured Variable | Chapters 9.4, 12.4.2 |
| | RD _{ind} | NA | NA | - | NA | NA | Device Measured Variable | Chapters 9.4 |
| | T _{dm} | 2 | 12 | °F | 3 | NA | Device Measured Variable | Chapters 9.4, 12.4.2, 11.1 |
| | P _{dm} | 1 | 12 | psig | 0 | NA | Device Measured Variable | Chapters 9.4, 12.4.2, 11.1 |
| | DMF | 4 | NA | - | 4 | NA | Fixed Parameter | Chapters 9.4, 12.4.2 |
| | $\rho_{obs} = \rho_{ind} \times DMF$ | | | | | | | |
| | Chapter 11.1 Iteration Routine INPUTS to determine ρ_{60}, CTL_{60-TdmPdm}, CPL_{60-TdmPdm}, CTPL_{60-TdmPdm} | | | | | | | |
| | | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Parameter | Reference Standards |
| | ρ_{obs} | 12 | 12 | kg/m ³ | NA | NA | Iteration Input Variable | Chapters 9.4, 12.4.2, 11.1 |
| | API _{obs} | NA | NA | °API | NA | NA | Calculated Variable | Chapters 9.4, 12.4.2, 11.1 |
| | RD _{obs} | NA | NA | - | NA | NA | Calculated Variable | Chapters 9.4, 12.4.2, 11.1 |
| | T _{dm} | 2 | 12 | °F | NA | NA | Iteration Input Variable | Chapters 9.4, 12.4.2, 11.1 |
| | P _{dm} | 1 | 12 | psig | NA | NA | Iteration Input Variable | Chapters 9.4, 12.4.2, 11.1 |
| | T _B | 0 | 0 | °F | NA | NA | Fixed Parameter | Chapters 9.4, 12.4.2, 11.1 |
| | P _B | 0 | 0 | psig | NA | NA | Fixed Parameter | Chapters 9.4, 12.4.2, 11.1 |
| | P _E | NA | NA | psig | NA | NA | Fixed Parameter | Chapters 9.4, 12.4.2, 11.1 |
| | Note: The Chapter 11.1 Iteration Routine is based on a specific set of USC Input units (kg/m ³ , °F, and psig) since the empirical data set is recorded in these units of measurement. Therefore, the APIobs, RDobs, Tdm, and Pdm values MUST be converted to these specified set of USC units prior to entering the Chapter 11.1 Iteration Routine (very complex and rigid in the sequence of steps). | | | | | | | |
| | Chapter 11.1 Iteration Routine OUTPUTS - ρ_{60}, CTL_{60-Tdm}, CPL_{60-TdmPdm}, CTPL_{60-TdmPdm} | | | | | | | |
| | | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Parameter | Reference Standards |
| | ρ_{60} | 12 | 12 | kg/m ³ | NA | NA | Iteration Output Variable | Chapters 9.4, 12.4.2, 11.1 |
| | API ₆₀ | 12 | 12 | °API | NA | NA | Calculated Variable | Chapters 9.4, 12.4.2, 11.1 |
| | RD ₆₀ | 12 | 12 | - | NA | NA | Calculated Variable | Chapters 9.4, 12.4.2, 11.1 |
| | CTL _{Tdm} , CPL _{TdmPdm} , CTPL _{TdmPdm} | 12 | 12 | - | NA | NA | Iteration Output Variable | Chapters 9.4, 12.4.2, 11.1 |

Table 2 – Online or Handheld Densitometer

| Chapter 11.1 Correlation Routine - ρ_{Si} , CTL _{60-to-Si} , CPL _{60-to-Si} , CTPL _{60-to-Si} | USC Units | | | SI Units | | | Parameter | Reference Standards |
|---|---|--------|-------|-------------------|--------|------|-----------------------------|--------------------------------------|
| | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | | | |
| | | | | | | | | |
| | | | | | | | | |
| | ρ_{60} | 12 | 12 | kg/m ³ | NA | NA | Iteration Output Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | T _{15-B} | 0 | 0 | °F | 0 | 0 | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | T _{20-B} | 0 | 0 | °F | 0 | 0 | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | P _B | 0 | 0 | psig | 0 | 0 | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | P _E | NA | NA | psig | NA | NA | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | Chapter 11.1 Correlation Routine INPUTS to determine ρ_{Si}, CTL_{60-to-Si}, CPL_{60-to-Si}, CTPL_{60-to-Si} | | | | | | | |
| | | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Parameter | Reference Standards |
| | ρ_{60} | 12 | 12 | kg/m ³ | NA | NA | Iteration Output Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | T _{15-B} | 0 | 0 | °F | NA | NA | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | T _{20-B} | 0 | 0 | °F | NA | NA | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | P _B | 0 | 0 | psig | NA | NA | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | P _E | NA | NA | psig | NA | NA | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | Chapter 11.1 Correlation Routine OUTPUTS - ρ_{Si}, CTL_{60-to-Si}, CPL_{60-to-Si}, CTPL_{60-to-Si} | | | | | | | |
| | | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Parameter | Reference Standards |
| | ρ_{15} | NA | NA | kg/m ³ | 12 | 12 | Correlation Output Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | API ₁₅ | NA | NA | °API | 12 | 12 | Calculated Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | RD ₁₅ | NA | NA | - | NA | 12 | Calculated Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | CTL _{60-to-15} , CPL _{60-to-15} , CTPL _{60-to-15} | NA | NA | - | 12 | 12 | Correlation Output Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | ρ_{20} | NA | NA | kg/m ³ | 12 | 12 | Correlation Output Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | API ₂₀ | NA | NA | °API | 12 | 12 | Calculated Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | RD ₂₀ | NA | NA | - | NA | 12 | Calculated Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | CTL _{60-to-20} , CPL _{60-to-20} , CTPL _{60-to-20} | NA | NA | - | 12 | 12 | Correlation Output Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |

Table 3 – API MPMS Chapter 11.1 Correlation Routine for ρ_{Si}

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Chapter 11.1 Correlations of CTL, CPL and CTPL - Prover and Meter

| Acronyms | USC Units | | | SI Units | | | Parameter | Reference Standards |
|-----------------|-----------|------|-------------------|----------|------|-------------------|---------------------------|-----------------------|
| | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Units | | |
| ρ_{60} | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Iteration Output Variable | Chapters 12.4.2, 11.1 |
| T_{P_INLET} | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable | Chapter 12.4.2, 11.1 |
| T_{P_OUTLET} | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable | Chapter 12.4.2, 11.1 |
| P_{P_INLET} | 1 | 12 | psig | 0 | 12 | kPag | Device Measured Variable | Chapter 12.4.2, 11.1 |
| P_{P_OUTLET} | 1 | 12 | psig | 0 | 12 | kPag | Device Measured Variable | Chapter 12.4.2, 11.1 |
| T_M | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable | Chapter 12.4.2, 11.1 |
| P_M | 1 | 12 | psig | 0 | 12 | kPag | Device Measured Variable | Chapter 12.4.2, 11.1 |

| Chapter 11.1 Correlation Routine INPUTS to determine CTL _p , CPL _p , and CTPL _p | | | | | | | | |
|--|--------|------|-------------------|--------|------|-------------------|---------------------------|-------------------------------------|
| Acronyms | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Units | Parameter | Reference Standards |
| ρ_{60} | 12 | 12 | kg/m ³ | NA | NA | kg/m ³ | Iteration Output Variable | Chapters 12.4.2, 11.1 |
| T_{P_RUN} | 12 | 12 | °F | NA | NA | °C | Calculated Variable | Chapter 12.4.2, 11.1 - varies w Std |
| P_{P_RUN} | 12 | 12 | psig | NA | NA | kPag | Calculated Variable | Chapter 12.4.2, 11.1 - varies w Std |

Note: The Chapter 11.1 Correlation Routine is based on a specific set of USC Input units (kg/m³, °F, and psig) since the empirical data set is recorded in these units of measurement. Therefore, the ρ_{60} , T_P , P_P values MUST be converted to these specified set of USC units prior to entering the Chapter 11.1 Correlation Routine (very complex and rigid in the sequence of steps).

| Chapter 11.1 Correlation Routine OUTPUTS - CTL _p , CPL _p , CTPL _p | | | | | | | | |
|--|----|----|---|----|----|---|-----------------------------|-----------------------|
| CTL _{60_P} , CPL _{60_P} , CTPL _{60_P} | 12 | 12 | - | NA | NA | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |
| CTL _{15_P} , CPL _{15_P} , CTPL _{15_P} | NA | NA | - | 12 | 12 | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |
| CTL _{20_P} , CPL _{20_P} , CTPL _{20_P} | NA | NA | - | 12 | 12 | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |

| Chapter 11.1 Correlation Routine INPUTS to determine CTL _M , CPL _M , and CTPL _M | | | | | | | | |
|--|--------|------|-------------------|--------|------|-------------------|---------------------------|-----------------------|
| Acronyms | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Units | Parameter | Reference Standards |
| ρ_{60} | 12 | 12 | kg/m ³ | NA | NA | kg/m ³ | Iteration Output Variable | Chapters 12.4.2, 11.1 |
| T_M | 2 | 12 | °F | NA | NA | °C | Device Measured Variable | Chapter 12.4.2, 11.1 |
| P_M | 1 | 12 | psig | NA | NA | kPag | Device Measured Variable | Chapter 12.4.2, 11.1 |

Note: The Chapter 11.1 Correlation Routine is based on a specific set of USC Input units (kg/m³, °F, and psig) since the empirical data set is recorded in these units of measurement. Therefore, the ρ_{60} , T_M , P_M values MUST be converted to these specified set of USC units prior to entering the Chapter 11.1 Correlation Routine (very complex and rigid in the sequence of steps).

| Chapter 11.1 Correlation Routine OUTPUTS - CTL _M , CPL _M , CTPL _M | | | | | | | | |
|--|----|----|---|----|----|---|-----------------------------|-----------------------|
| CTL _{60_M} , CPL _{60_M} , CTPL _{60_M} | 12 | 12 | - | NA | NA | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |
| CTL _{15_M} , CPL _{15_M} , CTPL _{15_M} | NA | NA | - | 12 | 12 | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |
| CTL _{20_M} , CPL _{20_M} , CTPL _{20_M} | NA | NA | - | 12 | 12 | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |

| Chapter 11.1 Rounded Values for Proving Report and BPV Determination Calculations | | | | | | | | |
|---|---|----|---|---|----|---|---------------------------|-----------------------|
| Rnd CTL, Rnd CPL, Rnd CTPL | 9 | NA | - | 9 | NA | - | Rounded Correlation Value | Chapters 12.4.2, 11.1 |

Table 4 – API MPMS Chapter 11.1 Correlation Routine for CTL, CPL and CTPL

| Steel - Dimensions, Properties, Correction Factors (CTS _p , CPS _p) | Acronyms | USC Units | | | SI Units | | | Parameter | Reference Standards |
|---|-----------------------------------|-----------|------|----------|----------|------|---------------------|-----------------------|-------------------------|
| | | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Units | | |
| | OD _p | NA | NA | in | NA | NA | mm | Fixed Parameter | Chapters 12.4.1, 12.4.2 |
| | ID _p | 4 | 4 | in | 3 | 3 | mm | Fixed Parameter | Chapters 12.4.1, 12.4.2 |
| | WT _p | 4 | 4 | in | 3 | 3 | mm | Fixed Parameter | Chapters 12.4.1, 12.4.2 |
| | E _p | 0 | 0 | per psig | 0 | 0 | per kPag | Fixed Parameter | Chapters 12.4.1, 12.4.2 |
| | GL _p | 8 | 8 | per °F | 8 | 8 | per °C | Fixed Parameter | Chapters 12.4.1, 12.4.2 |
| | GL _Q | 8 | 8 | per °F | 8 | 8 | per °C | Fixed Parameter | Chapters 12.4.1, 12.4.2 |
| | Open Tank Prover, GC _p | 8 | 8 | per °F | 8 | 8 | per °C | Fixed Parameter | Chapters 12.4.1, 12.4.2 |
| | T _B | 0 | 0 | °F | 0 | 0 | °C | Fixed Parameter | Chapters 12.4.2, 11.1 |
| P _B | 0 | 0 | psig | 0 | 0 | kPag | Fixed Parameter | Chapters 12.4.2, 11.1 | |
| CTS _p | 12 | 12 | - | 12 | 12 | - | Calculated Variable | Chapter 12.4.2 | |
| CPS _p | 12 | 12 | - | 12 | 12 | - | Calculated Variable | Chapter 12.4.2 | |
| Rnd CTS _p | 9 | 9 | - | 9 | 9 | - | Calculated Variable | Chapter 12.4.2 | |
| Rnd CPS _p | 9 | 9 | - | 9 | 9 | - | Calculated Variable | Chapter 12.4.2 | |
| Chapter 12.4.2 calculates the CTS _p and CPS _p terms to 12 decimal places to convert Master CPV to Master BPV (10 digits). | | | | | | | | | |
| Chapter 12.4.2 rounds the CTS _p and CPS _p terms to 9 decimal places for the report calculations. | | | | | | | | | |
| Terms not contained in Chapter 11.1 have defaulted to the discriminations stated in Chapter 12.4.2. | | | | | | | | | |

Table 5 – Steel Dimensions, Properties and Correction Factors

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| Acronyms | USC Units | | | SI Units | | | Parameter | Reference Standards |
|--|-----------|-----------|---------------------|-----------|-----------|-------------------------|-----------------------------|--------------------------------------|
| | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | Units | | |
| | 1 | 12 | | 1 | 12 | | | |
| API _{ind} | 1 | 12 | °API | 1 | 12 | °API | Device Measured Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| RD _{ind} | NA | NA | - | NA | NA | - | Device Measured Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| Hydrometer or Densitometer ρ _{ind} | 3 | 12 | kg/m ³ | 3 | 12 | kg/m ³ | Device Measured Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| Hydrometer T _{obs} | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable | Chapters 9.1, 9.3, 12.4.2, 11.1 |
| Densitometer T _{dm} | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable | Chapters 9.4, 12.4.2, 11.1 |
| T _{P_inlet} , T _{P_outlet} , T _D , T _M | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable | Chapters 12.4.2, 11.1 |
| Densitometer P _{dm} | 1 | 12 | psig | 0 | 12 | kPag | Device Measured Variable | Chapters 12.4.2, 11.1 |
| P _{P_inlet} , P _{P_outlet} , P _M | 1 | 12 | psig | 0 | 12 | kPag | Device Measured Variable | Chapters 12.4.2, 11.1 |
| N | 0 | 0 | whole pulses | 0 | 0 | whole pulses | Device Measured Variable | Chapters 12.4.2, 11.1 |
| N _i | 3 | 3 | interpolated pulses | 3 | 3 | interpolated pulses | Device Measured Variable | Chapters 12.4.2, 11.1 |
| Open Tank Provers, SR _{UPPER} | Cert | Cert | Bbl | Cert | NA | M ³ | Device Measured Variable | Chapters 12.4.1, 12.4.2 |
| Open Tank Provers, SR _{LOWER} | Cert | Cert | Bbl | Cert | NA | M ³ | Device Measured Variable | Chapters 12.4.1, 12.4.2 |
| Q _{av} | 5 digits | 5 digits | BPH | 5 digits | 5 digits | MPH | Device Measured Variable | 5 digits per Chapter 12.4.2 |
| Hydrometer P _{obs} | 0 | 0 | psig | 0 | 0 | kPag | Fixed Parameter | Chapters 12.4.2, 11.1 |
| T _B | 0 | 0 | °F | 0 | 0 | °C | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| P _B | 0 | 0 | psig | 0 | 0 | kPag | Fixed Parameter | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| DMF | 4 | 4 | - | 4 | 4 | - | Fixed Parameter | Chapters 9.4, 12.4.2, 11.1 |
| ID _P | 4 | 4 | inch | 3 | 3 | mm | Fixed Parameter | Chapters 12.4.2, 11.1 |
| WT _P | 4 | 4 | inch | 3 | 3 | mm | Fixed Parameter | Chapters 12.4.2, 11.1 |
| E _P | 0 | 0 | per psig | 0 | 0 | per kPag | Fixed Parameter | Chapters 12.4.2, 11.1 |
| GL _P | 8 | 8 | per °F | 8 | 8 | per °C | Fixed Parameter | Chapters 12.4.2, 11.1 |
| GL _D | 8 | 8 | per °F | 8 | 8 | per °C | Fixed Parameter | Chapters 12.4.2, 11.1 |
| Master Prover BPV _P | 4 | 4 | cubic inches | 3 | 3 | mL | Fixed Parameter | Chapters 12.4.2, 11.1 |
| NKF | 7 digits | 7 digits | Pulses / Bbl | 7 digits | 7 digits | Pulses / M ³ | Fixed Parameter | 7 digits per Chapter 12.4.2 |
| Base - CTS ₀₀ , CTS ₁₅ , CTS ₂₀ | 9 | 9 | - | 9 | 9 | - | Calculated Parameter | Chapter 12.4.2 |
| Master - BPV ₀₀ , BPV ₁₅ , BPV ₂₀ | 10 digits | 10 digits | Bbl | 10 digits | 10 digits | M ³ | Calculated Parameter | 10 digits per Ch 12.4.2 |
| P ₀₀ | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Iteration Output Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| P ₀₀ | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Correlation Input Variable | Chapters 12.4.2, 11.1 |
| P ₁₅ , P ₂₀ | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Correlation Output Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| API _B , API ₀₀ , API ₁₅ , API ₂₀ | 12 | 12 | °API | 12 | 12 | °API | Calculated Variable | Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| N _{avg} | 7 digits | 7 digits | pulses | 7 digits | 7 digits | pulses | Calculated Variable | 7 digits per Chapters 12.4.2, 11.1 |
| N _{i avg} | 7 digits | 7 digits | pulses | 7 digits | 7 digits | pulses | Calculated Variable | 7 digits per Chapters 12.4.2, 11.1 |
| T _{P_RUN} | 12 | 12 | °F | 12 | 12 | °C | Calculated Variable | Chapter 12.4.2, 11.1 - varies w Std |
| P _{P_RUN} | 12 | 12 | psig | 12 | 12 | kPag | Calculated Variable | Chapter 12.4.2, 11.1 - varies w Std |
| CTS _P | 9 | 9 | - | 9 | 9 | - | Calculated Variable | Chapter 12.4.2 |
| CPS _P | 9 | 9 | - | 9 | 9 | - | Calculated Variable | Chapter 12.4.2 |
| CTL _{obs} , CTL _{TdmPdm} , CTL _P , CTL _M | 12 | 12 | - | 12 | 12 | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |
| CPL _{obs} , CPL _{TdmPdm} , CPL _P , CPL _M | 12 | 12 | - | 12 | 12 | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |
| CTPL _{obs} , CTPL _{TdmPdm} , CTPL _P , CTPL _M | 12 | 12 | - | 12 | 12 | - | Correlation Output Variable | Chapters 12.4.2, 11.1 |
| Rnd'd - CTL _P , CTL _M | 9 | 9 | - | 9 | 9 | - | Rounded Correlation Output | Chapters 12.4.2 |
| Rnd'd - CPL _P , CPL _M | 9 | 9 | - | 9 | 9 | - | Rounded Correlation Output | Chapters 12.4.2 |
| Rnd'd - CTPL _P , CTPL _M | 9 | 9 | - | 9 | 9 | - | Rounded Correlation Output | Chapters 12.4.2 |
| Proving Repeatability (r) | 3 | 3 | % | 3 | 3 | % | Calculated Variable | Chapters 12.4.2, 11.1 |
| IMF | 8 | 8 | - | 8 | 8 | - | Calculated Variable | Chapters 12.4.2, 11.1 |
| IMF | 7 | 7 | - | 7 | 7 | - | Calculated Variable | Chapters 12.4.2, 11.1 |
| GSV | 10 digits | 10 digits | Bbl | 10 digits | 10 digits | M ³ | Calculated Variable | 10 digits per Ch 12.4.2, 11.1 |
| IV, ISV | 10 digits | 10 digits | Bbl | 10 digits | 10 digits | M ³ | Calculated Variable | 10 digits per Ch 12.4.2, 11.1 |

Chapter 12.4.2 specifies **only** one (1) trip per proving run. Multiple trips as a single proving run is **NOT** allowed.
Terms not contained in Chapter 11.1 have been assigned a discrimination by Chapter 12.4.2.

Table 6 – Master Meter Proving Report

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| Chapter 12.4.2 - Master Meter Calibration of Displacement Prover - BPV Report Determination | USC Units | | | SI Units | | | Parameter | Reference Standards |
|---|--|-----------|-----------|---------------------|-----------|-----------|-------------------|--|
| | Acronyms | 12.4.2 | 11.1 | Units | 12.4.2 | 11.1 | | |
| | | | | | | | | |
| | Densitometer ρ_{hd} | 3 | 12 | kg/m ³ | 3 | 12 | kg/m ³ | Device Measured Variable Chapters 9.1, 9.3, 12.4.2, 11.1 |
| | Densitometer T_{dm} | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable Chapters 9.4, 12.4.2, 11.1 |
| | T_D , T_{P_INLET} , T_{P_OUTLET} | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable Chapters 12.4.2, 11.1 |
| | P_{P_INLET} , P_{P_OUTLET} | 1 | 12 | psig | 0 | 12 | kPag | Device Measured Variable Chapters 12.4.2, 11.1 |
| | T_M | 2 | 12 | °F | 3 | 12 | °C | Device Measured Variable Chapters 12.4.2, 11.1 |
| | P_M | 1 | 12 | psig | 0 | 12 | kPag | Device Measured Variable Chapters 12.4.2, 11.1 |
| | Q_{av} | 5 digits | 5 digits | BPH | 5 digits | 5 digits | MPH | Device Measured Variable 5 digits per Chapter 12.4.2 |
| | N | 0 | 0 | whole pulses | 0 | 0 | pulses | Device Measured Variable Chapters 12.4.2, 11.1 |
| | Ni | 3 | 3 | interpolated pulses | 3 | 3 | pulses | Device Measured Variable Chapters 12.4.2, 11.1 |
| | Open Tank Provers, SR_{UPPER} | Cert | Cert | Bbl | Cert | NA | M ³ | Device Measured Variable Chapters 12.4.1, 12.4.2 |
| | Open Tank Provers, SR_{LOWER} | Cert | Cert | Bbl | Cert | NA | M ³ | Device Measured Variable Chapters 12.4.1, 12.4.2 |
| | Hydrometer P_{obs} | 0 | 0 | psig | 0 | 0 | kPag | Fixed Parameter Chapters 9.1, 9.3, 12.4.2 |
| | T_B | 0 | 0 | °F | 0 | 0 | °C | Fixed Parameter Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | P_B | 0 | 0 | psig | 0 | 0 | kPag | Fixed Parameter Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | DMF | 4 | 4 | - | 4 | 4 | - | Fixed Parameter Chapters 9.4, 12.4.2, 11.1 |
| | ID _p | 4 | 4 | inch | 3 | 3 | mm | Fixed Parameter Chapters 12.4.1, 12.4.2, 11.1 |
| | WT _p | 4 | 4 | inch | 3 | 3 | mm | Fixed Parameter Chapters 12.4.1, 12.4.2, 11.1 |
| | E _p | 8 | 8 | per psig | 8 | 8 | per kPag | Fixed Parameter Chapters 12.4.1, 12.4.2, 11.1 |
| | GL _p | 8 | 8 | per °F | 8 | 8 | per °C | Fixed Parameter Chapters 12.4.1, 12.4.2, 11.1 |
| | NKF | 7 digits | 7 digits | P / Bbl | 7 digits | 7 digits | P / M3 | Fixed Parameter 7 digits per Chapter 12.4.1 |
| | BPV _{OLD} or BPV _{TARGET} | 4 | 4 | cubic inches | 3 | 3 | mL | Fixed Parameter Chapters 12.4.1, 12.4.2, 11.1 |
| | BPV _{OLD} or BPV _{TARGET} | 6 digits | 6 digits | Bbl | 6 digits | 6 digits | M ³ | Fixed Parameter 6 digits per Chapters 12.4.1, 12.4.2 |
| | Base - CTS ₆₀ , CTS ₁₅ , CTS ₂₀ | 9 | 9 | - | 9 | 9 | - | Calculated Parameter Chapter 12.4.2, Converts Master BPV _p to 10 digits |
| | ρ_{obs} | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Iteration Input Variable Chapters 9.1, 12.4.2, 11.1 |
| | ρ_{60} | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Iteration Output Variable Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | ρ_{60} | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Correlation Input Variable Chapters 12.4.2, 11.1 |
| | ρ_{15} , ρ_{20} | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Correlation Output Variable Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | API _B , API ₆₀ , API ₁₅ , API ₂₀ | 12 | 12 | °API | 12 | 12 | °API | Calculated Variable Chapters 9.1, 9.3, 9.4, 12.4.2, 11.1 |
| | P_{60_START} , P_{60_STOP} , P_{60_SET} | 12 | 12 | kg/m ³ | 12 | 12 | kg/m ³ | Calculated Variable Chapters 12.4.2, 11.1 |
| | MMF _{START} , MMF _{STOP} , MMF _{SET} | 7 | 7 | - | 7 | 7 | - | Calculated Variable Chapter 12.4.2 |
| | Navg | 7 digits | 7 digits | pulses | 7 digits | 7 digits | pulses | Calculated Variable 7 digits per Chapters 12.4.2, 11.1 |
| | N _{avg} | 7 digits | 7 digits | pulses | 7 digits | 7 digits | pulses | Calculated Variable 7 digits per Chapters 12.4.2, 11.1 |
| | T_{P_RUN} | 12 | 12 | °F | 12 | 12 | °C | Calculated Variable Chapter 12.4.2, 11.1 - varies w Std |
| | P_{P_RUN} | 12 | 12 | psig | 12 | 12 | kPag | Calculated Variable Chapter 12.4.2, 11.1 - varies w Std |
| | CTS _p | 9 | 9 | - | 9 | 9 | - | Calculated Variable Chapter 12.4.2 |
| | CPS _p | 9 | 9 | - | 9 | 9 | - | Calculated Variable Chapter 12.4.2 |
| | CTL _{obs} , CTL _{Tdmpdm} , CTL _p , CTL _M | 12 | 12 | - | 12 | 12 | - | Correlation Output Variable Chapters 12.4.2, 11.1 |
| | CPL _{obs} , CPL _{Tdmpdm} , CPL _p , CPL _M | 12 | 12 | - | 12 | 12 | - | Correlation Output Variable Chapters 12.4.2, 11.1 |
| | CTPL _{obs} , CTPL _{Tdmpdm} , CTPL _p , CTPL _M | 12 | 12 | - | 12 | 12 | - | Correlation Output Variable Chapters 12.4.2, 11.1 |
| | Rnd'd - CTL _p , CTL _M | 9 | 9 | - | 9 | 9 | - | Rounded Correlation Output Chapters 12.4.2 |
| | Rnd'd - CPL _p , CPL _M | 9 | 9 | - | 9 | 9 | - | Rounded Correlation Output Chapters 12.4.2 |
| | Rnd'd - CTPL _p , CTPL _M | 9 | 9 | - | 9 | 9 | - | Rounded Correlation Output Chapters 12.4.2 |
| | GSV | 10 digits | 10 digits | Bbl | 10 digits | 10 digits | M ³ | Calculated Variable 10 digits per Ch 12.4.2, 11.1 |
| | IV, ISV | 10 digits | 10 digits | Bbl | 10 digits | 10 digits | M ³ | Calculated Variable 10 digits per Ch 12.4.2, 11.1 |
| | Proving Repeatability (r) | 3 | 3 | % | 3 | 3 | % | Calculated Variable Chapters 12.4.2, 11.1 |
| | ICPV _{RUN} | 9 digits | 9 digits | Bbl | 9 digits | 9 digits | M ³ | Calculated Variable 9 digits per Chapter 12.4.2 |
| | CPV _{RUN} , CPV _{SET} | 9 digits | 9 digits | Bbl | 9 digits | 9 digits | M ³ | Calculated Variable 9 digits per Chapter 12.4.2 |
| | Average CPV _{SET} | 9 digits | 9 digits | Bbl | 9 digits | 9 digits | M ³ | Calculated Variable 9 digits per Chapter 12.4.2 |
| | Repeatability (r) in a Set - ICPV _{RUN} , CPV _{RUN} | 3 | 3 | % | 3 | 3 | % | Calculated Variable Chapter 12.4.2 |
| | Δ MMF (MMF _{START} , MMF _{STOP}) in a Set | 3 | 3 | % | 3 | 3 | % | Calculated Variable Chapter 12.4.2 |
| | Reproducibility (R) of CPV _{SET} between Sets | 3 | 3 | % | 3 | 3 | % | Calculated Variable Chapter 12.4.2 |
| | ΔQ_{SET} | 3 | 3 | % | 3 | 3 | % | Calculated Variable Chapter 12.4.2 |
| | BPV _{NEW} | 4 | 4 | cubic inches | 3 | 3 | mL | Calculated Variable Chapters 12.4.1, 12.4.2 |
| | BPV _{NEW} | 6 digits | 6 digits | Bbl | 6 digits | 6 digits | M ³ | Calculated Variable 6 digits per Chapters 12.4.1, 12.4.2 |
| | BPV _{NEW} | 6 digits | 6 digits | gal | 6 digits | 6 digits | L | Calculated Variable 6 digits per Chapters 12.4.1, 12.4.2 |
| | BPV _{NEW} | 6 digits | 6 digits | ft ³ | NA | NA | - | Calculated Variable 6 digits per Chapters 12.4.1, 12.4.2 |

Chapter 12.4.2 specifies **only** one (1) trip per proving run. Multiple trips as a single proving run is **NOT** allowed.
Terms not contained in Chapter 11.1 have been assigned a discrimination by Chapter 12.4.2.

Table 7 – Field Prover's BPV Calibration Report

| Base Unit Volume | | |
|-------------------------|-------------------|-----------------------------------|
| BPV₆₀ | XXX XXX XXX.xxx x | cubic inches at 60.0 °F, 0.0 psig |
| BPV₁₅ | XXX XXX XXX.xxx | mL at 15.0 °C and 0.0 kPag |
| BPV₂₀ | XXX XXX XXX.xxx | mL at 20.0 °C and 0.0 kPag |

Table 8 – Base Unit Volumes

| Base Prover Volume (BPV) | | | | |
|--------------------------|-----------------------|----------------------------------|-----------------------------------|---------------|
| USC | | | SI | |
| Barrels (Bbl) | U.S. Gallons (gal) | Cubic Feet (ft ³) | Cubic Meters (M ³) | Liters (L) |
| XX XXX.x0 | XX XXX.x0 | XX XXX.x0 | XX XXX.x0 | XX XXX.x0 |
| X XXX.xx 0 | X XXX.xx 0 | X XXX.xx 0 | X XXX.xx 0 | X XXX.xx 0 |
| XXX.xxx 0 | XXX.xxx 0 | XXX.xxx 0 | XXX.xxx 0 | XXX.xxx 0 |
| XX.xxx x0 | XX.xxx x0 | XX.xxx x0 | XX.xxx x0 | XX.xxx x0 |
| X.xxx xx0 | X.xxx xx0 | X.xxx xx0 | X.xxx xx0 | X.xxx xx0 |
| 0.xxx xxx 0 | 0.xxx xxx 0 | 0.xxx xxx 0 | 0.xxx xxx 0 | 0.xxx xxx 0 |
| 0.0xx xxx x0 | 0.0xx xxx x0 | 0.0xx xxx x0 | 0.0xx xxx x0 | 0.0xx xxx x0 |

Note: The BPV Volumes shown above are specified based on 6 significant digits (10 ppm, or 0.001 %).

Table 9 – BPV Reporting

6. Correction for Temperature on Steel (CTS)

Any container (displacement prover, tank prover) when subjected to a change in temperature will change its volume accordingly. The volume change, regardless of shape, is proportional to the coefficient of thermal expansion of the single construction material(s).

The linear coefficient of thermal expansion (GL) is required for displacement provers.

The linear or cubical coefficient of thermal expansion (GL, GC) may be used for an open tank prover.

For displacement prover and open tank provers, the equations to calculate CTS are specified in API *MPMS* Chapter 12.4.1.

7. Correction for Pressure on Steel (CPS)

If a metal pressurized container (displacement prover) is subjected to an internal pressure, the walls of the container will stretch elastically, and the volume of the container will change accordingly.

The modulus of elasticity (*E*) shall be determined for the materials used in the construction of the calibrated section. If the modulus of elasticity (*E*) is unknown, the values contained in Table 4 through Table 6 shall be used.

For displacement provers, the equations to calculate CPS are specified in API *MPMS* Chapter 12.4.1.

Since an open tank prover operates at atmospheric pressure, this prover design is not subjected to internal pressure. Therefore, the CPS = 1.000 000 for an open tank prover.

8. Correction for Temperature and Pressure on Hydrocarbon Liquid (CTL, CPL, CTPL)

For displacement provers (free or captive displacer), the application of this standard shall be limited to low vapor pressure hydrocarbon liquids, which are assumed to be clean and air/gas free. To properly implement the procedures to correct measured quantities at flowing temperatures and pressures to corresponding quantities at base (reference or standard) conditions, the hydrocarbon liquid density correlations specified in API *MPMS* Chapter 11.1 shall be utilized to perform the complex calculations.

8.1 Correction for Effect of Temperature on Hydrocarbon Liquid (CTL)

If a hydrocarbon liquid is subjected to a change in temperature, its density will decrease as the temperature rises or increase as the temperature falls. This density change is proportional to the thermal coefficient of expansion of the liquid and temperature.

The correction factor for the effect of temperature on the liquid's density (CTL) is a function of the following correlation:

$$CTL \sim f(\rho_B, T)$$

8.2 Correction for Effect of Pressure on Hydrocarbon Liquid (CPL)

If a hydrocarbon liquid is subjected to a change in pressure, the liquid density will increase as the pressure rises or decrease as the pressure falls.

The correction factor for the effect of pressure on the liquid's density (CPL) is a function of the following correlation:

$$CPL \sim f(\rho_B, F, P_E, P)$$

8.3 Correction for Effect of Temperature and Pressure on Hydrocarbon Liquid (CTPL)

If a hydrocarbon liquid is subjected to a change in temperature and pressure, the liquid density is a function of the following correlations:

$$CTPL = CTL \times CPL = \frac{\rho_{TP}}{\rho_B}$$

9. Correction for Temperature and Pressure on Water (CTL, CPL, CTPL)

For any open tank provers that are utilized as a master prover, the application of this standard shall be limited to potable water, which is assumed to be clean, air/gas free. To properly implement the procedures to correct measured volumes at flowing temperatures and pressures to corresponding volumes at base (reference or standard) conditions, the water density correlations specified in API *MPMS* Chapters 12.4.1 and 11.4.1 shall be utilized to perform the complex calculations.

10. Measurement Readings

There are two approaches for the **measurement of temperature and pressure** - automated or manual.

There are two methods for the measurement of **fluid density** - continuous sampling (online densitometer) or spot sampling.

10.1 Measurement of Temperature and Pressure - Automated

For systems employing **automated measurements**, the readings associated with the master prover, master meter and field prover (T_P , T_D , P_P , T_M , P_M) shall be a snapshot or averaged (flow-weighted or time-based) when the displacer is between detector switches for each proving run (roundtrip) **of the master prover** in accordance with API *MPMS* Chapter 4.8 **to determine a Master Meter Factor (MMF)**.

For systems employing **automated measurements**, the readings of T_P , T_D , P_P , T_M , and P_M shall be a snapshot or averaged (flow-weighted or time-based) when the displacer is between detector switches for each proving run (roundtrip) **of the field prover** in accordance with API *MPMS* Chapter 4.9.2 **to determine a CPV_{RUN}** .

10.2 Measurement of Temperature and Pressure - Manual

For systems employing **manual measurements**, the readings associated with the master prover and master meter (T_P , T_D , P_P , T_M , P_M) shall be recorded when the displacer is between detector switches for each proving run (roundtrip) **of the master prover** in accordance with API *MPMS* Chapter 4.8 **to determine a Master Meter Factor (MMF)**.

For systems employing **manual measurements**, the readings associated with the master meter and field prover (T_M , P_M , T_P , T_D , P_P) shall be recorded when the displacer is between detector switches for each proving run (roundtrip) **of the field prover** in accordance with API *MPMS* Chapter 4.9.2 **to determine a CPV_{RUN}** .

10.3 Density Measurement – Continuous or Online

The Continuous (or Online) Sampling Method requires an online densitometer to determine the base density (ρ_B) for each proving run. The values of ρ_{obs} , T_{dm} , and P_{dm} shall be a snapshot or averaged (flow-weighted or time-based) when the displacer is between detector switches for each proving run (roundtrip) **of the master prover** in accordance with API *MPMS* Chapter 4.8 **to determine a Master Meter Factor (MMF)**.

10.4 Density Measurement – Spot Sample

The Spot Sampling Method requires a density determination at the START of a Proving Report using atmospheric density devices (hydrometer, thermohydrometer, handheld densitometer) or laboratory analysis to determine the base density (ρ_B). This method assumes the base density (ρ_B) is constant for the proving report (all proving runs) in accordance with API *MPMS* Chapter 4.8 **to determine a Master Meter Factor (MMF)**.

The Spot Sampling Method requires a density determination at the START of a CPV_{RUN} using atmospheric density devices (hydrometer, thermohydrometer, handheld densitometer) or laboratory analysis to determine the base density (ρ_B) **of the master meter and field prover** in accordance with

API MPMS Chapter 4.9.2 to **determine a CPV_{RUN}**. This method assumes the base density (ρ_B) is constant for a calibration run of the field prover (CPV_{RUN}) and any fluid properties' variation (ρ_B , v_{TP}) between the START and STOP Proving Reports and associated Calibration Runs (CPV_{RUN}) will have a minimal impact of the calibration of the field prover.

11. MMF Methods

There are two methods to establish a **Master Meter Factor (MMF)** - Intermediate Meter Factor (IMF) and Average Data.

The **Intermediate Meter Factor (IMF) Method** uses the GSV_P and ISV_M to calculate the IMF for each proving run. The average of the selected proving runs' IMF values that satisfy the repeatability criteria (r%) determines the MF or MMF.

The Intermediate Factor Method (IMF) is the preferred method as variations in temperature, pressure, and if employing an online densitometer - base density, are accounted for in the evaluation of the proving results.

The **Average Data Method** uses the average of the measurements (ρ_B , T_P , T_D , P_P , N or N_i , T_M , P_M) from the selected proving runs' that satisfy a Fixed Range (r%) criteria (5 consecutive runs) to calculate a single value for GSV_P, ISV_M, and MF or MMF. The proving runs' pulses (N or N_i) are evaluated to satisfy the repeatability ($r \leq 0.020$ %) criteria.

The **Multiple Run Sets Method** shall not be applied to generate a MMF for calibration of a field prover. This method is applied to unstable process conditions (flowrates, fluid density, temperature, pressure, viscosity) or use of an inappropriately sized prover for challenging applications.

12. Repeatability (r%) Methods

The Master Meter Repeatability Criteria is, as specified in API MPMS Chapter 4.9.3, $r\% \leq 0.020$ % for a MMF using the Fixed Range Method.

The maximum number of consecutive proving runs is ten (10) by industry practice.

There are two methods to determine flowmeter repeatability (r%) - Moving Range and Fixed Range.

To restate, API MPMS Chapter 12.2 states: "Historically, the Average Data Method has been used since it only requires a single calculation at the end to determine the Meter Factor. *The Intermediate Factor Method (IMF) is the preferred method as variations in temperature and pressure are accounted for in the evaluation of the proving results.*"

The **Moving Range (or Standard Deviation) Method** requires three (3) or more consecutive proving runs' IMF to satisfy the repeatability criteria. The maximum number of consecutive proving runs is ten (10) according to industry practice.

Matrixes C, D, and E are applicable to stable process conditions (flowrates, base density, viscosity, temperature, pressure). These Matrixes will produce a calibration system's discriminations approximating Matrixes A and B values for repeatability and reproducibility.

The Multiple Run Sets Method *shall not be applied to generate a MMF for calibration of a field prover*. This method is applied to unstable process conditions (flowrates, fluid density, temperature, pressure, viscosity) or use of an inappropriately sized prover for challenging applications.

| Matrix | MMF Proving Matrixes | | | | | |
|----------------------|----------------------|----|----|----|----|---------------------------|
| | A | B | C | D | E | |
| ρ_{obs} Methods | x | x | - | - | - | Continuous Sampling |
| | - | - | x | x | x | Spot Sample |
| Meter Factor Methods | x | x | x | x | - | Intermediate (IMF) |
| | - | - | - | - | x | Average Data |
| | NA | NA | NA | NA | NA | Multiple Run Sets |
| (r%) Methods | x | - | x | - | - | Moving Range (or Std Dev) |
| | - | x | - | x | x | Fixed Range |

Figure 1 – MMF Proving Report Matrixes

14. Prover Calibration Method Using a Master Meter

The Master Meter Method for Calibrating a Prover consists of the matrixes shown in Figure 2.

Matrix A will provide the calibration system's highest discrimination for repeatability and reproducibility.

Matrix B is applicable to stable process conditions (flowrates, base density, viscosity, temperature, pressure). This Matrix will produce a calibration system's discriminations approximating Matrix A values for repeatability and reproducibility.

Three (3) methods for prover calibration using the master meter volumetric method are specified in API MPMS Chapter 4.9.3 and shown in Figure 3.

14.1 Master Meter Criteria

For the Standard Method, the ΔMMF_{SET} shall be ≤ 0.020 % for Selected Three (3) Consecutive Runs for a Set.

For Alternate "A" Method, the ΔMMF_{RUN} shall be ≤ 0.020 % for Selected Three (3) Consecutive Runs in a Set.

For Alternate "B" Method, ΔMMF_{START} , $ABS(MMF_1 - MMF_2)$, $ABS(MMF_2 - MMF_3)$, shall be ≤ 0.020 % for Selected Three (3) Consecutive Runs in a Set.

| | BPV Determination - Matrixes | | |
|-------------------|------------------------------|---|----------------------|
| | A | B | |
| ρ_b Methods | x | - | Continuous Sampling |
| | - | x | Spot Sample |
| BPV Determination | x | x | Standard Method |
| | x | x | Alternate Method "A" |
| | x | x | Alternate Method "B" |
| (r%) Method | x | x | Fixed Range |

Figure 2 – Master Meter Method Matrix for Prover Calibration

14.2 Field Prover Calibration Criteria

For All Methods, a Calibration Set (CPV_{SET}) consists of a minimum of three (3) consecutive and a maximum of six (6) consecutive Calibration Runs (CPV_{RUN}), in accordance with API *MPMS* Chapter 4.9.3.

14.2.1 Flowrate Variation in a Calibration Set Criteria (ΔQ_{SET})

The flow rate during a calibration run set should be stable. Maintaining the flow rate of each pass of a calibration run set within a range of 5 % will aid in fulfilling the other repeatability criteria.

14.2.2 Repeatability in a Calibration Set ($r_{\Delta CPV_{SET}}$)

API *MPMS* Chapter 4.9.3, the prover calibration shall demonstrate a **Calibration Set Repeatability** ($r_{\Delta CPV_{SET}} \leq 0.020$ % for three (3) consecutive calibration runs out of a maximum of six (6) consecutive calibration runs in a Calibration Set.

14.2.3 Reproducibility of Three (3) Calibration Sets Criteria ($R_{\Delta CPV_{SET}}$)

For All Methods, in accordance with API *MPMS* Chapter 4.9.3, the $r_{\Delta CPV_{RUN}}$ shall be ≤ 0.020 % for Selected three (3) Consecutive Runs in a Set.

14.3 CPV Determinations

For All Methods, in accordance with API *MPMS* Chapter 4.9.3, a Calibration Set (CPV_{SET}) is calculated using the following equation:

$$CPV_{SET} = \frac{\sum^3 CPV_{RUN}}{3} \quad (2)$$

For All Methods, the following criteria shall be met:

- three (3) Consecutive Calibration Sets (CPV_{SET}) shall be performed at three (3) different flowrates.

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- the flowrate for the 2nd Calibration Set (CPV_{SET_II}) shall be at least ± 25.0 % different from 1st Calibration Set (CPV_{SET_I}).
- the flowrate for the 3rd Calibration Set (CPV_{SET_III}) shall be at least 25.0 % greater than the highest flowrate of the two previous Consecutive Calibration Sets.
- Three (3) Consecutive Calibration Sets to satisfy the reproducibility criteria ($R_{\Delta CPV_{SET}} \leq 0.020$ % over three (3) different flowrates.
- the ΔCPV_{SET} reproducibility (R) shall be ≤ 0.020 % for the three (3) Consecutive Calibration Sets.

For the Standard Method, the $r_{\Delta CPV_{RUN}}$ shall be ≤ 0.020 % for Selected 3 Consecutive Runs in a Set.

| Standard Method | | Alternate Method A | | Alternate Method B | |
|---|-----------------|---|-----------------|---|-----------------|
| | | Uses MMF _{stop} as the MMF _{start} for next run | | Simultaneous MMF and Field Prover Calibration | |
| Calibration Run Set I | | Calibration Run Set I | | Calibration Run Set I | |
| MMF _{start} | MMF1 | MMF _{start} | MMF1 | | |
| Calibration Run 1 | 1st consecutive | Calibration Run 1 | 1st consecutive | MMF | MMF1 |
| | | MMF _{stop} | MMF2 | and Calibration Run 1 | 1st consecutive |
| | | MMF _{start} | Same as MMF2 | | |
| Calibration Run 2 | 2nd consecutive | Calibration Run 2 | 2nd consecutive | MMF | MMF2 |
| | | MMF _{stop} | MMF3 | and Calibration Run 2 | 2nd consecutive |
| | | MMF _{start} | Same as MMF3 | | |
| Calibration Run 3 | 3rd consecutive | Calibration Run 3 | 3rd consecutive | MMF | MMF3 |
| MMF _{stop} | MMF2 | MMF _{stop} | MMF4 | and Calibration Run 3 | 3rd consecutive |
| Above pattern can be continued up to a maximum of six consecutive calibration runs | | Above pattern can be continued up to a maximum of six consecutive calibration runs | | Above pattern can be continued up to a maximum of six consecutive calibration runs. | |
| Allowable for Calibration Runs | | Allowable for Calibration Runs | | Allowable for Calibration Runs | |
| Three consecutive runs, within a range of 0.020 %, out of a maximum of six consecutive calibration runs | | Three consecutive runs, within a range of 0.020 %, out of a maximum of six consecutive calibration runs | | Three consecutive runs, within a range of 0.020 %, out of a maximum of six consecutive calibration runs | |
| Allowable for Each MMF | | Allowable for Each MMF | | Allowable for Each MMF | |
| Five consecutive runs, within a range of 0.020 %, out of a maximum of ten consecutive proving runs | | Five consecutive runs, within a range of 0.020 %, out of a maximum of ten consecutive proving runs | | Seven consecutive runs, within a range of 0.020 %, out of a maximum of 14 consecutive proving runs | |
| MMF1 shall be within 0.020 % of MMF2 | | MMF1 shall be within 0.020 % of MMF2 | | MMF1 shall be within 0.020 % of MMF2 | |
| | | MMF2 shall be within 0.020 % of MMF3 | | MMF2 shall be within 0.020 % of MMF3 | |
| | | MMF3 shall be within 0.020 % of MMF4 | | | |
| Calibration Run Set II | | Calibration Run Set II | | Calibration Run Set II | |
| Conduct the same as calibration run set I except at different flow rate | | Conduct the same as calibration run set I except at different flow rate | | Conduct the same as calibration run set I except at different flow rate | |
| Calibration Run Set III | | Calibration Run Set III | | Calibration Run Set III | |
| Conduct the same as calibration run set II except at different flow rate | | Conduct the same as calibration run set II except at different flow rate | | Conduct the same as calibration run set II except at different flow rate | |

Figure 3 – Master Meter Methods for Prover Calibration

14.4 CPV_{SET} Stability Parameters

Analysis of the stability in each CPV_{SET} will assist in analyzing the prover calibration system

performance (master meter, master prover), presence of a homogeneous and stable base density (ρ_B), stable fluid properties (T_P , P_P), stable flow conditions (Q), and the prover's physical condition.

The following parameters demonstrate stability in a CPV_{SET} determination:

- ΔMMF_{SET} Variation of calibration system performance over a CPV_{SET}
- $\Delta \rho_{B_SET}$ Variation of ρ_B over a CPV_{SET}
- ΔT_{FP_SET} Variation of T_{FP} over a CPV_{SET}
- ΔP_{FP_SET} Variation of P_{FP} over a CPV_{SET}
- ΔQ_{MM_SET} Variation of Q_{MM} over a CPV_{SET}

15. Standard Method for Calibrating a Prover Using Master Meter

The Standard Method specifies the calibration of the Master Meter *at the START and STOP of each Calibration Set* (MMF_{START} , MMF_{STOP}). This will result in six (6) MMF determinations and three (3) MMF_{SET} values to determine the Base Prover Volume (BPV).

The calibration sequence is shown in the Process Maps (Figures 6 or 7).

The flowrate for a Calibration Set is established and the system shall exhibit a homogeneous, stable flow regime (temperature, flowrate, base density).

At the 'START' of a Calibration Set, the master meter is calibrated using the master prover to generate a MMF_{START} proving report.

A Calibration Run of the field prover is performed using the master meter as a transfer standard.

An Initial Calibrated Prover Volume ($ICPV_{RUN}$) is determined for each Calibration Run using the following equations:

$$GSV_M = MMF_{START} \times IV_M \times CTL_M \times CPL_M \quad (3)$$

$$ICPV_{RUN} = \frac{GSV_M}{(CTS_P \times CPS_P \times CTL_P \times CPL_P)} \quad (4)$$

A 'STOP' of the Calibration Set is initiated when a minimum of three (3) consecutive Calibration Runs out of a maximum of six (6) consecutive Calibration Runs demonstrate a $ICPV_{RUN}$ repeatability tolerance, $r_{\Delta ICPV} \leq 0.020 \%$.

The master meter is calibrated using the master prover to generate a MMF_{STOP} proving report.

The Master Meter shall demonstrate a reproducibility tolerance, ΔMMF (r%) $\leq 0.020 \%$, between the MMF_{START} and MMF_{STOP} values, for each CPV_{SET} .

If employing a Spot Sampling Method for calibration of a field prover,

$$\rho_{B_SET} = \frac{(\rho_{B_START} + \rho_{B_STOP})}{2} \quad (5)$$

If employing a continuous Sampling Method (online densitometer),

$$\rho_{B_SET} = \frac{\Sigma^3(\rho_{B_RUN} \text{ of three consecutive selected runs in a Set })}{3} \quad (6)$$

A Calibrated Prover Volume for each Run (CPV_{RUN}) is determined using the following equations:

$$MMF_{SET} = \frac{(MMF_{START} + MMF_{STOP})}{2} \quad (7)$$

$$CTL \sim f(\rho_{B_SET}, T) \quad (8)$$

$$F \sim f(\rho_{B_SET}, T) \quad (9)$$

$$CPL \sim f(F, P) \quad (10)$$

$$GSV_M = MMF_{SET} \times IV_M \times CTL_M \times CPL_M \quad (11)$$

$$CPV_{RUN} = \frac{GSV_M}{(CTS_P \times CPS_P \times CTL_P \times CPL_P)} \quad (12)$$

The Fixed Range Method criteria stated in API *MPMS* Chapter 4.9.3, requires a repeatability tolerance, $r_{\Delta CPV_{RUN}} \leq 0.020\%$ for three (3) consecutive calibration runs out of a maximum of six (6) consecutive calibration runs in each Calibration Set at a constant flowrate.

The Fixed Range Method criteria stated in API *MPMS* Chapter 4.9.3, requires a reproducibility tolerance, $R_{\Delta CPV_{SET}} \leq 0.020\%$, for three (3) consecutive Calibration Sets over the three (3) different flowrates.

16. Alternate Method “A” for Calibrating a Prover Using Master Meter

Alternate Method “A” specifies the calibration of the Master Meter *at the START and STOP of each Calibration Run* (MMF_{START} , MMF_{STOP}). This will result in four (4) to seven (7) MMF determinations for each Calibration Set and three (3) MMF_{SET} values to determine the Base Prover Volume (BPV).

The calibration and calculation sequences are shown in the Process Maps (Figures 8 or 9).

The flowrate for a Calibration Set is established and the system shall exhibit a homogeneous, stable flow regime (temperature, flowrate, base density).

At the 'START' of each Calibration Run, the master meter is calibrated using the master prover to generate a MMF_{START} proving report.

A Calibration Run of the field prover is performed using the master meter as a transfer standard.

At the 'STOP' of each Calibration Run, the master meter is calibrated using the master prover to generate a MMF_{STOP} proving report. The MMF_{STOP} value is the MMF_{START} value for the next consecutive Run in a Calibration Set.

The Master Meter shall demonstrate a reproducibility tolerance, $\Delta MMF (r\%) \leq 0.020 \%$, between the MMF_{START} and MMF_{STOP} values, for each CPV_{RUN} .

A Calibrated Prover Volume for each Run (CPV_{RUN}) is determined using the following equations:

$$MMF_{RUN} = \frac{(MMF_{START} + MMF_{STOP})}{2} \quad (13)$$

$$\rho_{B_RUN} = \frac{(\rho_{B_START} + \rho_{B_STOP})}{2} \quad (14)$$

$$CTL \sim f(\rho_{B_RUN}, T) \quad (15)$$

$$F \sim f(\rho_{B_RUN}, T) \quad (16)$$

$$CPL \sim f(F, P) \quad (17)$$

$$GSV_M = MMF_{RUN} \times IV_M \times CTL_M \times CPL_M \quad (18)$$

$$CPV_{RUN} = \frac{GSV_M}{(CTS_P \times CPS_P \times CTL_P \times CPL_P)} \quad (19)$$

A 'STOP' of the Calibration Set is initiated when a minimum of three (3) consecutive Calibration Runs out of a maximum of six (6) consecutive Calibration Runs demonstrate a CPV_{RUN} repeatability tolerance, $\Delta CPV(r\%) \leq 0.020 \%$.

The Fixed Range Method criteria stated in API *MPMS* Chapter 4.9.3, requires a repeatability tolerance, $r_{\Delta CPV_{RUN}} \leq 0.020 \%$ for three (3) consecutive calibration runs out of a maximum of six (6) consecutive calibration runs in each Calibration Set at a constant flowrate.

The Fixed Range Method criteria stated in API *MPMS* Chapter 4.9.3, requires a reproducibility tolerance, $R_{\Delta CPV_{SET}} \leq 0.020 \%$, for three (3) consecutive Calibration Sets over the three (3) different flowrates.

17. Alternate Method “B” for Calibrating a Prover Using Master Meter

The Alternate Method “B” specifies a single calibration of the Master Meter simultaneously *at the START of each Calibration Run* (MMF_{RUN}). This will result in three (3) to six (6) MMF determinations for each Calibration Set and three (3) MMF_{SET} values to determine the Base Prover Volume (BPV).

The calibration and calculation sequences are shown in the Process Maps (Figures 10 or 11).

The flowrate for a Calibration Set is established and the system shall exhibit a homogeneous, stable flow regime (temperature, flowrate, base density) prior to initiating a MMF proving report.

At the ‘START’ of each Calibration Run, the master meter is calibrated using the master prover to generate a MMF_{START} proving report.

A Calibration Run of the field prover is performed using the master meter as a transfer standard.

A Calibrated Prover Volume for each Calibration Run (CPV_{RUN}) is determined using the following equations:

$$GSV_M = MMF_{START} \times IV_M \times CTL_M \times CPL_M \quad (20)$$

$$CPV_{RUN} = \frac{GSV_M}{(CTS_p \times CPS_p \times CTL_p \times CPL_p)} \quad (21)$$

The Master Meter shall demonstrate a reproducibility tolerance, $\Delta MMF (r\%) \leq 0.020 \%$, between the MMF_{START} values for each consecutive pair of Calibration Runs.

A ‘STOP’ of the Calibration Set is initiated when a minimum of three (3) consecutive Calibration Runs out of a maximum of six (6) consecutive Calibration Runs demonstrate a CPV_{RUN} repeatability tolerance, $r_{\Delta CPV} \leq 0.020 \%$.

The Fixed Range Method criteria stated in API *MPMS* Chapter 4.9.3, requires a repeatability tolerance, $r_{\Delta CPV_{RUN}} \leq 0.020 \%$ for three (3) consecutive calibration runs out of a maximum of six (6) consecutive calibration runs in each Calibration Set at a constant flowrate.

The Fixed Range Method criteria stated in API *MPMS* Chapter 4.9.3, requires a reproducibility tolerance, $R_{\Delta CPV_{SET}} \leq 0.020 \%$, for three (3) consecutive Calibration Sets over the three (3) different flowrates.

18. Average Calibrated Prover Volume for Sets (CPV_{SET})

When the Prover Calibration Criteria have been satisfied for the selected calibration method (Standard, Alternate “A”, Alternate “B”), the Average CPV_{SET} is calculated as follows:

$$\text{Average } CPV_{SET} = \frac{(CPV_{SET_I} + CPV_{SET_{II}} + CPV_{SET_{III}})}{3} \quad (22)$$

To convert the Average CPV_{SET} to various BPV to units at base (reference or standard) conditions as shown in Figure 13.

19. Process Maps

Eight (8) Process Maps have been prepared to assist the user of this standard to fully comprehend the complexity associated with the calculations:

- Master Proving Report Using Online Densitometer (Figure 4)
- Master Meter Proving Report Using Spot Sample (Figure 5)
- Standard Method for Displacement Prover Using Online Densitometer (Figure 6)
- Standard Method for Displacement Prover Using Spot Sample (Figure 7)
- Alternate A Method for Displacement Prover Using Densitometer (Figure 8)
- Alternate A Method for Displacement Prover Using Spot Sample (Figure 9)
- Alternate B Method for Displacement Prover Using Online Densitometer (Figure 10)
- Alternate B Method for Displacement Prover Using Spot Sample (Figure 11)
- Expanded Discrimination of Master Prover's BPV (Figure 12)
- Conversion of Average CPV_{SET} to BPV (Figure 13)

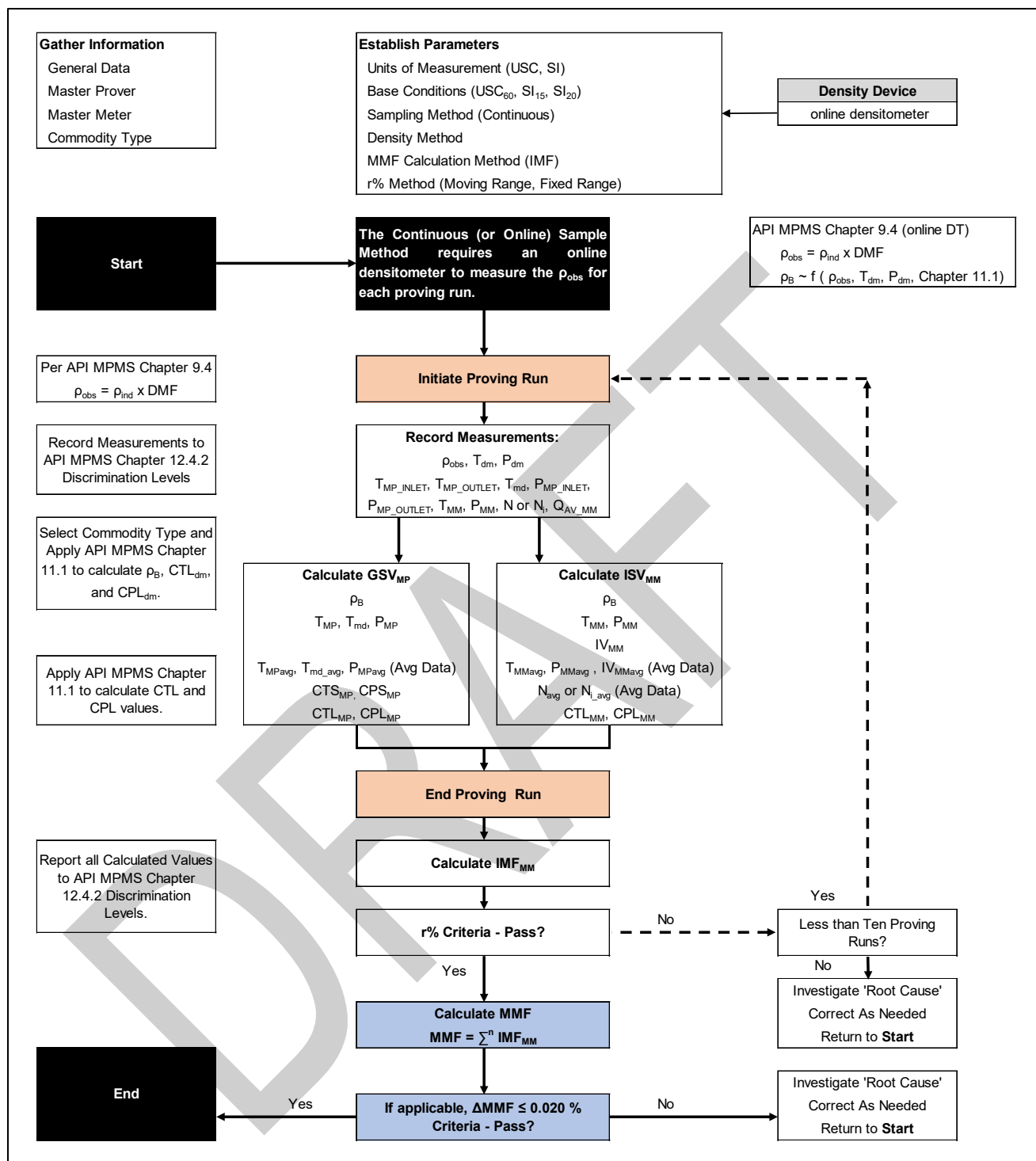


Figure 4 – Master Meter Proving Using Online Densitometer

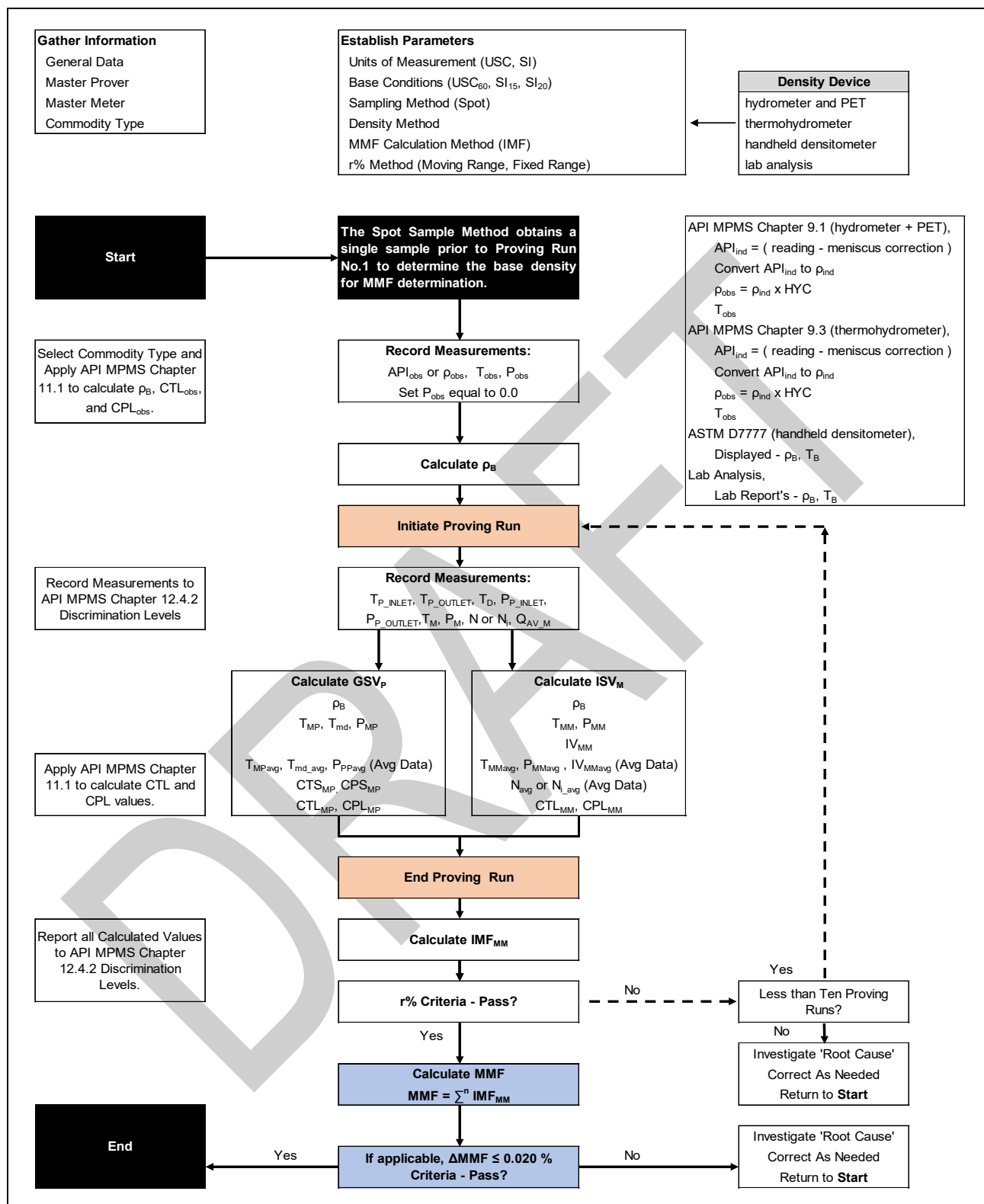


Figure 5 – Master Meter Proving Using Spot Sample

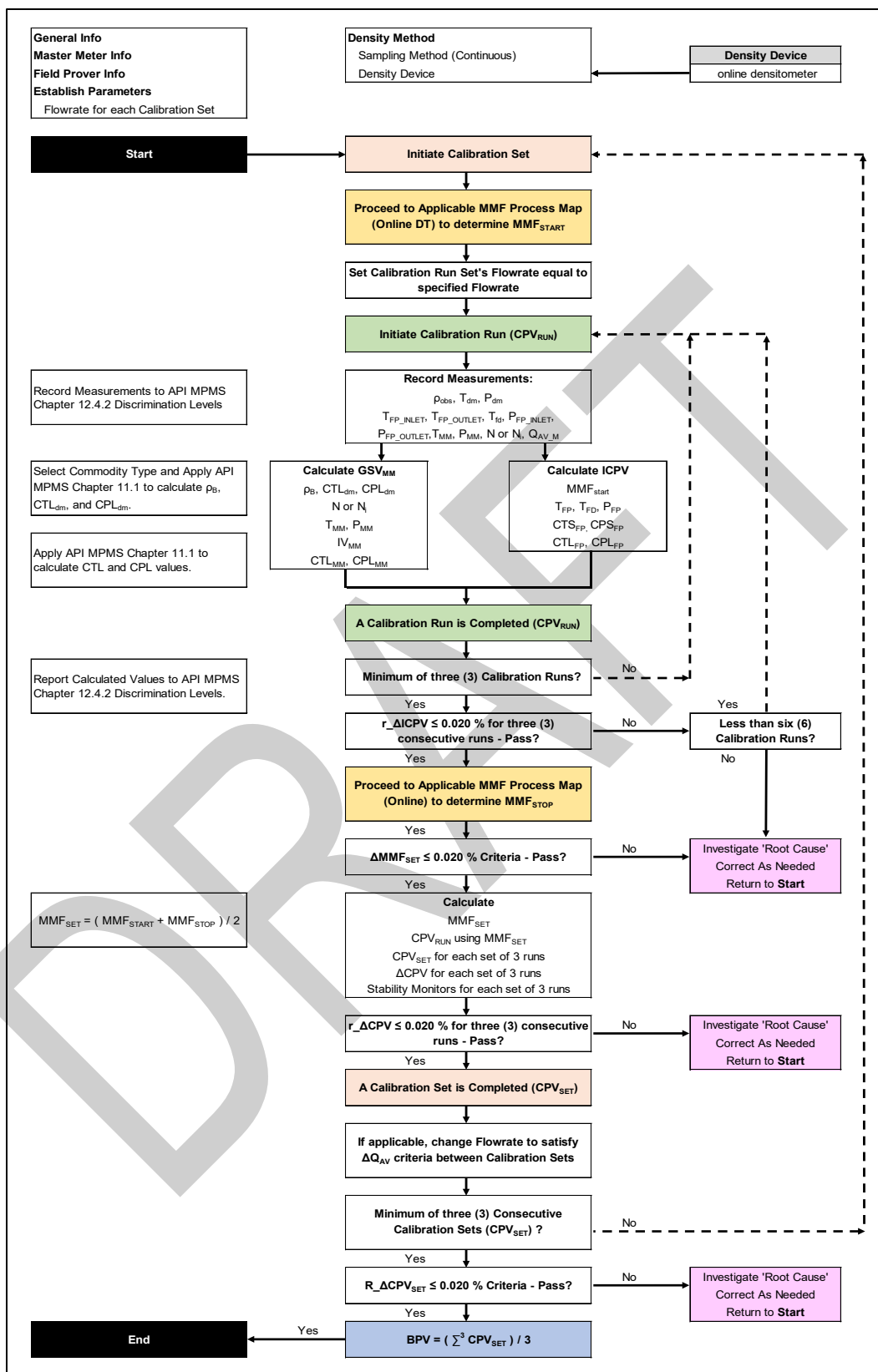


Figure 6 – Standard Method for Displacement Prover Using Online Densitometer

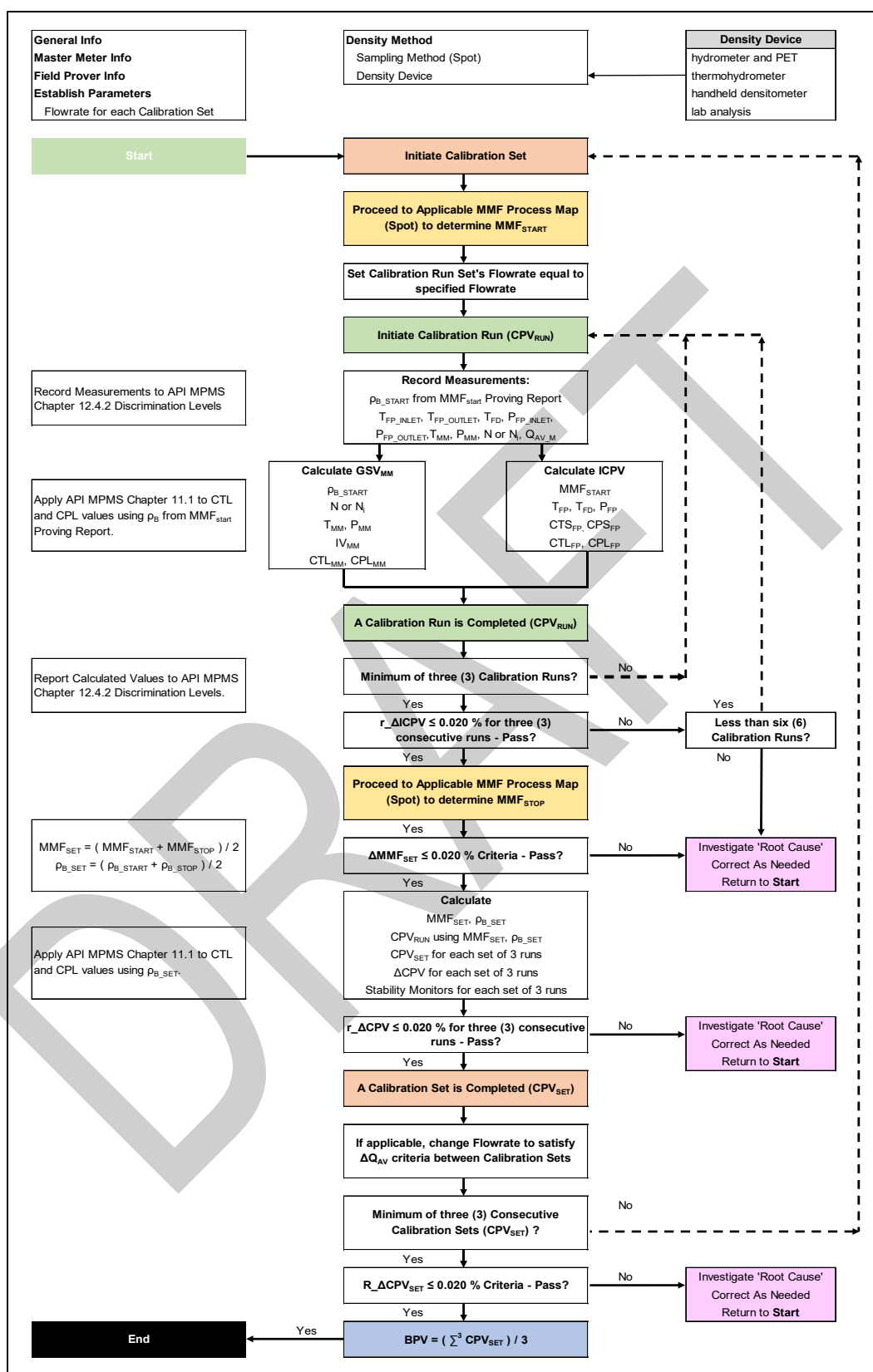


Figure 7 – Standard Method for Displacement Prover Using Spot Sample

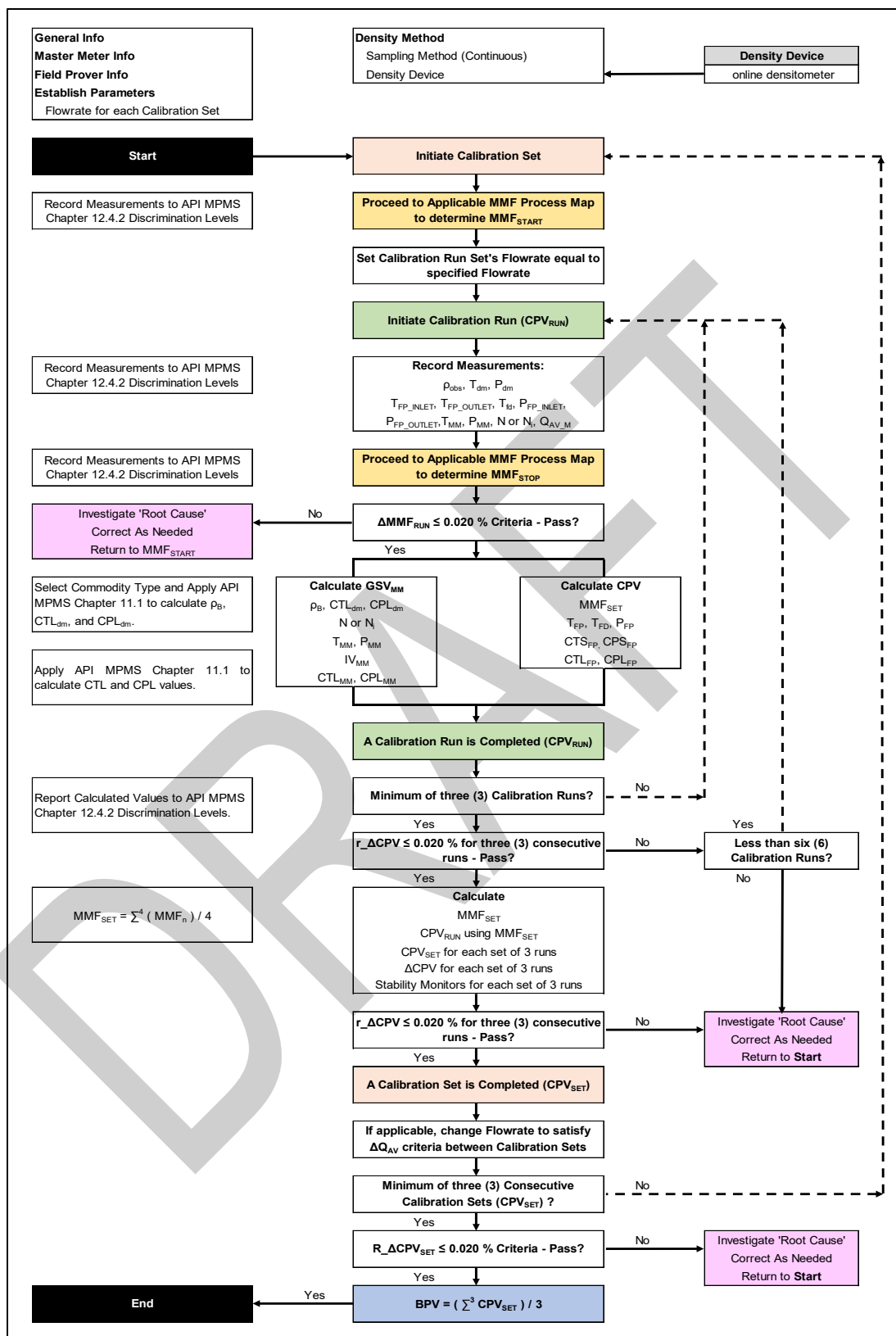


Figure 8 – Alternate Method “A” for Displacement Prover Using Online Densitometer

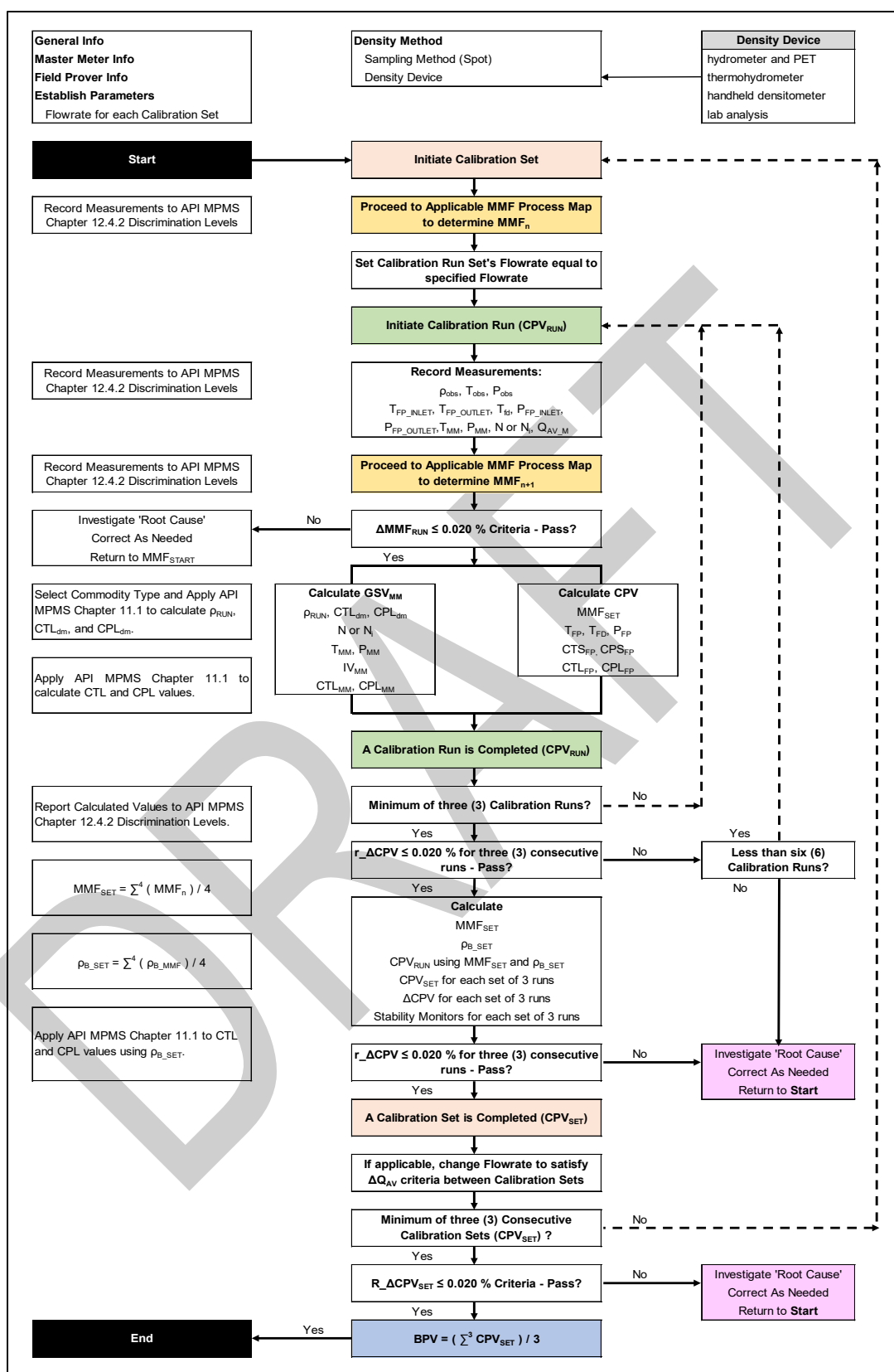


Figure 9 – Alternate Method “A” for Displacement Prover Using Spot Sample

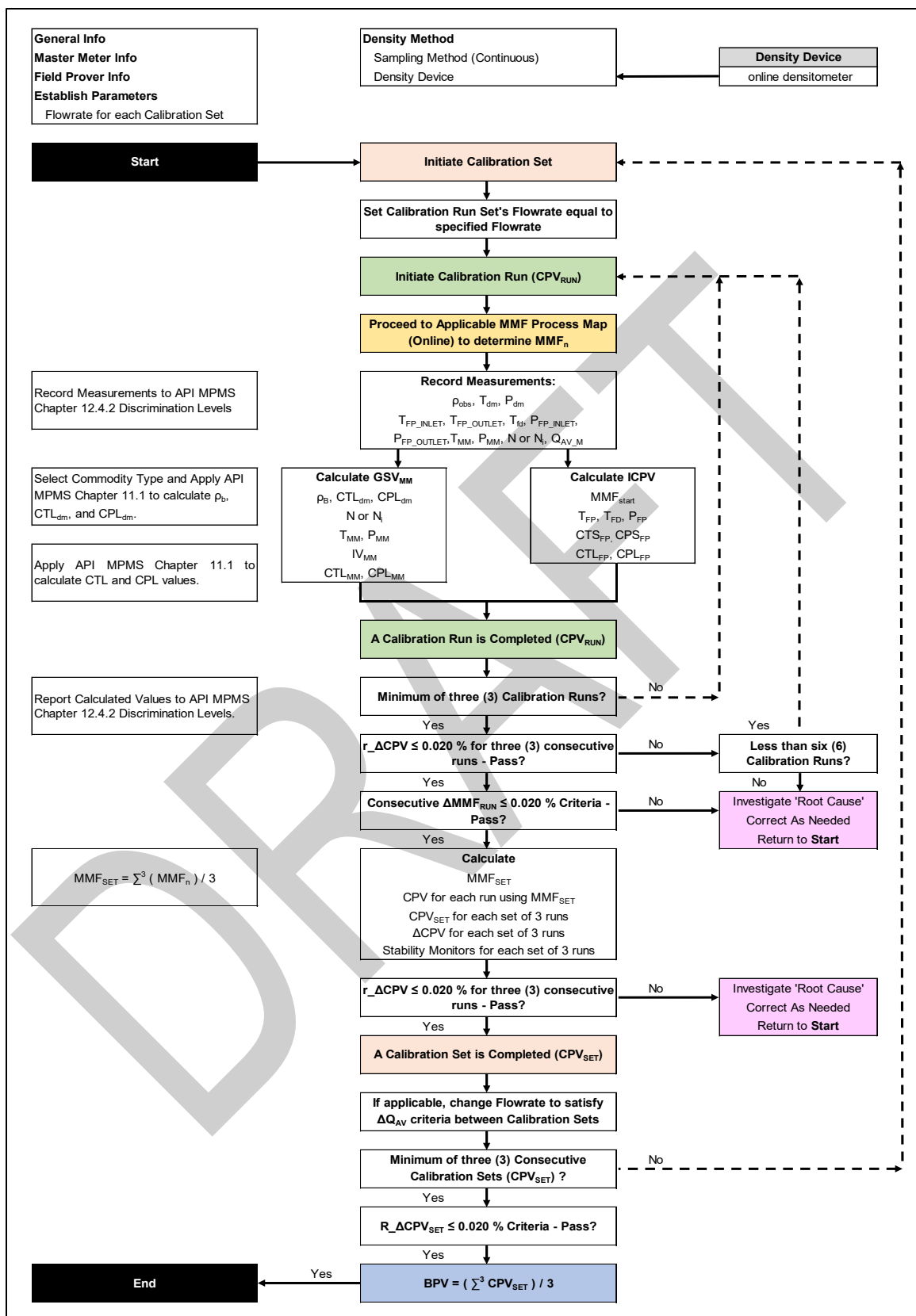


Figure 10 – Alternate Method “B” for Displacement Prover Using Online Densitometer

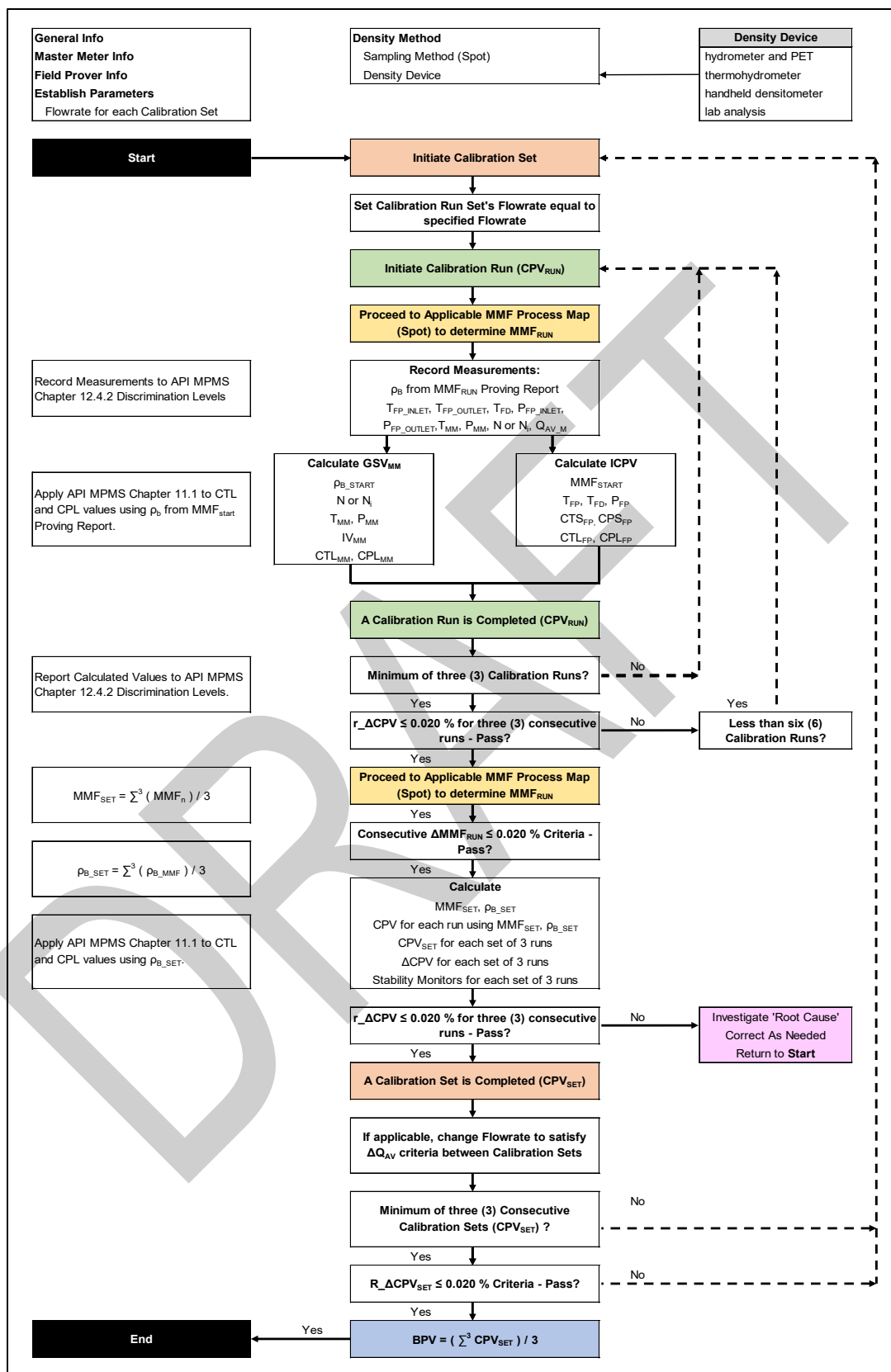


Figure 11 – Alternate Method “B” for Displacement Prover Using Spot Sample

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| Field Prover | |
|--|--|
| Measurement Units | 0 (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) |
| Detector Design | 0 (0-Internal, 1-External) |
| Wall Material | 1 (1-CS, 2-304SS, 3-316SS, 4-17-4PH) |
| Rod Material | 0 (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) |
| Source for GL _{MP} , GL _{md} , E _{MP} | 1 (0-Prover Manufacturer, 1-API Table) |
| BPV _P | 30,030.795 3 cubic inches at 60.0 °F, 0.0 psig |

| Base Prover Volume (BPV) | | | |
|--------------------------|------------------------------------|-----------------------------------|-----------------------------------|
| | BPV ₆₀ Barrels | BPV ₁₅ Cubic Meters | BPV ₂₀ Cubic Meters |
| | 3.095 320 068 027 | 0.492 107 411 000 | 0.492 189 795 000 |
| Decimals | 9 | 10 | 10 |
| Conversion | in ³ / Bbl 9.702E+03 | mL / M ³ 1.00E+06 | mL / M ³ 1.00E+06 |
| Rnd'd BPV | 3.095 320 068 000 | 0.492 107 411 000 | 0.492 189 795 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to **10 digits** (the appropriate decimal place) to increase the precision of the Master Prover's BPV, not the uncertainty of the Master Prover's BPV.

| | T _B | |
|---------------------------|----------------|-----------------------------------|
| Decimal Base CTS | 60.0 | °F |
| Decimal BPV ₆₀ | 9 | - |
| Decimal BPV _{SI} | 4 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV | 3 | mL at 15.0 °C and 0.0 kPag |
| Decimal BPV | 9 | Barrels |
| Decimal BPV | 10 | Cubic Meters |

Detector Design,

CTS_P = [1 + (T_P - T_B) x GL_P]³, for detectors mounted in calibrated section

CTS_P = [1 + (T_P - T_B) x GL_P]² x [1 + (T_D - T_B) x GL_d], for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F

BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig

BPV₁₅ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C

BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig

BPV₁₅ = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = ROUND(BPV₁₅ x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C

BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig

BPV₁₅ = ROUND(BPV₂₀ x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| | per °F | per °C | per °C |
|---|---------------|---------------|---------------|
| GL _P | 0.000 006 20 | 0.000 011 16 | 0.000 011 16 |
| GL _D | NA | NA | NA |
| Base Temperature (T_B) | | | |
| | 60.0 | 15.0 | 20.0 |
| Base CTS ₆₀ | 1.000 000 000 | 1.000 018 600 | 0.999 851 207 |
| Base CTS ₁₅ | 0.999 981 400 | 1.000 000 000 | 0.999 832 609 |
| Base CTS ₂₀ | 1.000 148 807 | 1.000 167 409 | 1.000 000 000 |

| Base Unit Volume | |
|-------------------|--|
| BPV ₆₀ | 30,030.795 3 cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 492,107.411 mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 492,189.795 mL at 20.0 °C and 0.0 kPag |

| API Properties | | |
|---|------------------------------------|---------------------------------------|
| Linear Coefficient of Thermal Expansion, GL | | |
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,3,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar™ | 0.000 001 44 | 0.000 000 80 |

Notes:

(1) The User/Owner should obtain GL values from the prover manufacturer.

(2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.

(3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.

(4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.

(5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Figure 12 – Expanded Discrimination of Master Prover's BPV

Step 1

Average CPV_{SET} = [$\sum^3 (CPV_{SET})$] / 3

0.000 000 000 0

Bbls or M³

rounded to 9 digits

Detector Design,
CTS = [1 + (T_P - T_B) x GL_P]³, for detectors mounted in calibrated section
CTS = [1 + (T_P - T_B) x GL_P]² x [1 + (T_D - T_B) x GL_D], for detectors mounted on external shaft

All CTS values are rounded to nine (9) decimal places.

Step 2
If Average CPV_{SET} is in Bbls and T_B is 60.0 °F, Proceed to Step 2A.
If Average CPV_{SET} is in M³ and T_B is 15.0 °C, Proceed to Step 2B.
If Average CPV_{SET} is in M³ and T_B is 20.0 °C, Proceed to Step 2C.

Step 2A **If Average CPV_{SET} is in Bbls and T_B is 60.0 °F**
BPV₆₀ = ROUND(Average CPV_{SET} x 9,702 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
BPV₁₅ = ROUND(Average CPV_{SET} x 9,702 x 16.387 064 x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
BPV₂₀ = ROUND(Average CPV_{SET} x 9,702 x 16.387 064 x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

Step 2B **If Average CPV_{SET} is in M³ and T_B is 15.0 °C**
BPV₆₀ = ROUND(Average CPV_{SET} x 1.0E+06 / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
BPV₁₅ = ROUND(Average CPV_{SET} x 1.0E+06 x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
BPV₂₀ = ROUND(Average CPV_{SET} x 1.0E+06 x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

Step 2C **If Average CPV_{SET} is in M³ and T_B is 20.0 °C**
BPV₆₀ = ROUND(Average CPV_{SET} x 1.0E+06 / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
BPV₁₅ = ROUND(Average CPV_{SET} x 1.0E+06 x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
BPV₂₀ = ROUND(Average CPV_{SET} x 1.0E+06 x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

Step 3 **Convert BPV values (in³, mL) using following equations and round the results to six (6) significant digits.**

BPV₆₀

Bbl = (in³ at 60.0 °F and 0.0 psig) / 9.702E+03
U.S. Gallons = (in³ at 60.0 °F and 0.0 psig) / 2.31E+02
Cubic Feet = (in³ at 60.0 °F and 0.0 psig) / 1.728E+03

BPV₁₅

M³ = (mL at 15.0 °C and 0.0 kPag) x 1E-06
L = (mL at 15.0 °C and 0.0 kPag) x 1E-03

BPV₂₀

M³ = (mL at 20.0 °C and 0.0 kPag) x 1E-06
L = (mL at 20.0 °C and 0.0 kPag) x 1E-03

Example

Average CPV_{SET}

11.903 072 600 0

Bbls at 60 degF

rounded to 9 digits

BPV₆₀

115,483.610 4

in³ at 60.0 °F and 0.0 psig

4 decimal places per Ch 12.4

BPV₁₅

1,892,402.115

mL at 15.0 °C and 0.0 kPag

3 decimal places per Ch 12.4

BPV₂₀

1,892,718.922

mL at 20.0 °C and 0.0 kPag

3 decimal places per Ch 12.4

| Decimal Places | Base Prover Volume (BPV) | | | | | | |
|----------------|--------------------------|--------------|------------|-------------------|--------------|-------------------|--------------|
| | BPV ₆₀ | | | BPV ₁₅ | | BPV ₂₀ | |
| | Barrels | U.S. Gallons | Cubic Feet | Liters | Cubic Meters | Liters | Cubic Meters |
| 1 | - | - | - | - | - | - | - |
| 2 | - | - | - | - | 1,892.40 | - | 1,892.72 |
| 3 | - | 499.929 | - | - | - | - | - |
| 4 | 11.903 1 | - | 66.830 8 | - | - | - | - |
| 5 | - | - | - | 1.892 40 | - | 1.892 72 | - |
| 6 | - | - | - | - | - | - | - |
| 7 | - | - | - | - | - | - | - |

Note: The BPV Volumes shown above are specified based on 6 significant digits (10 ppm, or, 0.001%).

Figure 13 - Conversion of Average CPV_{SET} to BPV

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20. Examples¹

Four (4) examples using the Standard Method for displacement provers have been prepared to clarify the process: two (2) in SI Units (see Annex A) and two (2) in USC units (see Annex B).

The presented examples depict the required proper calculations and documentation.

| Transfer Standard | | | | | | | | | | | | | | | |
|-------------------|-----|----------|------|---------------|----------|-------------|--------------|----|--------------|-------------|-----------|----------|--------------|----------|-------------|
| Units | | Sampling | | Master Prover | | | Master Meter | | MF (r %) | | MF Method | | Field Prover | | |
| SI | USC | Online | Spot | Bidi Free | Uni Free | Uni Captive | Turbine | PD | Moving Range | Fixed Range | IMF | Avg Data | Bidi Free | Uni Free | Uni Captive |
| X | - | X | - | X | - | - | - | X | X | - | X | - | X | - | - |
| X | - | - | X | - | - | X | X | - | - | X | X | - | - | - | X |
| - | X | X | - | - | - | X | X | - | X | - | X | - | X | - | - |
| - | X | - | X | X | - | - | - | X | - | X | X | - | - | - | X |

From API Chapter 12.2 Section 12.2.1, page 24, wrt Proving Reports -

"Historically, the Average Data Method has been used since it only requires a single calculation at the end to determine the Meter Factor. *The Intermediate Factor Method (IMF) is the preferred method* as variations in temperature and pressure are accounted for in the evaluation of the proving results."

| Four (4) BPV Examples for Displacement Prover | |
|---|--|
| 1 | SI Units, Continuous Sampling, Master Prover - Bidirectional Free Displacer, Master Meter - PD, MF r% - Fixed Range, MF Method - IMF, Field Prover - Bidirectional Free Displacer |
| 2 | SI Units, Spot Sampling, Master Prover - Unidirectional Captive Displacer, Master Meter - Turbine, MF r% - Moving Range, MF Method - IMF, Field Prover - Unidirectional Captive Displacer |
| 3 | USC Units, Continuous Sampling, Master Prover - Bidirectional Free Displacer, Master Meter - PD, MF r% - Fixed Range, MF Method - IMF, Field Prover - Bidirectional Free Displacer |
| 4 | USC Units, Spot Sampling, Master Prover - Unidirectional Captive Displacer, Master Meter - Turbine, MF r% - Moving Range, MF Method - IMF, Field Prover - Unidirectional Captive Displacer |

Figure 14 – Standard Method Examples

Examples have not been presented using Alternate Method "A", Alternate Method "B", or when using an Open Tank Prover as a Master Prover.

¹ The following examples are for illustration purposes only. Each company should develop its own approach. They are not to be considered exclusive or exhaustive in nature. API makes no warranties, express or implied, for reliance on or any omissions from the information contained in this document.

Annex A (informative) **SI Unit Examples²**

Example A.1 – Standard Method

SI Units, Continuous Sampling, Master Prover - Bidirectional Free Displacer, Master Meter - PD, MF
r% - Fixed Range, MF Method - IMF, Field Prover - Bidirectional Free Displacer

² The following examples are for illustration purposes only. Each company should develop its own approach. They are not to be considered exclusive or exhaustive in nature. API makes no warranties, express or implied, for reliance on or any omissions from the information contained in this document.

| Master Prover | |
|-------------------|--|
| Measurement Units | 1 (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) |
| Detector Design | 0 (0-Internal, 1-External) |
| Wall Material | 1 (1-CS, 2-304SS, 3-316SS, 4-17-4PH) |
| Rod Material | 0 (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) |
| Certificate BPV | 492,107.411 0 mL at 15.0 °C and 0.0 kPag |

| Base Prover Volume (BPV) | | | |
|--------------------------|------------------------------------|-----------------------------------|-----------------------------------|
| | BPV ₆₀ Barrels | BPV ₁₅ Cubic Meters | BPV ₂₀ Cubic Meters |
| | 3.095 320 068 027 | 0.492 107 411 000 | 0.492 189 794 000 |
| Decimals | 9 | 10 | 10 |
| Conversion | in ³ / Bbl 9.702E+03 | mL / M ³ 1.00E+06 | mL / M ³ 1.00E+06 |
| Rnd'd BPV | 3.095 320 068 000 | 0.492 107 411 000 | 0.492 189 794 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to 10 digits (the appropriate decimal place) to increase the precision of the Master Prover's BPV, not the uncertainty of the Master Prover's BPV.

| | T _B | |
|---------------------------|----------------|-----------------------------------|
| Decimal Base CTS | 15.0 | °C |
| Decimal BPV ₆₀ | 9 | - |
| Decimal BPV _{SI} | 4 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV | 3 | mL at 15.0 °C and 0.0 kPag |
| | 10 | Cubic Meters |

Detector Design,
 $CTS_P = [1 + (T_P - T_B) \times GL_P]^3$, for detectors mounted in calibrated section
 $CTS_P = [1 + (T_P - T_B) \times GL_P]^2 \times [1 + (T_D - T_B) \times GL_D]$, for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F
BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig
BPV₁₅ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
BPV₂₀ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C
BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
BPV₁₅ = mL at 15.0 °C, 0.0 kPag
BPV₂₀ = ROUND(BPV₁₅ x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C
BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
BPV₁₅ = ROUND(BPV₂₀ x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| T _B | 60.0 °F | 15.0 °C | 20.0 °C |
|-----------------|--------------|--------------|--------------|
| GL _P | 0.000 006 20 | 0.000 011 16 | 0.000 011 16 |
| GL _D | NA | NA | NA |

| | Base CTS ₆₀ | Base CTS ₁₅ | Base CTS ₂₀ |
|--|------------------------|------------------------|------------------------|
| | 1.000 000 000 | 1.000 018 600 | 0.999 851 207 |
| | 0.999 981 400 | 1.000 000 000 | 0.999 832 609 |
| | 1.000 148 807 | 1.000 167 409 | 1.000 000 000 |

| | Base Unit Volume | |
|-------------------|------------------|-----------------------------------|
| BPV ₆₀ | 30,030.795 3 | cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 492,107.411 | mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 492,189.794 | mL at 20.0 °C and 0.0 kPag |

in³ = mL / 16.387 064
U.S. Gallons = in³ / 2.31E+02
Bbl = in³ / 9.702E+03
Cubic Feet = in³ / 1.728E+03

mL = M³ x 1E+06
mL = in³ x 16.387 064

M³ = mL x 1E-06
L = mL x 1E-03

| API Properties | | |
|---|------------------------------------|---------------------------------------|
| Linear Coefficient of Thermal Expansion, GL | | |
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,3,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar TM | 0.000 001 44 | 0.000 000 80 |

Notes:
(1) The User/Owner should obtain GL values from the prover manufacturer.
(2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.
(3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.
(4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.
(5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Example A.1 - Expanded Discrimination of Master Prover's BPV

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| Washington, D.C., USA | | | | | | | | | |
|---|-------------------------------|-----------------|----------------------------|-----------------------|-----------------------|---|--------------------|---------------------|-------------------|
| Master Meter Proving Report | | | | | | | | | |
| General Data | | | Displacement Prover | | | Report Summary | | | |
| Operator | API Midstream | | Manufacturer | API | | Report No. | Start | Stop | |
| Station Name | MPMS | | Prover Type | Displacement | | Date | Start I | Stop I | |
| Ch 11.1 | Tables 5B/6B | | Flow Design | Bidirectional | | Time | 14-Feb-24 | 14-Feb-24 | |
| T _B | 15.0 °C | | Wall Design | Single | | Totalizer | 8:21:18 | 11:21:18 | |
| P _B | 0.0 kPag | | Detector | Internal | | Fluid, Batch No. | 2,342,501.020 | 2,343,601.020 | M3 |
| Master Meter | | | Displacer | Free Sphere | | API ₆₀ | Products | Products | |
| Flowmeter ID | 200 | | Wall Material | Carbon Steel | | ρ ₆₀ | 60.8 | 60.6 | °API |
| Manufacturer | PD | | Rod Material | NA | | API ₁₅ | 735.210 | 735.710 | kg/m ³ |
| Model | 0 | | GL _P | 0.000 011 16 per °C | | API ₁₅ | 60.7 | 60.5 | °API |
| Nominal Size | 100 mm | | GL _D | NA per °C | | ρ ₁₅ | 735.715 | 736.216 | kg/m ³ |
| Type | PD | | E _P | 206 842 710 per kPag | | API ₂₀ | 61.7 | 61.5 | °API |
| Proving Result | MMF | | ID _P | 202.717 4 mm | | ρ ₂₀ | 731.158 | 731.660 | kg/m ³ |
| T _F Comp | No | | WT _P | 8.178 8 mm | | Flowrate, Q | 111.350 | 111.350 | MPH |
| P _F Comp | No | | Calibration Date | 2021-09-04 | | T _{P,AVG} | 22.830 | 22.829 | °C |
| NKF | 52,834.410 5 P / M3 | | Serial No. | 8904-01 | | P _{P,AVG} | 1176.0 | 1210.0 | kPag |
| Cartridge No. | API-0011 | | Certificate No. | 10101010 | | Trips per Run | 1 | 1 | |
| Density Method | | | Switches | 9201 to 9202 | | Roundtrips | Runs 1-5 | Runs 1-5 | |
| Sample Method | Continuous | | BPV | 0.492 107 411 0 M3 | | Repeatability (r) | 0.018 | 0.017 | % |
| ρ _{obs} Device | Densitometer | | Spot Sample | | | Allowable (r) | 0.020 | 0.020 | % |
| DMF | 0.999 8 | | API _{ind} | °API | | (r) Pass/Fail | Pass | Pass | |
| HYC Factor | NA | | ρ _{ind} | kg/m ³ | | MMF | 0.999 900 0 | 0.999 904 0 | |
| API MPMS Chapter 12.4.2 Measurement Units - SI_15 Sampling Method - Continuous (or Online) Meter Factor Method - Intermediate (or IMF) Repeatability Method (r%) - Fixed, 5 out of 5 Runs API MPMS Chapter 11.1 - Tables 5B/6B | | | T _{obs} | °C | | ΔMMF | NA | 0.000 | % |
| | | | P _{obs} | kPag | | Allowable ± ΔMMF | NA | 0.020 | % |
| | | | | | ΔMMF Pass/Fail | NA | Pass | | |
| | | | | | Prior vs Current | ΔQ | 0.0 | % | |
| | | | ΔT _P | (0.001) | °C | | | | |
| Base Density | Roundtrip Measurements | | | | | | | Base Density | |
| API _B | ρ _{ind} | T _{dm} | P _{dm} | T _{P,INLET} | T _{P,OUTLET} | T _M | T _D | ρ _B | Run |
| °API | kg/m ³ | °C | kPag | °C | °C | °C | °C | kg/m ³ | |
| 60.6 | 729.543 | 23.244 | 1,273.0 | 22.817 | 22.889 | 22.994 | | 735.817 | 1 |
| 60.5 | 729.745 | 23.739 | 1,275.0 | 22.806 | 22.844 | 22.983 | | 736.465 | 2 |
| 60.5 | 729.543 | 23.761 | 1,284.0 | 22.822 | 22.856 | 23.000 | | 736.276 | 3 |
| 60.5 | 729.545 | 23.750 | 1,281.0 | 22.811 | 22.817 | 22.972 | | 736.270 | 4 |
| 60.5 | 729.512 | 23.767 | 1,281.0 | 22.806 | 22.828 | 22.922 | | 736.252 | 5 |
| NA | | | | | | | | | 6 |
| NA | | | | | | | | | 7 |
| NA | | | | | | | | | 8 |
| NA | | | | | | | | | 9 |
| NA | | | | | | | | | 10 |
| 60.5 | 729.578 | 23.652 | 1,279.0 | NA | NA | 22.974 | NA | 736.216 | Runs 1-5 |
| Commodity Type | Roundtrip Measurements | | | | | T_P and P_P Values | | | |
| | N or N _i | Q _M | P _{P,INLET} | P _{P,OUTLET} | P _M | T _{P,RUN} | P _{P,RUN} | | Run |
| | Pulses | MPH | kPag | kPag | kPag | °C | kPag | | |
| Gasoline, Napthene | 26,020.000 | 111.308 6 | 1,227.0 | 1,194.0 | 1,196.0 | 22.853 0 | 1,210.50 | | 1 |
| Gasoline, Napthene | 26,016.000 | 111.310 2 | 1,229.0 | 1,192.0 | 1,196.0 | 22.825 0 | 1,210.50 | | 2 |
| Gasoline, Napthene | 26,018.000 | 111.330 9 | 1,222.0 | 1,196.0 | 1,193.0 | 22.839 0 | 1,209.00 | | 3 |
| Gasoline, Napthene | 26,020.000 | 111.453 3 | 1,225.0 | 1,198.0 | 1,196.0 | 22.814 0 | 1,211.50 | | 4 |
| Gasoline, Napthene | 26,018.000 | 111.329 3 | 1,222.0 | 1,193.0 | 1,198.0 | 22.817 0 | 1,207.50 | | 5 |
| NA | | | | | | | | | 6 |
| NA | | | | | | | | | 7 |
| NA | | | | | | | | | 8 |
| NA | | | | | | | | | 9 |
| NA | | | | | | | | | 10 |
| Runs 1-5 | 26,018.400 0 | 111.350 0 | NA | NA | 1,196.0 | 22.829 0 | 1,210.03 | | Runs 1-5 |

Example A.1 - Calibration Set I - Stop Proving Report - 1 of 2

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| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | |
|---|---|---------------------------|--|--|-----------------|------------------|-------------------|----------|--|--|-------|---------|------------|---------|--------|------|-----------|-----------|------|----------|----------|------------------|----------|----------|
| Master Meter Proving Report | | | | | | | | | | | | | | | | | | | | | | | | |
| API MPMS Chapter 12.4.2 Measurement Units - SI_15 Sampling Method - Continuous (or Online) Meter Factor Method - Intermediate (or IMF) Repeatability Method (r%) - Fixed, 5 out of 5 Runs API MPMS Chapter 11.1 - Tables 5B/6B | | | <div style="text-align: right; font-weight: bold;">Report Summary</div> <table style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 30%;"></th> <th style="width: 35%; text-align: center;">Prior</th> <th style="width: 35%; text-align: center;">Current</th> </tr> <tr> <td>Report No.</td> <td style="text-align: center;">Start I</td> <td style="text-align: center;">Stop I</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">14-Feb-24</td> <td style="text-align: center;">14-Feb-24</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">08:21:18</td> <td style="text-align: center;">11:21:18</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">Products</td> <td style="text-align: center;">Products</td> </tr> </table> | | | | | | | | Prior | Current | Report No. | Start I | Stop I | Date | 14-Feb-24 | 14-Feb-24 | Time | 08:21:18 | 11:21:18 | Fluid, Batch No. | Products | Products |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start I | Stop I | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | |
| Time | 08:21:18 | 11:21:18 | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Products | Products | | | | | | | | | | | | | | | | | | | | | | |
| Run | BPV M3 | CTSp | CPSp | Rnd CTLp | Rnd CPLp | Rnd CTPLp | GSVp M3 | Run | | | | | | | | | | | | | | | | |
| 1 | 0.492 107 411 0 | 1.000 262 941 | 1.000 145 053 | 0.990 262 343 | 1.001 436 834 | 0.991 685 185 | 0.488 214 755 3 | 1 | | | | | | | | | | | | | | | | |
| 2 | 0.492 107 411 0 | 1.000 262 004 | 1.000 145 053 | 0.990 309 872 | 1.001 432 007 | 0.991 728 002 | 0.488 235 377 1 | 2 | | | | | | | | | | | | | | | | |
| 3 | 0.492 107 411 0 | 1.000 262 473 | 1.000 144 873 | 0.990 288 827 | 1.001 431 681 | 0.991 706 605 | 0.488 224 983 8 | 3 | | | | | | | | | | | | | | | | |
| 4 | 0.492 107 411 0 | 1.000 261 636 | 1.000 145 173 | 0.990 319 771 | 1.001 434 377 | 0.991 740 264 | 0.488 241 291 9 | 4 | | | | | | | | | | | | | | | | |
| 5 | 0.492 107 411 0 | 1.000 261 736 | 1.000 144 693 | 0.990 315 273 | 1.001 429 798 | 0.991 731 224 | 0.488 236 656 3 | 5 | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | 8 | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | |
| Runs 1-5 | 0.492 107 411 0 | 1.000 262 158 | 1.000 144 969 | 0.990 299 217 | 1.001 432 939 | 0.991 718 256 | 0.488 230 612 9 | Runs 1-5 | | | | | | | | | | | | | | | | |
| Run | N or Ni | NKF P / M3 | IVM | Rnd CTLM | Rnd CPLM | Rnd CTPLM | ISVM M3 | Run | | | | | | | | | | | | | | | | |
| 1 | 26,020.000 | 52,834.410 5 | 0.492 482 072 8 | 0.990 086 861 | 1.001 421 227 | 0.991 494 000 | 0.488 293 019 9 | 1 | | | | | | | | | | | | | | | | |
| 2 | 26,016.000 | 52,834.410 5 | 0.492 406 364 6 | 0.990 113 931 | 1.001 416 638 | 0.991 516 564 | 0.488 229 066 7 | 2 | | | | | | | | | | | | | | | | |
| 3 | 26,018.000 | 52,834.410 5 | 0.492 444 218 7 | 0.990 088 666 | 1.001 414 532 | 0.991 489 178 | 0.488 253 113 7 | 3 | | | | | | | | | | | | | | | | |
| 4 | 26,020.000 | 52,834.410 5 | 0.492 482 072 8 | 0.990 123 062 | 1.001 417 858 | 0.991 526 916 | 0.488 309 230 8 | 4 | | | | | | | | | | | | | | | | |
| 5 | 26,018.000 | 52,834.410 5 | 0.492 444 218 7 | 0.990 184 822 | 1.001 419 787 | 0.991 590 673 | 0.488 303 094 5 | 5 | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | 8 | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | |
| Runs 1-5 | 26,018.400 0 | 52,834.410 5 | 0.492 451 789 5 | 0.990 119 468 | 1.001 418 008 | 0.991 523 466 | 0.488 277 505 1 | Runs 1-5 | | | | | | | | | | | | | | | | |
| Run | *I indicates Repeatability (r%) criteria satisfied | Repeatability (r%) | | Meter Factor Method - Intermediate (or IMF) | | IMF | | Run | | | | | | | | | | | | | | | | |
| | | Actual | Allowable | | | | | | | | | | | | | | | | | | | | | |
| NA | | NA | NA | | | | | 1 | | | | | | | | | | | | | | | | |
| NA | | NA | NA | | | | | 2 | | | | | | | | | | | | | | | | |
| NA | NA | NA | NA | | | | | 3 | | | | | | | | | | | | | | | | |
| NA | NA | NA | NA | Repeatability Method (r%) - Fixed, 5 out of 5 Runs | | | | 4 | | | | | | | | | | | | | | | | |
| Runs 1-5 | 1 | 0.017 | 0.020 | | | | | 5 | | | | | | | | | | | | | | | | |
| Runs 2-6 | | | 0.020 | | | | | 6 | | | | | | | | | | | | | | | | |
| Runs 3-7 | | | 0.020 | | | | | 7 | | | | | | | | | | | | | | | | |
| Runs 4-8 | | | 0.020 | | | | | 8 | | | | | | | | | | | | | | | | |
| Runs 5-9 | | | 0.020 | | | | | 9 | | | | | | | | | | | | | | | | |
| Runs 6-10 | | | 0.020 | | | | | 10 | | | | | | | | | | | | | | | | |
| | Pass | 0.017 | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | 0.999 904 00 | | MMF | | | | | | | | | | | | | | | | |

MMF Rounded to 7 decimal places

| | |
|--|------------------------------|
| | API Midstream Representative |
| | |
| | |

Example A.1 - Calibration Set I - Stop Proving Report - 2 of 2

| Field Prover | |
|--|--|
| Measurement Units | 1 (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) |
| Detector Design | 0 (0-Internal, 1-External) |
| Wall Material | 1 (1-CS, 2-304SS, 3-316SS, 4-17-4PH) |
| Rod Material | 0 (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) |
| Source for GL _{MP} , GL _{md} , E _{MP} | 1 (0-Prover Manufacturer, 1-API Table) |
| BPV _P | 1,892,370.578 0 mL at 15.0 °C and 0.0 kPag |

| Base Prover Volume (BPV) | | |
|--------------------------|-------------------|-------------------|
| BPV ₆₀ | BPV ₁₅ | BPV ₂₀ |
| Barrels | Cubic Meters | Cubic Meters |
| 11.902 874 232 117 | 1.892 370 578 000 | 1.892 687 378 000 |

| Decimals | 4 | 5 | 5 |
|------------|------------------------------------|---------------------------------|---------------------------------|
| Conversion | in ³ / Bbl 9.702E+03 | mL / M ³ 1.00E+06 | mL / M ³ 1.00E+06 |
| Rnd'd BPV | 11.902 900 000 000 | 1.892 370 000 000 | 1.892 690 000 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to 6 digits (the appropriate decimal place).

| T _B | 15.0 | °C |
|---------------------------|------|-----------------------------------|
| Decimal Base CTS | 9 | - |
| Decimal BPV ₆₀ | 4 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV _{SI} | 3 | mL at 15.0 °C and 0.0 kPag |
| Decimal BPV | 5 | Cubic Meters |
| Decimal BPV | 4 | Barrels |

Detector Design,

CTS_P = [1 + (T_P - T_B) x GL_P]³, for detectors mounted in calibrated section
 CTS_P = [1 + (T_P - T_B) x GL_P]² x [1 + (T_D - T_B) x GL_d], for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F

BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig
 BPV₁₅ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₁₅, 12) = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₂₀, 12) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C

BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 x Base CTS₆₀, 12) = in³ at 60.0 °F, 0.0 psig
 BPV₁₅ = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = ROUND(BPV₁₅ x Base CTS₂₀, 12) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C

BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 x Base CTS₆₀, 12) = in³ at 60.0 °F, 0.0 psig
 BPV₁₅ = ROUND(BPV₂₀ x Base CTS₁₅, 12) = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| GL _P | 0.000 006 20 | 0.000 011 16 | 0.000 011 16 |
|-----------------|--------------|--------------|--------------|
| GL _D | NA | NA | NA |
| T _B | 60.0 | 15.0 | 20.0 |

| Base CTS ₆₀ | 1.000 000 000 | 1.000 018 600 | 0.999 851 207 |
|------------------------|---------------|---------------|---------------|
| Base CTS ₁₅ | 0.999 981 400 | 1.000 000 000 | 0.999 832 609 |
| Base CTS ₂₀ | 1.000 148 807 | 1.000 167 409 | 1.000 000 000 |

| Base Unit Volume | |
|-------------------|---|
| BPV ₆₀ | 115,481.685 8 cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 1,892,370.578 mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 1,892,687.378 mL at 20.0 °C and 0.0 kPag |

| API Properties | | |
|---|------------------------------------|-------------------------------------|
| Linear Coefficient of Thermal Expansion, GL | | |
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar TM | 0.000 001 44 | 0.000 000 80 |

Notes:

(1) The User/Owner should obtain GL values from the prover manufacturer.

(2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.

(3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.

(4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.

(5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Example A.1 - Field Prover's BPV Conversion

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| Washington, D.C., USA | | | | | | | | | |
|--|------------------------------|--------------------------|----------------------------|---------------------------|-------------------|----------------------------|-------------------|----|--|
| BPV Determination using a Master Meter - Standard Method | | | | | | | | | |
| General Data | | | Master Meter | | | Field Prover | | | |
| API Midstream | Operator | Flowmeter ID | 200 | - | Manufacturer | API | - | | |
| Headquarters | Station Name | Manufacturer | API | - | Prover Design | Displacement | - | | |
| Washington | City, Town | Model | API-PD | - | Flow Design | Bidirectional | - | | |
| D.C. | State, Province | Nominal Size | 100 | mm | Wall Design | Single | - | | |
| USA | Country | Type | PD | - | Detector | Internal | - | | |
| RBOB | Fluid, Batch No. | Proving Result | MMF | - | Displacer | Free Sphere | - | | |
| Products | Ch 11.1 | T _F Comp | No | - | Wall Material | Carbon Steel | - | | |
| 15.0 | T _B | P _F Comp | No | - | Rod Material | NA | - | | |
| 0.0 | P _B | NKF | 52,834.410 5 | P / M3 | GL _P | 0.000 011 16 | per °C | | |
| 14-Feb-2024 | Start Calibration | Cartridge No. | API-0011 | - | GL _D | NA | per °C | | |
| 14-Feb-2024 | Stop Calibration | | | - | E _P | 206 842 710 | per kPag | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r \leq 0.02\%$, for 3 consecutive Calibration Sets Refined Product - Tables 5B/6B | | | ρ_{obs} Method | Continuous | - | ID _P | 547.675 0 | mm | |
| | | | ρ_{obs} Device | Online Density | - | WT _P | 30.963 0 | mm | |
| | | | DMF | 0.999 8 | - | Trips per Run | 1 | | |
| | | | HYC Factor | No | - | Serial No. | Bidi-SI-001 | | |
| | | | | | - | Switches | 9206 to 9236 | | |
| | | Calibration Set I | | Calibration Set II | | Calibration Set III | | | |
| | Start | Stop | Start | Stop | Start | Stop | | | |
| Report No. | Start 1 | Stop 1 | Start 2 | Stop 2 | Start 3 | Stop 3 | | | |
| Date | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | | | |
| Products | Products | Products | 84RBOB | 84RBOB | Products | Products | | | |
| API _B | 60.7 | 60.5 | 60.9 | 60.9 | 60.7 | 60.5 | °API | | |
| ρ_B | 735.715 | 736.216 | 734.963 | 734.924 | 735.715 | 736.216 | kg/m ³ | | |
| Q _{MM} | 111.347 | 111.347 | 83.332 | 83.434 | 140.250 | 140.222 | MPH | | |
| T _{MP_AVG} | 22.828 | 21.163 | 21.506 | 21.517 | 22.833 | 22.911 | °C | | |
| P _{MP_AVG} | 1,176.2 | 1,209.3 | 1,303.8 | 1,306.6 | 1,294.1 | 1,298.3 | kPag | | |
| Roundtrips | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | | | |
| Repeatability (r) | 0.018 | 0.017 | 0.011 | 0.008 | 0.018 | 0.017 | % | | |
| MMF | 0.999 900 0 | 0.999 904 1 | 0.999 974 0 | 0.999 999 0 | 1.000 099 0 | 1.000 154 0 | | | |
| MMF _{SET} | NA | 0.999 902 1 | NA | 0.999 986 5 | NA | 1.000 126 5 | | | |
| ΔMMF | NA | 0.000 | NA | 0.003 | NA | 0.006 | % | | |
| | ΔMMF_{SET} | Pass | | Pass | | Pass | | | |
| | (r) CPV_{RUN} | Pass | | Pass | | Pass | | | |
| | (R) CPV_{SET} | NA | | Pass | | Pass | | | |
| | ΔQ_{SET} | NA | | Pass | | Pass | | | |
| | Selected Set | Runs 4-6 | | Runs 1-3 | | Runs 1-3 | | | |
| | CPV_{SET} | 1.892 503 6 | M3 | 1.892 305 3 | M3 | 1.892 397 2 | M3 | | |
| | API _{B_SET} | 60.6 | °API | 61.0 | °API | 60.6 | °API | | |
| | ρ_{B_SET} | 735.962 | kg/m ³ | 734.522 | kg/m ³ | 735.889 | kg/m ³ | | |
| | T _{FP_SET} | 22.820 | °C | 21.442 | °C | 22.839 | °C | | |
| | P _{FP_SET} | 1,212.0 | kPag | 1,280.0 | kPag | 1,208.0 | kPag | | |
| | Q _{MM_SET} | 111.456 | MPH | 83.332 | MPH | 140.247 | MPH | | |
| CPV_{SET} Stability Parameters | ΔMMF _{SET} | 0.000 | % | 0.003 | % | 0.006 | % | | |
| | Δ ρ_{B_SET} | 0.073 | kg/m ³ | 0.292 | kg/m ³ | 0.278 | kg/m ³ | | |
| | ΔT _{P_SET} | 0.005 | °C | 0.028 | °C | 0.028 | °C | | |
| | ΔP _{P_SET} | 2.0 | kPag | 7.0 | kPag | 3.0 | kPag | | |
| | ΔQ _{MM_SET} | 0.0 | % | 0.0 | % | 0.0 | % | | |
| | ΔQ _{between SETS} | NA | % | (25.2) | % | 40.6 | % | | |
| | (r) CPV _{RUN} | 0.004 | % | 0.015 | % | 0.005 | % | | |
| | (R) CPV _{SET} | NA | % | 0.011 | % | 0.005 | % | | |

Example A.1 - Calibration Report Summary - 1 of 2

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|-------------------|---|--|----------|-------------------|--------------|--------------------|-------------|------|--------------------|-------------|---------|------|------------------|----------|---------|---------|---|----------------------------|----------------|-------------|-------------------|---------------|---|---|---------------|----------------------------|-------------------|---------------|----------------------------|---------------|--------------|-------------|---------------|-------------|--------|----------|----------|-----------|-------------|---------------|--------------|--------------|----|-----------------|--------------|--------|-----------------|----|--------|----------------|-------------|----------|-----------------|-----------|----|-----------------|----------|----|------------|-------------|--|----------|--------------|--|
| BPV Determination using a Master Meter - Standard Method | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| General Data <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td>API Midstream</td><td>Operator</td></tr> <tr><td>Headquarters</td><td>Station Name</td></tr> <tr><td>Washington</td><td>City, Town</td></tr> <tr><td>D.C.</td><td>State, Province</td></tr> <tr><td>USA</td><td>Country</td></tr> <tr><td>RBOB</td><td>Fluid, Batch No.</td></tr> <tr><td>Products</td><td>Ch 11.1</td></tr> <tr><td>15.0</td><td>T_B</td></tr> <tr><td>0.0</td><td>P_B</td></tr> <tr><td>14-Feb-2024</td><td>Start Calibration</td></tr> <tr><td>14-Feb-2024</td><td>Stop Calibration</td></tr> </table> | | | API Midstream | Operator | Headquarters | Station Name | Washington | City, Town | D.C. | State, Province | USA | Country | RBOB | Fluid, Batch No. | Products | Ch 11.1 | 15.0 | T _B | 0.0 | P _B | 14-Feb-2024 | Start Calibration | 14-Feb-2024 | Stop Calibration | Field Prover <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td>Manufacturer</td><td>API</td></tr> <tr><td>Prover Design</td><td>Displacement</td></tr> <tr><td>Flow Design</td><td>Bidirectional</td></tr> <tr><td>Wall Design</td><td>Single</td></tr> <tr><td>Detector</td><td>Internal</td></tr> <tr><td>Displacer</td><td>Free Sphere</td></tr> <tr><td>Wall Material</td><td>Carbon Steel</td></tr> <tr><td>Rod Material</td><td>NA</td></tr> <tr><td>GL_P</td><td>0.000 011 16</td><td>per °C</td></tr> <tr><td>GL_D</td><td>NA</td><td>per °C</td></tr> <tr><td>E_P</td><td>206 842 710</td><td>per kPag</td></tr> <tr><td>ID_P</td><td>547.675 0</td><td>mm</td></tr> <tr><td>WT_P</td><td>30.963 0</td><td>mm</td></tr> <tr><td>Serial No.</td><td>Bidi-SI-001</td><td></td></tr> <tr><td>Switches</td><td>9206 to 9236</td><td></td></tr> </table> | | | | Manufacturer | API | Prover Design | Displacement | Flow Design | Bidirectional | Wall Design | Single | Detector | Internal | Displacer | Free Sphere | Wall Material | Carbon Steel | Rod Material | NA | GL _P | 0.000 011 16 | per °C | GL _D | NA | per °C | E _P | 206 842 710 | per kPag | ID _P | 547.675 0 | mm | WT _P | 30.963 0 | mm | Serial No. | Bidi-SI-001 | | Switches | 9206 to 9236 | |
| API Midstream | Operator | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Headquarters | Station Name | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Washington | City, Town | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| D.C. | State, Province | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| USA | Country | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RBOB | Fluid, Batch No. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Products | Ch 11.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15.0 | T _B | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.0 | P _B | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14-Feb-2024 | Start Calibration | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14-Feb-2024 | Stop Calibration | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Manufacturer | API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Prover Design | Displacement | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow Design | Bidirectional | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Wall Design | Single | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Detector | Internal | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Displacer | Free Sphere | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Wall Material | Carbon Steel | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Rod Material | NA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GL _P | 0.000 011 16 | per °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GL _D | NA | per °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| E _P | 206 842 710 | per kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ID _P | 547.675 0 | mm | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| WT _P | 30.963 0 | mm | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Serial No. | Bidi-SI-001 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Switches | 9206 to 9236 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r \leq 0.02\%$, for 3 consecutive Calibration Sets Refined Product - Tables 5B/6B | | | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td>BPV_{NEW}</td><td>1.892 400 0</td><td>M3</td></tr> <tr><td>BPV_{OLD}</td><td>1.892 370 0</td><td>M3</td></tr> <tr><td>ΔBPV</td><td>0.000 030 0</td><td>M3</td></tr> <tr><td>ΔBPV</td><td>0.001 6</td><td>% BPV_{NEW} Bigger / (Smaller)</td></tr> </table> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td>Average CPV_{SET}</td><td>1.892 402 020</td><td>M3</td></tr> </table> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td>BPV₆₀</td><td>115,483.604 6</td><td>in³ at 60.0 °F and 0.0 psig</td></tr> <tr><td>BPV₁₅</td><td>1,892,402.020</td><td>mL at 15.0 °C and 0.0 kPag</td></tr> <tr><td>BPV₂₀</td><td>1,892,718.825</td><td>mL at 20.0 °C and 0.0 kPag</td></tr> </table> | | | | BPV _{NEW} | 1.892 400 0 | M3 | BPV _{OLD} | 1.892 370 0 | M3 | ΔBPV | 0.000 030 0 | M3 | ΔBPV | 0.001 6 | % BPV _{NEW} Bigger / (Smaller) | Average CPV _{SET} | 1.892 402 020 | M3 | BPV ₆₀ | 115,483.604 6 | in ³ at 60.0 °F and 0.0 psig | BPV ₁₅ | 1,892,402.020 | mL at 15.0 °C and 0.0 kPag | BPV ₂₀ | 1,892,718.825 | mL at 20.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV _{NEW} | 1.892 400 0 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV _{OLD} | 1.892 370 0 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔBPV | 0.000 030 0 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔBPV | 0.001 6 | % BPV _{NEW} Bigger / (Smaller) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Average CPV _{SET} | 1.892 402 020 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₆₀ | 115,483.604 6 | in ³ at 60.0 °F and 0.0 psig | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₁₅ | 1,892,402.020 | mL at 15.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₂₀ | 1,892,718.825 | mL at 20.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Base Prover Volume (BPV _{NEW}) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₆₀ | | | BPV ₁₅ | | BPV ₂₀ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Barrels | U.S. Gallons | Cubic Feet | Cubic Meters | Liters | Cubic Meters | Liters | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | 1,892.40 | - | 1,892.72 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | 499.929 | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 11.903 1 | - | 66.830 8 | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | 1.892 40 | - | 1.892 72 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Note: The BPV_{NEW} values (BPV₆₀, BPV₁₅, BPV₂₀) shown are reported to 6 significant digits (10 ppm, or, 0.001%).

| Signature | Date | Company |
|-----------|------|------------------------------|
| | | API Midstream Representative |
| | | |
| | | |
| | | |

Example A.1 - Calibration Report Summary - 2 of 2

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| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|-------------------------------|-------------------------|---|-------------------------------|------------------------|--|-------------------------------------|--------------|--|--|-------|------|--|------------|---------|--------|--|------|-----------|-----------|--|------|------------|-------------|--|-----------|---------------|---------------|----|------------------|----------|----------|--|-------------------|------|------|------|-----------------|---------|---------|-------------------|-------------------|------|------|------|-----------------|---------|---------|-------------------|-------------------|------|------|------|-----------------|---------|---------|-------------------|---------------------------|---------|---------|-----|---------------------|--------|--------|----|---------------------|--------|--------|------|---------------|---|---|--|------------|----------|----------|--|-------------------|-------|-------|---|---------------|-------|-------|---|---------------|------|------|--|-----|-------------|-------------|--|------|----|-------|---|------------------|----|-------|---|----------------|----|------|--|
| BPV Determination using Master Meter - Calibration Set I | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| General Data Operator: API Midstream Station Name: Headquarters Fluid or Batch: RBOB Ch 11.1: Products T _B : 15.0 °C P _B : 0.0 kPag | | | Field Prover Prover Manufacturer: API Prover Design: Displacement Flow Design: Bidirectional Wall Design: Single Detector: Internal Displacer: Free Sphere Wall Material: 300 SS Rod Material: NA GL _P : 0.000 011 16 per °C GL _D : NA per °C E _P : 206 842 710 per kPag ID _P : 547.675 0 mm WT _P : 30.963 0 mm Serial No.: Bidi-SI-001 Switches: 9206 to 9236 | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="background-color: #d9ead3;">Start</th> <th style="background-color: #d9ead3;">Stop</th> <th></th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td>Start 1</td> <td>Stop 1</td> <td></td> </tr> <tr> <td>Date</td> <td>14-Feb-24</td> <td>14-Feb-24</td> <td></td> </tr> <tr> <td>Time</td> <td>8:21:18 AM</td> <td>11:21:18 AM</td> <td></td> </tr> <tr> <td>Totalizer</td> <td>2,342,501.020</td> <td>2,343,601.020</td> <td>M3</td> </tr> <tr> <td>Fluid, Batch No.</td> <td>Products</td> <td>Products</td> <td></td> </tr> <tr> <td>API₆₀</td> <td>60.8</td> <td>60.6</td> <td>°API</td> </tr> <tr> <td>P₆₀</td> <td>735.210</td> <td>735.710</td> <td>kg/m³</td> </tr> <tr> <td>API₁₅</td> <td>60.7</td> <td>60.5</td> <td>°API</td> </tr> <tr> <td>P₁₅</td> <td>735.715</td> <td>736.216</td> <td>kg/m³</td> </tr> <tr> <td>API₂₀</td> <td>61.7</td> <td>61.5</td> <td>°API</td> </tr> <tr> <td>P₂₀</td> <td>731.158</td> <td>731.660</td> <td>kg/m³</td> </tr> <tr> <td>Flowrate, Q_{av}</td> <td>111.347</td> <td>111.347</td> <td>MPH</td> </tr> <tr> <td>T_{MP_AVG}</td> <td>22.828</td> <td>21.163</td> <td>°C</td> </tr> <tr> <td>P_{MP_AVG}</td> <td>1176.2</td> <td>1209.3</td> <td>kPag</td> </tr> <tr> <td>Trips per Run</td> <td>1</td> <td>1</td> <td></td> </tr> <tr> <td>Roundtrips</td> <td>Runs 1-5</td> <td>Runs 1-5</td> <td></td> </tr> <tr> <td>Repeatability (r)</td> <td>0.018</td> <td>0.017</td> <td>%</td> </tr> <tr> <td>Allowable (r)</td> <td>0.020</td> <td>0.020</td> <td>%</td> </tr> <tr> <td>(r) Pass/Fail</td> <td>Pass</td> <td>Pass</td> <td></td> </tr> <tr> <td>MMF</td> <td>0.999 900 0</td> <td>0.999 904 1</td> <td></td> </tr> <tr> <td>ΔMMF</td> <td>NA</td> <td>0.000</td> <td>%</td> </tr> <tr> <td>Allowable ± ΔMMF</td> <td>NA</td> <td>0.020</td> <td>%</td> </tr> <tr> <td>ΔMMF Pass/Fail</td> <td>NA</td> <td>Pass</td> <td></td> </tr> </tbody> </table> | | | | | Start | Stop | | Report No. | Start 1 | Stop 1 | | Date | 14-Feb-24 | 14-Feb-24 | | Time | 8:21:18 AM | 11:21:18 AM | | Totalizer | 2,342,501.020 | 2,343,601.020 | M3 | Fluid, Batch No. | Products | Products | | API ₆₀ | 60.8 | 60.6 | °API | P ₆₀ | 735.210 | 735.710 | kg/m ³ | API ₁₅ | 60.7 | 60.5 | °API | P ₁₅ | 735.715 | 736.216 | kg/m ³ | API ₂₀ | 61.7 | 61.5 | °API | P ₂₀ | 731.158 | 731.660 | kg/m ³ | Flowrate, Q _{av} | 111.347 | 111.347 | MPH | T _{MP_AVG} | 22.828 | 21.163 | °C | P _{MP_AVG} | 1176.2 | 1209.3 | kPag | Trips per Run | 1 | 1 | | Roundtrips | Runs 1-5 | Runs 1-5 | | Repeatability (r) | 0.018 | 0.017 | % | Allowable (r) | 0.020 | 0.020 | % | (r) Pass/Fail | Pass | Pass | | MMF | 0.999 900 0 | 0.999 904 1 | | ΔMMF | NA | 0.000 | % | Allowable ± ΔMMF | NA | 0.020 | % | ΔMMF Pass/Fail | NA | Pass | |
| | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start 1 | Stop 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 8:21:18 AM | 11:21:18 AM | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Totalizer | 2,342,501.020 | 2,343,601.020 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Products | Products | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₆₀ | 60.8 | 60.6 | °API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P ₆₀ | 735.210 | 735.710 | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₁₅ | 60.7 | 60.5 | °API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P ₁₅ | 735.715 | 736.216 | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₂₀ | 61.7 | 61.5 | °API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P ₂₀ | 731.158 | 731.660 | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flowrate, Q _{av} | 111.347 | 111.347 | MPH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| T _{MP_AVG} | 22.828 | 21.163 | °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P _{MP_AVG} | 1176.2 | 1209.3 | kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Trips per Run | 1 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrips | Runs 1-5 | Runs 1-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Repeatability (r) | 0.018 | 0.017 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Allowable (r) | 0.020 | 0.020 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) Pass/Fail | Pass | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MMF | 0.999 900 0 | 0.999 904 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF | NA | 0.000 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Allowable ± ΔMMF | NA | 0.020 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF Pass/Fail | NA | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Master Meter Flowmeter ID: 200 Manufacturer: API Model: API-PD Nominal Size: 100 mm Type: PD Proving Result: MMF T _F Comp: No P _F Comp: No NKF: 52,834.410 5 P / M3 Cartridge No.: API-0011 | | | Density Method ρ _{obs} Method: Continuous ρ _{obs} Device: Online Density DMF: 0.999 8 HYC Factor: No | | | Calibration Set Criteria ΔMMF _{SET} ≤ 0.02 % (r) ICPV _{RUN} ≤ 0.02 % (r) CPV _{RUN} ≤ 0.02 % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs Refined Product - Tables 5B/6B | | | Spot Sample ρ _{60_START} : NA kg/m ³ ρ _{60_STOP} : NA kg/m ³ ρ _{60_SET} : NA kg/m ³ MMF _{SET} : 0.999 902 1 | | | Prior vs Current ΔQ _{av} : 0.02 % ΔT _P : 0.036 °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | Base Density | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ _{obs} kg/m ³ | T _{dm} °C | P _{dm} kPag | T _{P_INLET} °C | T _{P_OUTLET} °C | T _M °C | T _D °C | ρ _B kg/m ³ | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.748 | 22.906 | 1,203.0 | 22.817 | 22.889 | 22.994 | | 735.921 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.843 | 22.906 | 1,208.0 | 22.806 | 22.844 | 22.994 | | 736.011 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.545 | 22.928 | 1,208.0 | 22.822 | 22.856 | 23.000 | | 735.734 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.748 | 22.911 | 1,210.0 | 22.817 | 22.817 | 23.000 | | 735.919 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.799 | 22.911 | 1,205.0 | 22.811 | 22.828 | 23.056 | | 735.975 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.823 | 22.906 | 1,207.0 | 22.811 | 22.833 | 23.011 | | 735.992 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.751 | 22.911 | 1,207.0 | 22.814 | 22.845 | 23.009 | | 735.925 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Ch 11.1 Iteration Results | N or N _i Pulses | Q _M MPH | P _{P_INLET} kPag | P _{P_OUTLET} kPag | P _M kPag | T _{P_RUN} °C | P _{P_RUN} kPag | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,015.000 | 111.468 | 1,214.0 | 1,198.0 | 1,278.0 | 22.853 0 | 1,206.00 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,001.000 | 111.447 | 1,218.0 | 1,200.0 | 1,282.0 | 22.825 0 | 1,209.00 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,022.000 | 111.449 | 1,215.0 | 1,200.0 | 1,285.0 | 22.839 0 | 1,207.50 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,051.000 | 111.452 | 1,219.0 | 1,202.0 | 1,285.0 | 22.817 0 | 1,210.50 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,054.000 | 111.450 | 1,220.0 | 1,204.0 | 1,287.0 | 22.819 5 | 1,212.00 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,052.000 | 111.466 | 1,220.0 | 1,205.0 | 1,279.0 | 22.822 0 | 1,212.50 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 100,032.500 0 | 111.456 | 1,218.0 | 1,202.0 | 1,283.0 | 22.829 0 | 1,210.00 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Example A.1 - Calibration Set I - 1 of 2

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|--|------------------------------|---|--------------------------|--|-------------------|---------------|--------------------------------|--|---------------------------|-----------------------------|--------------------------|------------------------------|-------------------|---------------|--------------------|---------------|---------------|---------------|------------------|---------------|---------------|---|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|---|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|---|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|------|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|---|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|---|---------------|---------------|---------------|---------------|---------------|---------------|---------------|-----|
| BPV Determination using Master Meter - Calibration Set I | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Refined Product - Tables 5B/6B | | | ΔMMF_{SET} Pass $(r) ICPV_{RUN}$ Pass $(r) CPV_{RUN}$ Pass | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th>Prior</th> <th>Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td>Start</td> <td>Stop</td> </tr> <tr> <td>Date</td> <td>14-Feb-24</td> <td>14-Feb-24</td> </tr> <tr> <td>Time</td> <td>08:21:18</td> <td>11:21:18</td> </tr> <tr> <td>Fluid, Batch No.</td> <td>Products</td> <td>Products</td> </tr> </tbody> </table> | | | | Prior | Current | Report No. | Start | Stop | Date | 14-Feb-24 | 14-Feb-24 | Time | 08:21:18 | 11:21:18 | Fluid, Batch No. | Products | Products | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 08:21:18 | 11:21:18 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Products | Products | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>N or N_i Pulses</th> <th>NKF P / M3</th> <th>IV_M</th> <th>CTL_M</th> <th>CPL_M</th> <th>$CTPL_M$</th> <th>GSV_M M3</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>100,015.000</td><td>52,834.410 5</td><td>1.892 989 8</td><td>0.990 088 855</td><td>1.001 518 008</td><td>0.991 591 818</td><td>1.876 889 430</td><td>1</td></tr> <tr><td>100,001.000</td><td>52,834.410 5</td><td>1.892 724 8</td><td>0.990 090 711</td><td>1.001 522 097</td><td>0.991 597 725</td><td>1.876 637 860</td><td>2</td></tr> <tr><td>100,022.000</td><td>52,834.410 5</td><td>1.893 122 3</td><td>0.990 077 557</td><td>1.001 527 798</td><td>0.991 590 195</td><td>1.877 017 730</td><td>3</td></tr> <tr><td>100,051.000</td><td>52,834.410 5</td><td>1.893 671 2</td><td>0.990 081 364</td><td>1.001 526 420</td><td>0.991 592 644</td><td>1.877 566 600</td><td>4</td></tr> <tr><td>100,054.000</td><td>52,834.410 5</td><td>1.893 728 0</td><td>0.990 012 875</td><td>1.001 529 073</td><td>0.991 526 678</td><td>1.877 498 010</td><td>5</td></tr> <tr><td>100,052.000</td><td>52,834.410 5</td><td>1.893 690 1</td><td>0.990 069 185</td><td>1.001 518 877</td><td>0.991 572 979</td><td>1.877 548 100</td><td>6</td></tr> <tr><td>100,032.500 0</td><td>52,834.410 5</td><td>1.893 321 0</td><td>0.990 070 091</td><td>1.001 523 712</td><td>0.991 578 673</td><td>1.877 192 960</td><td>Avg</td></tr> </tbody> </table> | | | | | | | | N or N_i Pulses | NKF P / M3 | IV_M | CTL_M | CPL_M | $CTPL_M$ | GSV_M M3 | Run | 100,015.000 | 52,834.410 5 | 1.892 989 8 | 0.990 088 855 | 1.001 518 008 | 0.991 591 818 | 1.876 889 430 | 1 | 100,001.000 | 52,834.410 5 | 1.892 724 8 | 0.990 090 711 | 1.001 522 097 | 0.991 597 725 | 1.876 637 860 | 2 | 100,022.000 | 52,834.410 5 | 1.893 122 3 | 0.990 077 557 | 1.001 527 798 | 0.991 590 195 | 1.877 017 730 | 3 | 100,051.000 | 52,834.410 5 | 1.893 671 2 | 0.990 081 364 | 1.001 526 420 | 0.991 592 644 | 1.877 566 600 | 4 | 100,054.000 | 52,834.410 5 | 1.893 728 0 | 0.990 012 875 | 1.001 529 073 | 0.991 526 678 | 1.877 498 010 | 5 | 100,052.000 | 52,834.410 5 | 1.893 690 1 | 0.990 069 185 | 1.001 518 877 | 0.991 572 979 | 1.877 548 100 | 6 | 100,032.500 0 | 52,834.410 5 | 1.893 321 0 | 0.990 070 091 | 1.001 523 712 | 0.991 578 673 | 1.877 192 960 | Avg |
| N or N_i Pulses | NKF P / M3 | IV_M | CTL_M | CPL_M | $CTPL_M$ | GSV_M M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,015.000 | 52,834.410 5 | 1.892 989 8 | 0.990 088 855 | 1.001 518 008 | 0.991 591 818 | 1.876 889 430 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,001.000 | 52,834.410 5 | 1.892 724 8 | 0.990 090 711 | 1.001 522 097 | 0.991 597 725 | 1.876 637 860 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,022.000 | 52,834.410 5 | 1.893 122 3 | 0.990 077 557 | 1.001 527 798 | 0.991 590 195 | 1.877 017 730 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,051.000 | 52,834.410 5 | 1.893 671 2 | 0.990 081 364 | 1.001 526 420 | 0.991 592 644 | 1.877 566 600 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,054.000 | 52,834.410 5 | 1.893 728 0 | 0.990 012 875 | 1.001 529 073 | 0.991 526 678 | 1.877 498 010 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,052.000 | 52,834.410 5 | 1.893 690 1 | 0.990 069 185 | 1.001 518 877 | 0.991 572 979 | 1.877 548 100 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,032.500 0 | 52,834.410 5 | 1.893 321 0 | 0.990 070 091 | 1.001 523 712 | 0.991 578 673 | 1.877 192 960 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Iteration Results</th> <th>CTS_P</th> <th>CPS_P</th> <th>CTL_P</th> <th>CPL_P</th> <th>$CTPL_P$</th> <th>CPV_{run} M3</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>Gasoline, Napthene</td><td>1.000 262 941</td><td>1.000 103 130</td><td>0.990 264 161</td><td>1.001 430 750</td><td>0.991 680 981</td><td>1.891 941 650</td><td>1</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 262 004</td><td>1.000 103 387</td><td>0.990 300 787</td><td>1.001 433 363</td><td>0.991 720 247</td><td>1.891 614 450</td><td>2</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 262 473</td><td>1.000 103 259</td><td>0.990 277 805</td><td>1.001 433 674</td><td>0.991 697 540</td><td>1.892 040 030</td><td>3</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 261 736</td><td>1.000 103 515</td><td>0.990 308 886</td><td>1.001 435 693</td><td>0.991 730 666</td><td>1.892 530 990</td><td>4</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 261 820</td><td>1.000 103 644</td><td>0.990 306 886</td><td>1.001 437 118</td><td>0.991 730 074</td><td>1.892 462 580</td><td>5</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 261 903</td><td>1.000 103 686</td><td>0.990 304 133</td><td>1.001 437 617</td><td>0.991 727 811</td><td>1.892 517 150</td><td>6</td></tr> <tr><td></td><td>1.000 262 146</td><td>1.000 103 437</td><td>0.990 293 776</td><td>1.001 434 703</td><td>0.991 714 553</td><td>1.892 184 480</td><td>Avg</td></tr> </tbody> </table> | | | | | | | | Iteration Results | CTS_P | CPS_P | CTL_P | CPL_P | $CTPL_P$ | CPV_{run} M3 | Run | Gasoline, Napthene | 1.000 262 941 | 1.000 103 130 | 0.990 264 161 | 1.001 430 750 | 0.991 680 981 | 1.891 941 650 | 1 | Gasoline, Napthene | 1.000 262 004 | 1.000 103 387 | 0.990 300 787 | 1.001 433 363 | 0.991 720 247 | 1.891 614 450 | 2 | Gasoline, Napthene | 1.000 262 473 | 1.000 103 259 | 0.990 277 805 | 1.001 433 674 | 0.991 697 540 | 1.892 040 030 | 3 | Gasoline, Napthene | 1.000 261 736 | 1.000 103 515 | 0.990 308 886 | 1.001 435 693 | 0.991 730 666 | 1.892 530 990 | 4 | Gasoline, Napthene | 1.000 261 820 | 1.000 103 644 | 0.990 306 886 | 1.001 437 118 | 0.991 730 074 | 1.892 462 580 | 5 | Gasoline, Napthene | 1.000 261 903 | 1.000 103 686 | 0.990 304 133 | 1.001 437 617 | 0.991 727 811 | 1.892 517 150 | 6 | | 1.000 262 146 | 1.000 103 437 | 0.990 293 776 | 1.001 434 703 | 0.991 714 553 | 1.892 184 480 | Avg |
| Iteration Results | CTS_P | CPS_P | CTL_P | CPL_P | $CTPL_P$ | CPV_{run} M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 262 941 | 1.000 103 130 | 0.990 264 161 | 1.001 430 750 | 0.991 680 981 | 1.891 941 650 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 262 004 | 1.000 103 387 | 0.990 300 787 | 1.001 433 363 | 0.991 720 247 | 1.891 614 450 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 262 473 | 1.000 103 259 | 0.990 277 805 | 1.001 433 674 | 0.991 697 540 | 1.892 040 030 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 261 736 | 1.000 103 515 | 0.990 308 886 | 1.001 435 693 | 0.991 730 666 | 1.892 530 990 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 261 820 | 1.000 103 644 | 0.990 306 886 | 1.001 437 118 | 0.991 730 074 | 1.892 462 580 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 261 903 | 1.000 103 686 | 0.990 304 133 | 1.001 437 617 | 0.991 727 811 | 1.892 517 150 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 262 146 | 1.000 103 437 | 0.990 293 776 | 1.001 434 703 | 0.991 714 553 | 1.892 184 480 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>1 means ΔCPV Passed</th> <th>Δp_{B_SET} kg/m³</th> <th>ΔT_{P_SET} °C</th> <th>ΔP_{P_SET} kPag</th> <th>ΔQ_{M_SET} %</th> <th>r% CPV</th> <th>CPV_set</th> <th>CPV_set M3</th> <th></th> </tr> </thead> <tbody> <tr> <td rowspan="4" style="text-align: center;">1</td> <td>0.278</td> <td>0.028</td> <td>3.00</td> <td>0.0</td> <td>0.022</td> <td>-</td> <td>1.891 865 380</td> <td>Runs 1-3</td> </tr> <tr> <td>0.278</td> <td>0.022</td> <td>3.00</td> <td>0.0</td> <td>0.048</td> <td>-</td> <td>1.892 061 820</td> <td>Runs 2-4</td> </tr> <tr> <td>0.241</td> <td>0.022</td> <td>4.50</td> <td>0.0</td> <td>0.026</td> <td>-</td> <td>1.892 344 530</td> <td>Runs 3-5</td> </tr> <tr> <td>0.073</td> <td>0.005</td> <td>2.00</td> <td>0.0</td> <td>0.004</td> <td>Pass</td> <td>1.892 503 570</td> <td>Runs 4-6</td> </tr> </tbody> </table> | | | | | | | | 1 means ΔCPV Passed | Δp_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{M_SET} % | r% CPV | CPV_set | CPV_set M3 | | 1 | 0.278 | 0.028 | 3.00 | 0.0 | 0.022 | - | 1.891 865 380 | Runs 1-3 | 0.278 | 0.022 | 3.00 | 0.0 | 0.048 | - | 1.892 061 820 | Runs 2-4 | 0.241 | 0.022 | 4.50 | 0.0 | 0.026 | - | 1.892 344 530 | Runs 3-5 | 0.073 | 0.005 | 2.00 | 0.0 | 0.004 | Pass | 1.892 503 570 | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | |
| 1 means ΔCPV Passed | Δp_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{M_SET} % | r% CPV | CPV_set | CPV_set M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | 0.278 | 0.028 | 3.00 | 0.0 | 0.022 | - | 1.891 865 380 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.278 | 0.022 | 3.00 | 0.0 | 0.048 | - | 1.892 061 820 | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.241 | 0.022 | 4.50 | 0.0 | 0.026 | - | 1.892 344 530 | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.073 | 0.005 | 2.00 | 0.0 | 0.004 | Pass | 1.892 503 570 | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Signature</th> <th>Date</th> <th>Company</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td>API Midstream Representative</td> </tr> <tr> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> </tbody> </table> | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example A.1 - Calibration Set I - 2 of 2

This document is not an API Standard; it is under consideration within an API technical committee but has not received all approvals required to become an API Standard. It shall not be reproduced or circulated or quoted, in whole or in part, outside of API committee activities except with the approval of the Chairman of the committee having jurisdiction and staff of the API Standards Dept. Copyright API. All rights reserved.

| Washington, D.C., USA | | | | | | | | | |
|--|---------------------|-----------------------|---------------------------------|-----------------------------|-----------------|------------------------------|----------------|---|-------|
| BPV Determination using Master Meter - Calibration Set II | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start 2 | Stop 2 | |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | 14-Feb-24 | 14-Feb-24 | |
| Fluid or Batch | RBOB | | Flow Design | Bidirectional | | Time | 10:53:11 AM | 12:40:18 PM | |
| Ch 11.1 | Products | | Wall Design | Single | | Totalizer | 2,342,521.020 | 2,343,841.020 | M3 |
| T _B | 15.0 | °C | Detector | Internal | | Fluid, Batch No. | 84RBOB | 84RBOB | |
| P _B | 0.0 | kPag | Displacer | Free Sphere | | API ₆₀ | 61.0 | 61.0 | °API |
| Master Meter | | | Wall Material | 300 SS | | P ₆₀ | 734.457 | 734.419 | kg/m3 |
| Flowmeter ID | 200 | | Rod Material | NA | | API ₁₅ | 60.9 | 60.9 | °API |
| Manufacturer | API | | GL _P | 0.000 011 16 per °C | | P ₁₅ | 734.963 | 734.924 | kg/m3 |
| Model | API-PD | | GL _D | NA per °C | | API ₂₀ | 61.9 | 61.9 | °API |
| Nominal Size | 100 mm | | E _P | 206 842 710 per kPag | | P ₂₀ | 730.402 | 730.364 | kg/m3 |
| Type | PD | | ID _P | 547.675 0 mm | | Flowrate, Q _{av} | 83.332 | 83.434 | MPH |
| Proving Result | MMF | | WT _P | 30.963 0 mm | | T _{MP_AVG} | 21.506 | 21.517 | °C |
| T _F Comp | No | | Serial No. | Bidi-SI-001 | | P _{MP_AVG} | 1303.8 | 1306.6 | kPag |
| P _F Comp | No | | Switches | 9206 to 9236 | | Trips per Run | 1 | 1 | |
| NKF | 52,834.410 5 P / M3 | | | | | Roundtrips | Runs 1-5 | Runs 1-5 | |
| Cartridge No. | API-0011 | | | | | Repeatability (r) | 0.011 | 0.008 | % |
| Density Method | | | Calibration Set Criteria | | | Allowable (r) | 0.020 | 0.020 | % |
| ρ _{obs} Method | Continuous | | ΔMMF _{SET} | ≤ 0.02 % | | (r) Pass/Fail | Pass | Pass | |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 % | | MMF | 0.999 974 0 | 0.999 999 0 | % |
| DMF | 0.999 8 | | (r) CPV _{RUN} | ≤ 0.02 % | | ΔMMF | NA | 0.003 | % |
| HYC Factor | No | | Spot Sample | | | Allowable ± ΔMMF | NA | 0.020 | % |
| API Chapter 12.4.2 | | | ρ _{60_START} | NA kg/m ³ | | ΔMMF Pass/Fail | NA | Pass | |
| SI 15 Measurement Units | | | ρ _{60_STOP} | NA kg/m ³ | | | | | |
| Sampling Method - Continuous | | | ρ _{60_SET} | NA kg/m ³ | | | | | |
| BPV - Standard Method | | | MMF _{SET} | 0.999 986 5 | | | | | |
| Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs | | | | | | | | | |
| Refined Product - Tables 5B/6B | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | | |
| ρ _{obs} | T _{dm} | P _{dm} | T _{FP_INLET} | T _{FP_OUTLET} | T _{MM} | T _{FD} | Base Density | | |
| kg/m ³ | °C | kPag | °C | °C | °C | °C | ρ _B | kg/m ³ | Run |
| 729.748 | 21.506 | 1,300.0 | 21.494 | 21.394 | 21.400 | | 734.568 | | 1 |
| 729.843 | 21.494 | 1,308.0 | 21.500 | 21.411 | 21.422 | | 734.645 | | 2 |
| 729.545 | 21.494 | 1,301.0 | 21.494 | 21.361 | 21.461 | | 734.353 | | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| 729.712 | 21.498 | 1,303.0 | 21.496 | 21.389 | 21.428 | | 734.522 | | Avg |
| Ch 11.1 Iteration Results | | | | | | | | | |
| N or N_i | | Q_{MM} | | P_{FP_INLET} | | P_{FP_OUTLET} | | T_{FP} and P_{FP} Values | |
| Pulses | | MPH | | kPag | | kPag | | kPag | |
| °C | | kPag | | kPag | | kPag | | kPag | |
| Gasoline, Napthene | 100,015.000 | 83.332 | 1,284.0 | 1,279.0 | 1,268.0 | 21.444 0 | 1,281.50 | | 1 |
| Gasoline, Napthene | 100,001.000 | 83.331 | 1,288.0 | 1,278.0 | 1,270.0 | 21.455 5 | 1,283.00 | | 2 |
| Gasoline, Napthene | 100,022.000 | 83.332 | 1,284.0 | 1,268.0 | 1,257.0 | 21.427 5 | 1,276.00 | | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| | 100,012.700 0 | 83.332 | 1,285.0 | 1,275.0 | 1,265.0 | 21.442 0 | 1,280.00 | | Avg |

Example A.1 - Calibration Set II - 1 of 2

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|--|---|-----------------------------|---------------------------|--------------------|--------------------------|--------------------------|--------------------------------|--|---------------------------|-----------------------------|---------------------------|------------------------------|--------------------------|--------------------------|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|-------|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|----|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|----|----|----|----|--|---|--|----------|----------|--|----|----|----|----|--|---|---|----------|--|--|--|--|--|--|---|---------------|---------------|---------------|---------------|---------------|---------------|---------------|-----|
| BPV Determination using Master Meter - Calibration Set II | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Refined Product - Tables 5B/6B | | ΔMMF_{SET} Pass $(r) ICPV_{SET}$ Pass $(r) CPV_{SET}$ Pass | | Report Summary | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | Prior | | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | Date | Start 2 | Stop 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | Time | 00:00:00 | 00:00:00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | Fluid, Batch No. | 2342521.02 | 2343841.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th>N or N_i Pulses</th> <th>NKF P / M3</th> <th>IV_{MM}</th> <th>CTL_{MM}</th> <th>CPL_{MM}</th> <th>CTPL_{MM}</th> <th>GSV_{MM} M3</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>100,015.000</td><td>52,834.410 5</td><td>1.892 989 8</td><td>0.992 047 429</td><td>1.001 496 806</td><td>0.993 532 331</td><td>1.880 721 180</td><td>1</td></tr> <tr><td>100,001.000</td><td>52,834.410 5</td><td>1.892 724 8</td><td>0.992 021 304</td><td>1.001 498 874</td><td>0.993 508 218</td><td>1.880 412 260</td><td>2</td></tr> <tr><td>100,022.000</td><td>52,834.410 5</td><td>1.893 122 3</td><td>0.991 967 882</td><td>1.001 486 077</td><td>0.993 442 022</td><td>1.880 681 860</td><td>3</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>4</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>6</td></tr> <tr> <td>100,012.700 0</td> <td>52,834.410 5</td> <td>1.892 945 6</td> <td>0.992 012 205</td> <td>1.001 493 919</td> <td>0.993 494 191</td> <td>1.880 605 100</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | N or N _i Pulses | NKF P / M3 | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} M3 | Run | 100,015.000 | 52,834.410 5 | 1.892 989 8 | 0.992 047 429 | 1.001 496 806 | 0.993 532 331 | 1.880 721 180 | 1 | 100,001.000 | 52,834.410 5 | 1.892 724 8 | 0.992 021 304 | 1.001 498 874 | 0.993 508 218 | 1.880 412 260 | 2 | 100,022.000 | 52,834.410 5 | 1.893 122 3 | 0.991 967 882 | 1.001 486 077 | 0.993 442 022 | 1.880 681 860 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | 100,012.700 0 | 52,834.410 5 | 1.892 945 6 | 0.992 012 205 | 1.001 493 919 | 0.993 494 191 | 1.880 605 100 | Avg |
| N or N _i Pulses | NKF P / M3 | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,015.000 | 52,834.410 5 | 1.892 989 8 | 0.992 047 429 | 1.001 496 806 | 0.993 532 331 | 1.880 721 180 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,001.000 | 52,834.410 5 | 1.892 724 8 | 0.992 021 304 | 1.001 498 874 | 0.993 508 218 | 1.880 412 260 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,022.000 | 52,834.410 5 | 1.893 122 3 | 0.991 967 882 | 1.001 486 077 | 0.993 442 022 | 1.880 681 860 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,012.700 0 | 52,834.410 5 | 1.892 945 6 | 0.992 012 205 | 1.001 493 919 | 0.993 494 191 | 1.880 605 100 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th>Iteration Results</th> <th>CTS_{FP}</th> <th>CPS_{FP}</th> <th>CTL_{FP}</th> <th>CPL_{FP}</th> <th>CTPL_{FP}</th> <th>CPV_{run} M3</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>Gasoline, Napthene</td><td>1.000 215 761</td><td>1.000 109 587</td><td>0.991 992 627</td><td>1.001 513 300</td><td>0.993 493 810</td><td>1.892 421 900</td><td>1</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 216 146</td><td>1.000 109 715</td><td>0.991 979 587</td><td>1.001 514 647</td><td>0.993 482 085</td><td>1.892 132 420</td><td>2</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 215 208</td><td>1.000 109 116</td><td>0.992 009 625</td><td>1.001 508 167</td><td>0.993 505 742</td><td>1.892 361 550</td><td>3</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>4</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>6</td></tr> <tr> <td></td> <td>1.000 215 705</td> <td>1.000 109 473</td> <td>0.991 993 946</td> <td>1.001 512 038</td> <td>0.993 493 879</td> <td>1.892 305 290</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} M3 | Run | Gasoline, Napthene | 1.000 215 761 | 1.000 109 587 | 0.991 992 627 | 1.001 513 300 | 0.993 493 810 | 1.892 421 900 | 1 | Gasoline, Napthene | 1.000 216 146 | 1.000 109 715 | 0.991 979 587 | 1.001 514 647 | 0.993 482 085 | 1.892 132 420 | 2 | Gasoline, Napthene | 1.000 215 208 | 1.000 109 116 | 0.992 009 625 | 1.001 508 167 | 0.993 505 742 | 1.892 361 550 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | | 1.000 215 705 | 1.000 109 473 | 0.991 993 946 | 1.001 512 038 | 0.993 493 879 | 1.892 305 290 | Avg |
| Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 215 761 | 1.000 109 587 | 0.991 992 627 | 1.001 513 300 | 0.993 493 810 | 1.892 421 900 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 216 146 | 1.000 109 715 | 0.991 979 587 | 1.001 514 647 | 0.993 482 085 | 1.892 132 420 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 215 208 | 1.000 109 116 | 0.992 009 625 | 1.001 508 167 | 0.993 505 742 | 1.892 361 550 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 215 705 | 1.000 109 473 | 0.991 993 946 | 1.001 512 038 | 0.993 493 879 | 1.892 305 290 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr> <th>1 means ΔCPV Passed</th> <th>ΔP_{B_SET} kg/m³</th> <th>ΔT_{P_SET} °C</th> <th>ΔP_{P_SET} kPag</th> <th>ΔQ_{MM_SET} %</th> <th>r% CPV</th> <th>CPV_{set}</th> <th>CPV_{set} M3</th> <th></th> </tr> </thead> <tbody> <tr> <td>Runs 1-3</td> <td>1</td> <td>0.292</td> <td>0.028</td> <td>7.00</td> <td>0.0</td> <td>0.015</td> <td>Pass</td> <td>1.892 305 290</td> <td>Runs 1-3</td> </tr> <tr> <td>Runs 2-4</td> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td></td> <td>-</td> <td></td> <td>Runs 2-4</td> </tr> <tr> <td>Runs 3-5</td> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td></td> <td>-</td> <td></td> <td>Runs 3-5</td> </tr> <tr> <td>Runs 4-6</td> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td></td> <td>-</td> <td></td> <td>Runs 4-6</td> </tr> </tbody> </table> | | | | | | | | 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{MM_SET} % | r% CPV | CPV _{set} | CPV _{set} M3 | | Runs 1-3 | 1 | 0.292 | 0.028 | 7.00 | 0.0 | 0.015 | Pass | 1.892 305 290 | Runs 1-3 | Runs 2-4 | | NA | NA | NA | NA | | - | | Runs 2-4 | Runs 3-5 | | NA | NA | NA | NA | | - | | Runs 3-5 | Runs 4-6 | | NA | NA | NA | NA | | - | | Runs 4-6 | | | | | | | | | | | | | | | |
| 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{MM_SET} % | r% CPV | CPV _{set} | CPV _{set} M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 | 1 | 0.292 | 0.028 | 7.00 | 0.0 | 0.015 | Pass | 1.892 305 290 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 2-4 | | NA | NA | NA | NA | | - | | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 3-5 | | NA | NA | NA | NA | | - | | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 4-6 | | NA | NA | NA | NA | | - | | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 40%;">Signature</th> <th style="width: 20%;">Date</th> <th style="width: 40%;">Company</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td>API Midstream Representative</td> </tr> <tr><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td></tr> </tbody> </table> | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example A.1 - Calibration Set II - 2 of 2

This document is not an API Standard; it is under consideration within an API technical committee but has not received all approvals required to become an API Standard. It shall not be reproduced or circulated or quoted, in whole or in part, outside of API committee activities except with the approval of the Chairman of the committee having jurisdiction and staff of the API Standards Dept. Copyright API. All rights reserved.

| Washington, D.C., USA | | | | | | | | | |
|--|---------------------|-----------------------|---------------------------------|-----------------------------|-----------------|------------------------------|---------------------|---|-------|
| BPV Determination using Master Meter - Calibration Set III | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start 3 | Stop 3 | |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | 14-Feb-24 | 14-Feb-24 | |
| Fluid or Batch | RBOB | | Flow Design | Bidirectional | | Time | 8:21:18 AM | 11:21:18 AM | |
| Ch 11.1 | Products | | Wall Design | Single | | Totalizer | 2,342,501.020 | 2,343,601.020 | M3 |
| T _B | 15.0 | °C | Detector | Internal | | Fluid, Batch No. | Products | Products | |
| P _B | 0.0 | kPag | Displacer | Free Sphere | | API ₆₀ | 60.8 | 60.6 | °API |
| Master Meter | | | Wall Material | 300 SS | | P ₆₀ | 735.210 | 735.710 | kg/m3 |
| Flowmeter ID | 200 | | Rod Material | NA | | API ₁₅ | 60.7 | 60.5 | °API |
| Manufacturer | API | | GL _P | 0.000 011 16 per °C | | P ₁₅ | 735.715 | 736.216 | kg/m3 |
| Model | API-PD | | GL _D | NA per °C | | API ₂₀ | 61.7 | 61.5 | °API |
| Nominal Size | 100 mm | | E _P | 206 842 710 per kPag | | P ₂₀ | 731.158 | 731.660 | kg/m3 |
| Type | PD | | ID _P | 547.675 0 mm | | Flowrate, Q _{av} | 140.250 | 140.222 | MPH |
| Proving Result | MMF | | WT _P | 30.963 0 mm | | T _{MP_AVG} | 22.833 | 22.911 | °C |
| T _F Comp | No | | Serial No. | Bidi-SI-001 | | P _{MP_AVG} | 1294.1 | 1298.3 | kPag |
| P _F Comp | No | | Switches | 9206 to 9236 | | Trips per Run | 1 | 1 | |
| NKF | 52,834.410 5 P / M3 | | | | | Roundtrips | Runs 1-5 | Runs 1-5 | |
| Cartridge No. | API-0011 | | | | | Repeatability (r) | 0.018 | 0.017 | % |
| Density Method | | | Calibration Set Criteria | | | Allowable (r) | 0.020 | 0.020 | % |
| ρ _{obs} Method | Continuous | | ΔMMF _{SET} | ≤ 0.02 % | | (r) Pass/Fail | Pass | Pass | |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 % | | MMF | 1.000 099 0 | 1.000 154 0 | % |
| DMF | 0.999 8 | | (r) CPV _{RUN} | ≤ 0.02 % | | ΔMMF | NA | 0.006 | % |
| HYC Factor | No | | Spot Sample | | | Allowable ± ΔMMF | NA | 0.020 | % |
| API Chapter 12.4.2 | | | ρ _{60_START} | NA kg/m ³ | | ΔMMF Pass/Fail | NA | Pass | |
| SI_15 Measurement Units | | | ρ _{60_STOP} | NA kg/m ³ | | | | | |
| Sampling Method - Continuous | | | ρ _{60_SET} | NA kg/m ³ | | | | | |
| BPV - Standard Method | | | MMF _{SET} | 1.000 126 5 | | | | | |
| Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs | | | | | | | | | |
| Refined Product - Tables 5B/6B | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | | |
| ρ _{obs} | T _{dm} | P _{dm} | T _{FP_INLET} | T _{FP_OUTLET} | T _{MM} | T _{FD} | Base Density | | |
| kg/m ³ | °C | kPag | °C | °C | °C | °C | ρ _B | | |
| 729.748 | 22.906 | 1,203.0 | 22.817 | 22.889 | 22.994 | | 735.921 | Run | |
| 729.843 | 22.906 | 1,208.0 | 22.806 | 22.844 | 22.994 | | 736.011 | 1 | |
| 729.545 | 22.928 | 1,208.0 | 22.822 | 22.856 | 23.000 | | 735.734 | 2 | |
| | | | | | | | | 3 | |
| | | | | | | | | 4 | |
| | | | | | | | | 5 | |
| | | | | | | | | 6 | |
| 729.712 | 22.913 | 1,206.0 | 22.815 | 22.863 | 22.996 | | 735.889 | Avg | |
| Ch 11.1 Iteration Results | | | | | | | | | |
| N or N_i | | Q_{MM} | | P_{FP_INLET} | | P_{FP_OUTLET} | | T_{FP} and P_{FP} Values | |
| Pulses | | MPH | | kPag | | kPag | | kPag | |
| °C | | kPag | | kPag | | kPag | | kPag | |
| Gasoline, Napthene | 100,015.000 | 140.247 | 1,214.0 | 1,198.0 | 1,278.0 | 22.853 0 | 1,206.00 | Run | |
| Gasoline, Napthene | 100,018.000 | 140.248 | 1,218.0 | 1,200.0 | 1,282.0 | 22.825 0 | 1,209.00 | 1 | |
| Gasoline, Napthene | 100,022.000 | 140.247 | 1,215.0 | 1,200.0 | 1,285.0 | 22.839 0 | 1,207.50 | 2 | |
| | | | | | | | | 3 | |
| | | | | | | | | 4 | |
| | | | | | | | | 5 | |
| | | | | | | | | 6 | |
| | 100,018.300 0 | 140.247 | 1,216.0 | 1,199.0 | 1,282.0 | 22.839 0 | 1,208.00 | Avg | |

Example A.1 - Calibration Set III - 1 of 2

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|--|---|-----------------------------|---|--------------------|--------------------------|--------------------------|--------------------------------|--|---------------------------|-----------------------------|---------------------------|------------------------------|--------------------------|--------------------------|--------------------|---------------|---------------|------------------|---------------|---------------|---------------|-------|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|----|--------------------|---------------|---------------|---------------|---------------|---------------|---------------|----|----|----|----|--|---|--|----------|----------|--|----|----|----|----|--|---|---|----------|--|--|--|--|--|--|---|---------------|---------------|---------------|---------------|---------------|---------------|---------------|-----|
| BPV Determination using Master Meter - Calibration Set III | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Refined Product - Tables 5B/6B | | ΔMMF_{SET} Pass $(r) ICPV_{SET}$ Pass $(r) CPV_{SET}$ Pass | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start</td> <td style="text-align: center;">Stop</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">Start 3</td> <td style="text-align: center;">Stop 3</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">00:00:00</td> <td style="text-align: center;">00:00:00</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">2342501.02</td> <td style="text-align: center;">2343601.02</td> </tr> </tbody> </table> | | | | Prior | Current | Report No. | Start | Stop | Date | Start 3 | Stop 3 | Time | 00:00:00 | 00:00:00 | Fluid, Batch No. | 2342501.02 | 2343601.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | Date | Start 3 | Stop 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | Time | 00:00:00 | 00:00:00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | 2342501.02 | 2343601.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;">N or N_i Pulses</th> <th style="text-align: center;">NKF P / M3</th> <th style="text-align: center;">IV_{MM}</th> <th style="text-align: center;">CTL_{MM}</th> <th style="text-align: center;">CPL_{MM}</th> <th style="text-align: center;">CTPL_{MM}</th> <th style="text-align: center;">GSV_{MM} M3</th> <th style="text-align: center;">Run</th> </tr> </thead> <tbody> <tr><td>100,015.000</td><td>52,834.410 5</td><td>1.892 989 8</td><td>0.990 088 855</td><td>1.001 518 008</td><td>0.991 591 818</td><td>1.877 310 650</td><td>1</td></tr> <tr><td>100,018.000</td><td>52,834.410 5</td><td>1.893 046 6</td><td>0.990 090 711</td><td>1.001 522 097</td><td>0.991 597 725</td><td>1.877 378 160</td><td>2</td></tr> <tr><td>100,022.000</td><td>52,834.410 5</td><td>1.893 122 3</td><td>0.990 077 557</td><td>1.001 527 798</td><td>0.991 590 195</td><td>1.877 438 980</td><td>3</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>4</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>6</td></tr> <tr> <td>100,018.300 0</td> <td>52,834.410 5</td> <td>1.893 052 9</td> <td>0.990 085 708</td> <td>1.001 522 634</td> <td>0.991 593 246</td> <td>1.877 375 930</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | N or N _i Pulses | NKF P / M3 | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} M3 | Run | 100,015.000 | 52,834.410 5 | 1.892 989 8 | 0.990 088 855 | 1.001 518 008 | 0.991 591 818 | 1.877 310 650 | 1 | 100,018.000 | 52,834.410 5 | 1.893 046 6 | 0.990 090 711 | 1.001 522 097 | 0.991 597 725 | 1.877 378 160 | 2 | 100,022.000 | 52,834.410 5 | 1.893 122 3 | 0.990 077 557 | 1.001 527 798 | 0.991 590 195 | 1.877 438 980 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | 100,018.300 0 | 52,834.410 5 | 1.893 052 9 | 0.990 085 708 | 1.001 522 634 | 0.991 593 246 | 1.877 375 930 | Avg |
| N or N _i Pulses | NKF P / M3 | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,015.000 | 52,834.410 5 | 1.892 989 8 | 0.990 088 855 | 1.001 518 008 | 0.991 591 818 | 1.877 310 650 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,018.000 | 52,834.410 5 | 1.893 046 6 | 0.990 090 711 | 1.001 522 097 | 0.991 597 725 | 1.877 378 160 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,022.000 | 52,834.410 5 | 1.893 122 3 | 0.990 077 557 | 1.001 527 798 | 0.991 590 195 | 1.877 438 980 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,018.300 0 | 52,834.410 5 | 1.893 052 9 | 0.990 085 708 | 1.001 522 634 | 0.991 593 246 | 1.877 375 930 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;">Iteration Results</th> <th style="text-align: center;">CTS_{FP}</th> <th style="text-align: center;">CPS_{FP}</th> <th style="text-align: center;">CTL_{FP}</th> <th style="text-align: center;">CPL_{FP}</th> <th style="text-align: center;">CTPL_{FP}</th> <th style="text-align: center;">CPV_{run} M3</th> <th style="text-align: center;">Run</th> </tr> </thead> <tbody> <tr><td>Gasoline, Napthene</td><td>1.000 262 941</td><td>1.000 103 130</td><td>0.990 264 161</td><td>1.001 430 750</td><td>0.991 680 981</td><td>1.892 366 250</td><td>1</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 262 004</td><td>1.000 103 387</td><td>0.990 300 787</td><td>1.001 433 363</td><td>0.991 720 247</td><td>1.892 360 660</td><td>2</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 262 473</td><td>1.000 103 259</td><td>0.990 277 805</td><td>1.001 433 674</td><td>0.991 697 540</td><td>1.892 464 650</td><td>3</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>4</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>6</td></tr> <tr> <td></td> <td>1.000 262 473</td> <td>1.000 103 259</td> <td>0.990 280 917</td> <td>1.001 432 596</td> <td>0.991 699 590</td> <td>1.892 397 190</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} M3 | Run | Gasoline, Napthene | 1.000 262 941 | 1.000 103 130 | 0.990 264 161 | 1.001 430 750 | 0.991 680 981 | 1.892 366 250 | 1 | Gasoline, Napthene | 1.000 262 004 | 1.000 103 387 | 0.990 300 787 | 1.001 433 363 | 0.991 720 247 | 1.892 360 660 | 2 | Gasoline, Napthene | 1.000 262 473 | 1.000 103 259 | 0.990 277 805 | 1.001 433 674 | 0.991 697 540 | 1.892 464 650 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | | 1.000 262 473 | 1.000 103 259 | 0.990 280 917 | 1.001 432 596 | 0.991 699 590 | 1.892 397 190 | Avg |
| Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 262 941 | 1.000 103 130 | 0.990 264 161 | 1.001 430 750 | 0.991 680 981 | 1.892 366 250 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 262 004 | 1.000 103 387 | 0.990 300 787 | 1.001 433 363 | 0.991 720 247 | 1.892 360 660 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 262 473 | 1.000 103 259 | 0.990 277 805 | 1.001 433 674 | 0.991 697 540 | 1.892 464 650 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 262 473 | 1.000 103 259 | 0.990 280 917 | 1.001 432 596 | 0.991 699 590 | 1.892 397 190 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;">1 means ΔCPV Passed</th> <th style="text-align: center;">ΔP_{B_SET} kg/m³</th> <th style="text-align: center;">ΔT_{P_SET} °C</th> <th style="text-align: center;">ΔP_{P_SET} kPag</th> <th style="text-align: center;">ΔQ_{MM_SET} %</th> <th style="text-align: center;">r% CPV</th> <th style="text-align: center;">CPV_{set}</th> <th style="text-align: center;">CPV_{set} M3</th> <th></th> </tr> </thead> <tbody> <tr> <td>Runs 1-3</td> <td>1</td> <td>0.278</td> <td>0.028</td> <td>3.00</td> <td>0.0</td> <td>0.005</td> <td>Pass</td> <td>1.892 397 190</td> <td>Runs 1-3</td> </tr> <tr> <td>Runs 2-4</td> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td></td> <td>-</td> <td></td> <td>Runs 2-4</td> </tr> <tr> <td>Runs 3-5</td> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td></td> <td>-</td> <td></td> <td>Runs 3-5</td> </tr> <tr> <td>Runs 4-6</td> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td></td> <td>-</td> <td></td> <td>Runs 4-6</td> </tr> </tbody> </table> | | | | | | | | 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{MM_SET} % | r% CPV | CPV _{set} | CPV _{set} M3 | | Runs 1-3 | 1 | 0.278 | 0.028 | 3.00 | 0.0 | 0.005 | Pass | 1.892 397 190 | Runs 1-3 | Runs 2-4 | | NA | NA | NA | NA | | - | | Runs 2-4 | Runs 3-5 | | NA | NA | NA | NA | | - | | Runs 3-5 | Runs 4-6 | | NA | NA | NA | NA | | - | | Runs 4-6 | | | | | | | | | | | | | | | |
| 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{MM_SET} % | r% CPV | CPV _{set} | CPV _{set} M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 | 1 | 0.278 | 0.028 | 3.00 | 0.0 | 0.005 | Pass | 1.892 397 190 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 2-4 | | NA | NA | NA | NA | | - | | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 3-5 | | NA | NA | NA | NA | | - | | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 4-6 | | NA | NA | NA | NA | | - | | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;">Signature</th> <th style="text-align: center;">Date</th> <th style="text-align: center;">Company</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td style="text-align: center;">API Midstream Representative</td> </tr> <tr><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td></tr> </tbody> </table> | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example A.1 - Calibration Set III - 2 of 2

This document is not an API Standard; it is under consideration within an API technical committee but has not received all approvals required to become an API Standard. It shall not be reproduced or circulated or quoted, in whole or in part, outside of API committee activities except with the approval of the Chairman of the committee having jurisdiction and staff of the API Standards Dept. Copyright API. All rights reserved.

Example A.2 – Standard Method

SI Units, Spot Sampling, Master Prover - Unidirectional Captive Displacer, Master Meter - Turbine,
MF r% - Moving Range, MF Method - IMF, Field Prover - Unidirectional Captive Displacer

DRAFT

| Master Prover | | | |
|-----------------|--------------|--|--|
| BPV Units | 1 | (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) | |
| Detector Design | 1 | (0-Internal, 1-External) | |
| Wall Material | 3 | (1-CS, 2-304SS, 3-316SS, 4-17-4PH) | |
| Rod Material | 3 | (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) | |
| Certificate BPV | 93,818.781 0 | mL at 15.0 °C and 0.0 kPag | |

| Base Prover Volume (BPV) | | | |
|--------------------------|------------------------------------|-----------------------------------|-----------------------------------|
| | BPV ₆₀ Barrels | BPV ₁₅ Cubic Meters | BPV ₂₀ Cubic Meters |
| | 0.590 118 130 282 | 0.093 818 781 000 | 0.093 841 327 000 |
| Decimals | 10 | 11 | 11 |
| Conversion | in ³ / Bbl 9.702E+03 | mL / M ³ 1.00E+06 | mL / M ³ 1.00E+06 |
| Rnd'd BPV | 0.590 118 130 300 | 0.093 818 781 000 | 0.093 841 327 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to **10 digits** (the appropriate decimal place) to increase the precision of the Master Prover's BPV, not the uncertainty of the Master Prover's BPV.

| | T _B | |
|---------------------------|----------------|-----------------------------------|
| Decimal Base CTS | 15.0 | °C |
| Decimal BPV ₆₀ | 9 | - |
| Decimal BPV _{SI} | 4 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV | 3 | mL at 15.0 °C and 0.0 kPag |
| Decimal BPV | 11 | Cubic Meters |

Detector Design,

CTSP = [1 + (T_P - T_B) x GL_P]³, for detectors mounted in calibrated section

CTSP = [1 + (T_P - T_B) x GL_P]² x [1 + (T_D - T_B) x GL_D], for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F

BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig

BPV₁₅ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C

BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig

BPV₁₅ = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = ROUND(BPV₁₅ x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C

BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig

BPV₁₅ = ROUND(BPV₂₀ x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| T _B | 60.0 °F | 15.0 °C | 20.0 °C |
|-----------------|--------------|--------------|--------------|
| GL _P | 0.000 008 90 | 0.000 016 02 | 0.000 016 02 |
| GL _D | 0.000 008 90 | 0.000 016 02 | 0.000 016 02 |

| Base CTS | Base CTS ₆₀ | Base CTS ₁₅ | Base CTS ₂₀ |
|---------------|------------------------|------------------------|------------------------|
| 1.000 000 000 | 1.000 026 700 | 0.999 786 415 | |
| 0.999 973 300 | 1.000 000 000 | 0.999 759 719 | |
| 1.000 213 615 | 1.000 240 319 | 1.000 000 000 | |

| Base Unit Volume | |
|-------------------|---|
| BPV ₆₀ | 5,725.326 1 cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 93,818.781 mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 93,841.327 mL at 20.0 °C and 0.0 kPag |

| API Properties | | |
|---|------------------------------------|---------------------------------------|
| Linear Coefficient of Thermal Expansion, GL | | |
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,3,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar TM | 0.000 001 44 | 0.000 000 80 |

Notes:

(1) The User/Owner should obtain GL values from the prover manufacturer.

(2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.

(3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.

(4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.

(5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Example A.2 - Expanded Discrimination of Master Prover's BPV

| Washington, D.C., USA | | | | | | | | | | | | | | | | | |
|---|--------------------|---------------------|-----------------|---------------------|---------------------------|----------------------|----------------------|--------------------------|------------------------|----------------|----------------|------------------------|----------------|--------------------|-------------------|--|--|
| Master Meter Proving Report | | | | | | | | | | | | | | | | | |
| General Data | | | | Displacement Prover | | | | Report Summary | | | | | | | | | |
| Operator | API Midstream | | | Manufacturer | API | | | Report No. | Start | | Stop | | | | | | |
| Station Name | MPMS | | | Prover Type | Displacement | | | Date | Start I | | Stop I | | | | | | |
| Ch 11.1 | Tables 5A/6A | | | Flow Design | Unidirectional | | | | 14-Feb-24 | | 14-Feb-24 | | | | | | |
| T _B | 15.0 °C | | | Wall Design | Single | | | Time | 8:21:18 | | 11:21:18 | | | | | | |
| P _B | 0.0 kPag | | | Detector | External | | | Totalizer | 2,342,501.020 | | 2,343,601.020 | | | | | | |
| Master Meter | | | | Displacer | Captive Displacer | | | Fluid, Batch No. | Crude | | Crude | | | | | | |
| Flowmeter ID | 200 | | | Wall Material | 316SS | | | API ₆₀ | 35.1 | | 35.2 | | | | | | |
| Manufacturer | API | | | Rod Material | 316SS | | | ρ ₆₀ | 848.597 | | 848.217 | | | | | | |
| Model | Turbine | | | GL _P | 0.000 016 02 per °C | | | API ₁₅ | 35.0 | | 35.1 | | | | | | |
| Nominal Size | 75 mm | | | GL _D | 0.000 016 02 per °C | | | ρ ₁₅ | 848.999 | | 848.619 | | | | | | |
| Type | Coriolis | | | E _P | 193 053 196 per kPag | | | API ₂₀ | 35.6 | | 35.7 | | | | | | |
| Proving Result | MMF | | | ID _P | 441.960 0 mm | | | ρ ₂₀ | 845.377 | | 844.995 | | | | | | |
| T _F Comp | No | | | WT _P | 46.355 0 mm | | | Flowrate, Q | 58.025 | | 58.100 | | | | | | |
| P _F Comp | No | | | Calibration Date | 2021-09-04 | | | T _{P_AVG} | 22.874 | | 23.016 | | | | | | |
| NKF | 4,382.111 0 P / M3 | | | Serial No. | 8904-02 | | | P _{P_AVG} | 1210.6 | | 1214.2 | | | | | | |
| Cartridge No. | API-0011 | | | Certificate No. | 10101010 | | | Trips per Run | 1 | | 1 | | | | | | |
| Density Method | | | | Switches | 9201 to 9202 | | | Roundtrips | Runs 1-3 | | Runs 1-3 | | | | | | |
| Sample Method | Spot Sample | | | BPV | 0.093 818 781 0 M3 | | | Repeatability (r) | 0.004 | | 0.002 | | | | | | |
| ρ _{obs} Device | Hydrometer | | | Spot Sample | | | | Allowable (r) | 0.007 | | 0.007 | | | | | | |
| DMF | NA | | | API _{ind} | °API | | | (r) Pass/Fail | Pass | | Pass | | | | | | |
| HYC Factor | Yes | | | ρ _{ind} | 848.619 kg/m ³ | | | MMF | 0.999 997 7 | | 0.999 986 4 | | | | | | |
| API MPMS Chapter 12.4.2 Measurement Units - SI_15 Sampling Method - Spot Meter Factor Method - Intermediate (or IMF) Repeatability Method (r%) - Moving Range API MPMS Chapter 11.1 - Tables 5A/6A | | | | T _{obs} | 15.000 °C | | | ΔMMF | NA | | (0.001) | | | | | | |
| | | | | P _{obs} | 0.0 kPag | | | Allowable ± ΔMMF | NA | | 0.020 | | | | | | |
| | | | | | | | ΔMMF Pass/Fail | NA | | Pass | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | Prior vs Current | | | | | | | | | |
| | | | | | | | | ΔQ 0.1 % | | | | | | | | | |
| | | | | | | | | ΔT _P 0.142 °C | | | | | | | | | |
| Base Density | | | | | | | | | Roundtrip Measurements | | | | Base Density | | | | |
| API _B | ρ _{ind} | | T _{dm} | | P _{dm} | | T _{P_INLET} | | T _{P_OUTLET} | | T _M | | T _D | | ρ _B | | |
| °API | kg/m ³ | | °C | | kPag | | °C | | °C | | °C | | °C | | kg/m ³ | | |
| 35.1 | | | | | | | 23.044 | | 22.978 | | 22.894 | | 23.900 | | 848.619 | | |
| 35.1 | | | | | | | 23.061 | | 23.017 | | 22.933 | | 23.967 | | 848.619 | | |
| 35.1 | | | | | | | 23.039 | | 22.956 | | 22.906 | | 23.956 | | 848.619 | | |
| NA | | | | | | | | | | | | | | | | | |
| NA | | | | | | | | | | | | | | | | | |
| NA | | | | | | | | | | | | | | | | | |
| NA | | | | | | | | | | | | | | | | | |
| NA | | | | | | | | | | | | | | | | | |
| NA | | | | | | | | | | | | | | | | | |
| NA | | | | | | | | | | | | | | | | | |
| 35.1 | NA | | NA | | NA | | NA | | NA | | 22.911 | | 23.941 | | 848.619 | | |
| | | | | | | | | | | | | | Runs 1-3 | | | | |
| Commodity Type | | | | | | | | | | | | Roundtrip Measurements | | | | T _P and P _P Values | |
| | | N or N _i | | Q _M | | P _{P_INLET} | | P _{P_OUTLET} | | P _M | | T _{P_RUN} | | P _{P_RUN} | | | |
| | | Pulses | | MPH | | kPag | | kPag | | kPag | | °C | | kPag | | | |
| Crude Oil, JP-4 | | 411.278 | | 58.112 0 | | 1,227.0 | | 1,201.0 | | 1,196.0 | | 23.011 0 | | 1,214.00 | | 1 | |
| Crude Oil, JP-4 | | 411.291 | | 58.069 0 | | 1,227.0 | | 1,202.0 | | 1,197.0 | | 23.039 0 | | 1,214.50 | | 2 | |
| Crude Oil, JP-4 | | 411.294 | | 58.118 0 | | 1,227.0 | | 1,201.0 | | 1,196.0 | | 22.997 5 | | 1,214.00 | | 3 | |
| NA | | | | | | | | | | | | | | | | 4 | |
| NA | | | | | | | | | | | | | | | | 5 | |
| NA | | | | | | | | | | | | | | | | 6 | |
| NA | | | | | | | | | | | | | | | | 7 | |
| NA | | | | | | | | | | | | | | | | 8 | |
| NA | | | | | | | | | | | | | | | | 9 | |
| NA | | | | | | | | | | | | | | | | 10 | |
| Runs 1-3 | | 411.287 7 | | 58.100 0 | | NA | | NA | | 1,196.0 | | 23.015 8 | | 1,214.17 | | Runs 1-3 | |

Example A.2 - Calibration Set I - Stop Proving Report - 1 of 2

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| Washington, D.C., USA Master Meter Proving Report | | | | | | | | | | | | | | | | | | | | | | | | |
|---|--|------------------------|------------------------|---|----------------------------|-----------------------------|------------------------------|----------|--|--|-------|---------|------------|---------|--------|------|-----------|-----------|------|----------|----------|------------------|-------|-------|
| API MPMS Chapter 12.4.2 Measurement Units - SI_15 Sampling Method - Spot Meter Factor Method - Intermediate (or IMF) Repeatability Method (r%) - Moving Range API MPMS Chapter 11.1 - Tables 5A/6A | | | | Report Summary <table style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 30%;"></th> <th style="width: 35%; text-align: center;">Prior</th> <th style="width: 35%; text-align: center;">Current</th> </tr> <tr> <td>Report No.</td> <td style="text-align: center;">Start I</td> <td style="text-align: center;">Stop I</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">14-Feb-24</td> <td style="text-align: center;">14-Feb-24</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">08:21:18</td> <td style="text-align: center;">11:21:18</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">Crude</td> <td style="text-align: center;">Crude</td> </tr> </table> | | | | | | | Prior | Current | Report No. | Start I | Stop I | Date | 14-Feb-24 | 14-Feb-24 | Time | 08:21:18 | 11:21:18 | Fluid, Batch No. | Crude | Crude |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start I | Stop I | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | |
| Time | 08:21:18 | 11:21:18 | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Crude | Crude | | | | | | | | | | | | | | | | | | | | | | |
| Run | BPV M3 | CTS_p | CPS_p | Rnd CTL_p | Rnd CPL_p | Rnd CTPL_p | GSV_p M3 | Run | | | | | | | | | | | | | | | | |
| 1 | 0.093 818 781 0 | 1.000 399 304 | 1.000 059 955 | 0.993 153 177 | 1.000 925 626 | 0.994 072 465 | 0.093 305 500 9 | 1 | | | | | | | | | | | | | | | | |
| 2 | 0.093 818 781 0 | 1.000 401 274 | 1.000 059 980 | 0.993 129 388 | 1.000 926 151 | 0.994 049 176 | 0.093 303 500 9 | 2 | | | | | | | | | | | | | | | | |
| 3 | 0.093 818 781 0 | 1.000 399 768 | 1.000 059 955 | 0.993 164 595 | 1.000 925 551 | 0.994 083 820 | 0.093 306 609 9 | 3 | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | 4 | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | 5 | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | 8 | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | |
| Runs 1-3 | 0.093 818 781 0 | 1.000 400 115 | 1.000 059 963 | 0.993 149 053 | 1.000 925 776 | 0.994 068 487 | 0.093 305 203 9 | Runs 1-3 | | | | | | | | | | | | | | | | |
| Run | N or N_i | NKF P / M3 | IV_M | Rnd CTL_M | Rnd CPL_M | Rnd CTPL_M | ISV_M M3 | Run | | | | | | | | | | | | | | | | |
| 1 | 411.278 | 4,382.111 0 | 0.093 853 852 6 | 0.993 253 560 | 1.000 911 245 | 0.994 158 657 | 0.093 305 620 1 | 1 | | | | | | | | | | | | | | | | |
| 2 | 411.291 | 4,382.111 0 | 0.093 856 819 2 | 0.993 220 258 | 1.000 912 196 | 0.994 126 270 | 0.093 305 529 6 | 2 | | | | | | | | | | | | | | | | |
| 3 | 411.294 | 4,382.111 0 | 0.093 857 503 8 | 0.993 243 094 | 1.000 911 313 | 0.994 148 248 | 0.093 308 273 1 | 3 | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | 4 | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | 5 | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | 8 | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | |
| Runs 1-3 | 411.287 7 | 4,382.111 0 | 0.093 856 058 6 | 0.993 238 971 | 1.000 911 585 | 0.994 144 392 | 0.093 306 474 3 | Runs 1-3 | | | | | | | | | | | | | | | | |
| Run | *1 indicates Repeatability (r%) criteria satisfied | Repeatability (r%) | | Meter Factor Method - Intermediate (or IMF) | | | IMF | Run | | | | | | | | | | | | | | | | |
| | | Actual | Allowable | | | | | | | | | | | | | | | | | | | | | |
| 1 | | NA | NA | | | | 0.999 998 72 | 1 | | | | | | | | | | | | | | | | |
| 2 | | NA | NA | | | | 0.999 978 26 | 2 | | | | | | | | | | | | | | | | |
| 3 | 1 | 0.002 | 0.007 | Repeatability Method (r%) - Moving Range | | | 0.999 982 17 | 3 | | | | | | | | | | | | | | | | |
| 4 | | | 0.014 | | | | | 4 | | | | | | | | | | | | | | | | |
| 5 | | | 0.020 | | | | | 5 | | | | | | | | | | | | | | | | |
| 6 | | | 0.025 | | | | | 6 | | | | | | | | | | | | | | | | |
| 7 | | | 0.031 | | | | | 7 | | | | | | | | | | | | | | | | |
| 8 | | | 0.036 | | | | | 8 | | | | | | | | | | | | | | | | |
| 9 | | | 0.041 | | | | | 9 | | | | | | | | | | | | | | | | |
| 10 | | | 0.045 | | | | | 10 | | | | | | | | | | | | | | | | |
| | Pass | 0.002 | | | | | 0.999 986 40 | MMF | | | | | | | | | | | | | | | | |

MMF Rounded to 7 decimal places

| | |
|--|------------------------------|
| | API Midstream Representative |
| | |
| | |

Example A.2 - Calibration Set I - Stop Proving Report - 2 of 2

| Field Prover | | |
|--|--------------|--|
| Measurement Units | 1 | (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) |
| Detector Design | 1 | (0-Internal, 1-External) |
| Wall Material | 3 | (1-CS, 2-304SS, 3-316SS, 4-17-4PH) |
| Rod Material | 3 | (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) |
| Source for GL _{MP} , GL _{md} , E _{MP} | 1 | (0-Prover Manufacturer, 1-API Table) |
| BPV _P | 93,818.781 0 | mL at 15.0 °C and 0.0 kPag |

| Base Prover Volume (BPV) | | |
|--------------------------|---------------------|---------------------|
| BPV ₆₀ | BPV ₁₅ | BPV ₂₀ |
| Barrels | Cubic Meters | Cubic Meters |
| 0.590 118 130 282 | 0.093 818 781 000 | 0.093 841 327 000 |
| 6 | 7 | 7 |
| in ³ / Bbl | mL / M ³ | mL / M ³ |
| 9.702E+03 | 1.00E+06 | 1.00E+06 |
| Rnd'd BPV | 0.590 118 000 000 | 0.093 818 800 000 |
| | | 0.093 841 300 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to 6 digits (the appropriate decimal place).

| | T _B | |
|---------------------------|----------------|-----------------------------------|
| Decimal Base CTS | 9 | - |
| Decimal BPV ₆₀ | 4 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV _{SI} | 3 | mL at 15.0 °C and 0.0 kPag |
| Decimal BPV | 7 | Cubic Meters, 6 digits |
| Decimal BPV | 6 | Barrels, 6 digits |

Detector Design,

CTS_P = [1 + (T_P - T_B) x GL_P]³, for detectors mounted in calibrated section
 CTS_P = [1 + (T_P - T_B) x GL_P]² x [1 + (T_D - T_B) x GL_D], for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F
 BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig
 BPV₁₅ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₁₅, 12) = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₂₀, 12) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C
 BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 x Base CTS₆₀, 12) = in³ at 60.0 °F, 0.0 psig
 BPV₁₅ = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = ROUND(BPV₁₅ x Base CTS₂₀, 12) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C
 BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 x Base CTS₆₀, 12) = in³ at 60.0 °F, 0.0 psig
 BPV₁₅ = ROUND(BPV₂₀ x Base CTS₁₅, 12) = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| GL _P | 0.000 008 90 | 0.000 016 02 | 0.000 016 02 |
|-----------------|--------------|---------------|---------------|
| GL _D | 0.000 008 90 | 0.000 016 020 | 0.000 016 020 |
| T _B | 60.0 | 15.0 | 20.0 |

| | | | |
|------------------------|---------------|---------------|---------------|
| Base CTS ₆₀ | 1.000 000 000 | 1.000 026 700 | 0.999 786 415 |
| Base CTS ₁₅ | 0.999 973 300 | 1.000 000 000 | 0.999 759 719 |
| Base CTS ₂₀ | 1.000 213 615 | 1.000 240 319 | 1.000 000 000 |

| Base Unit Volume | |
|-------------------|---|
| BPV ₆₀ | 5,725.326 1 cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 93,818.781 mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 93,841.327 mL at 20.0 °C and 0.0 kPag |

API Properties

| Linear Coefficient of Thermal Expansion, GL | | |
|---|------------------------------------|---------------------------------------|
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,3,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar TM | 0.000 001 44 | 0.000 000 80 |

Notes:

(1) The User/Owner should obtain GL values from the prover manufacturer.

(2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.

(3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.

(4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.

(5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Example A.2 - Field Prover's BPV Conversion

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|-------------------|-------------------------|--------------------|-------------|---------------------|-------------------|-------------------|--|--|-------------------|--|--|--------------------|--|---------------------|--|--|--|-------|------|-------|------|-------|------|--|------------|---------|--------|---------|--------|---------|--------|---|------|-----------|-----------|-----------|-----------|-----------|-----------|---|-------|-------|-------|-------|-------|-------|-------|---|------------------|------|------|------|------|------|------|------|----------------|---------|---------|---------|---------|---------|---------|-------------------|-----------------|--------|--------|--------|--------|---------|---------|-----|---------------------|--------|--------|--------|--------|--------|--------|----|---------------------|---------|---------|---------|---------|---------|---------|------|------------|----------|----------|----------|----------|----------|----------|---|-------------------|-------|-------|-------|-------|-------|-------|---|-----|-------------|-------------|-------------|-------------|-------------|-------------|---|--------------------|----|-------------|----|-------------|----|-------------|---|------|----|---------|----|-------|----|-------|---|---------------------|--|------|------|--|------|--|--|------------------------|--|------|------|--|------|--|--|------------------------|--|----|------|--|------|--|--|-------------------|--|----|------|--|------|--|--|--------------|--|----------|----------|--|----------|--|--|--------------------|--|-------------|-------------|--|-------------|--|--|----------------------|--|------|------|--|------|--|------|--------------------|--|---------|---------|--|---------|--|-------------------|---------------------|--|--------|--------|--|--------|--|----|---------------------|--|---------|---------|--|---------|--|------|---------------------|--|---------|--------|--|---------|--|-----|---------------------|--|---------|-------|--|-------|--|---|---------------------|--|-------|---------|--|-------|--|-------------------|---------------------|--|-------|-------|--|-------|--|----|---------------------|--|-----|-----|--|-----|--|------|----------------------|--|-----|-----|--|-----|--|---|----------------------------|--|----|--------|--|------|--|---|------------------------|--|-------|-------|--|-------|--|---|------------------------|--|----|-------|--|-------|--|---|
| BPV Determination using a Master Meter - Standard Method | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| General Data | | Master Meter | | | | Field Prover | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Midstream | Operator | Flowmeter ID | 200 | - | Manufacturer | API | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Headquarters | Station Name | Manufacturer | API | - | Prover Design | Displacement | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Washington | City, Town | Model | Turbine | - | Flow Design | Unidirectional | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| D.C. | State, Province | Nominal Size | 75 | mm | Wall Design | Single | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| USA | Country | Type | Turbine | - | Detector | External | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude | Fluid, Batch No. | Proving Result | MMF | - | Displacer | Captive Displacer | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude | Ch 11.1 | T _F Comp | No | - | Wall Material | 316SS | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15.0 | T _B | P _F Comp | No | - | Rod Material | 316SS | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.0 | P _B | NKF | 4,382.111 0 | P / M3 | GL _P | 0.000 016 02 | per °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14-Feb-2024 | Start Calibration | Cartridge No. | API-0011 | - | GL _D | 0.000 016 02 | per °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14-Feb-2024 | Stop Calibration | | | - | E _P | 193 053 196 | per kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, r ≤ 0.02%, for 3 consecutive Calibration Sets Crude Oil - Tables 5A/6A | | ρ _{obs} Method | Spot Sample | - | ID _P | 441.960 0 | mm | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | ρ _{obs} Device | Online Density | - | WT _P | 46.355 0 | mm | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | DMF | 0.000 0 | - | Trips per Run | 1 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | HYC Factor | No | - | Serial No. | 8904-02 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | - | Switches | 9201 to 9202 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | Density Method | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table><thead><tr><th colspan="3">Calibration Set I</th><th colspan="2">Calibration Set II</th><th colspan="2">Calibration Set III</th><th></th></tr><tr><th></th><th>Start</th><th>Stop</th><th>Start</th><th>Stop</th><th>Start</th><th>Stop</th><th></th></tr></thead><tbody><tr><td>Report No.</td><td>Start I</td><td>Stop I</td><td>Start 2</td><td>Stop 2</td><td>Start 3</td><td>Stop 3</td><td>-</td></tr><tr><td>Date</td><td>14-Feb-24</td><td>14-Feb-24</td><td>14-Feb-24</td><td>14-Feb-24</td><td>14-Feb-24</td><td>14-Feb-24</td><td>-</td></tr><tr><td>Crude</td><td>Crude</td><td>Crude</td><td>Crude</td><td>Crude</td><td>Crude</td><td>Crude</td><td>-</td></tr><tr><td>API_B</td><td>35.0</td><td>35.1</td><td>35.1</td><td>35.0</td><td>35.1</td><td>35.1</td><td>°API</td></tr><tr><td>ρ_B</td><td>848.999</td><td>848.619</td><td>848.619</td><td>848.989</td><td>848.829</td><td>848.789</td><td>kg/m³</td></tr><tr><td>Q_{MM}</td><td>58.025</td><td>58.100</td><td>83.332</td><td>83.434</td><td>140.250</td><td>140.222</td><td>MPH</td></tr><tr><td>T_{MP_AVG}</td><td>22.874</td><td>23.016</td><td>21.506</td><td>21.517</td><td>22.833</td><td>22.911</td><td>°C</td></tr><tr><td>P_{MP_AVG}</td><td>1,210.6</td><td>1,214.2</td><td>1,303.8</td><td>1,306.6</td><td>1,294.1</td><td>1,298.3</td><td>kPag</td></tr><tr><td>Roundtrips</td><td>Runs 1-3</td><td>Runs 1-3</td><td>Runs 1-5</td><td>Runs 1-5</td><td>Runs 1-5</td><td>Runs 1-5</td><td>-</td></tr><tr><td>Repeatability (r)</td><td>0.004</td><td>0.002</td><td>0.011</td><td>0.008</td><td>0.008</td><td>0.014</td><td>%</td></tr><tr><td>MMF</td><td>0.999 997 7</td><td>0.999 986 4</td><td>1.000 055 2</td><td>1.000 058 6</td><td>0.999 845 2</td><td>0.999 865 5</td><td>-</td></tr><tr><td>MMF_{SET}</td><td>NA</td><td>0.999 992 1</td><td>NA</td><td>1.000 056 9</td><td>NA</td><td>0.999 855 4</td><td>-</td></tr><tr><td>ΔMMF</td><td>NA</td><td>(0.001)</td><td>NA</td><td>0.000</td><td>NA</td><td>0.002</td><td>%</td></tr><tr><td colspan="2">ΔMMF_{SET}</td><td>Pass</td><td colspan="2">Pass</td><td colspan="2">Pass</td><td></td></tr><tr><td colspan="2">(r) CPV_{RUN}</td><td>Pass</td><td colspan="2">Pass</td><td colspan="2">Pass</td><td></td></tr><tr><td colspan="2">(R) CPV_{SET}</td><td>NA</td><td colspan="2">Pass</td><td colspan="2">Pass</td><td></td></tr><tr><td colspan="2">ΔQ_{SET}</td><td>NA</td><td colspan="2">Pass</td><td colspan="2">Pass</td><td></td></tr><tr><td colspan="2">Selected Set</td><td>Runs 4-6</td><td colspan="2">Runs 1-3</td><td colspan="2">Runs 1-3</td><td></td></tr><tr><td colspan="2">CPV_{SET}</td><td>0.093 817 2</td><td colspan="2">0.093 820 1</td><td colspan="2">0.093 820 3</td><td></td></tr><tr><td colspan="2">API_{B_SET}</td><td>35.1</td><td colspan="2">35.1</td><td colspan="2">35.1</td><td>°API</td></tr><tr><td colspan="2">ρ_{B_SET}</td><td>848.809</td><td colspan="2">848.804</td><td colspan="2">848.809</td><td>kg/m³</td></tr><tr><td colspan="2">T_{FP_SET}</td><td>22.820</td><td colspan="2">21.442</td><td colspan="2">22.839</td><td>°C</td></tr><tr><td colspan="2">P_{FP_SET}</td><td>1,212.0</td><td colspan="2">1,280.0</td><td colspan="2">1,208.0</td><td>kPag</td></tr><tr><td colspan="2">Q_{MM_SET}</td><td>111.456</td><td colspan="2">83.332</td><td colspan="2">140.247</td><td>MPH</td></tr><tr><td colspan="2">ΔMMF_{SET}</td><td>(0.001)</td><td colspan="2">0.000</td><td colspan="2">0.002</td><td>%</td></tr><tr><td colspan="2">Δρ_{B_SET}</td><td>0.075</td><td colspan="2">(0.073)</td><td colspan="2">0.008</td><td>kg/m³</td></tr><tr><td colspan="2">ΔT_{P_SET}</td><td>0.005</td><td colspan="2">0.028</td><td colspan="2">0.028</td><td>°C</td></tr><tr><td colspan="2">ΔP_{P_SET}</td><td>2.0</td><td colspan="2">7.0</td><td colspan="2">3.0</td><td>kPag</td></tr><tr><td colspan="2">ΔQ_{MM_SET}</td><td>0.0</td><td colspan="2">0.0</td><td colspan="2">0.0</td><td>%</td></tr><tr><td colspan="2">ΔQ_{between SETS}</td><td>NA</td><td colspan="2">(25.2)</td><td colspan="2">40.6</td><td>%</td></tr><tr><td colspan="2">(r) CPV_{RUN}</td><td>0.006</td><td colspan="2">0.007</td><td colspan="2">0.001</td><td>%</td></tr><tr><td colspan="2">(R) CPV_{SET}</td><td>NA</td><td colspan="2">0.003</td><td colspan="2">0.000</td><td>%</td></tr></tbody></table> | | | | | | | | | | Calibration Set I | | | Calibration Set II | | Calibration Set III | | | | Start | Stop | Start | Stop | Start | Stop | | Report No. | Start I | Stop I | Start 2 | Stop 2 | Start 3 | Stop 3 | - | Date | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | - | Crude | Crude | Crude | Crude | Crude | Crude | Crude | - | API _B | 35.0 | 35.1 | 35.1 | 35.0 | 35.1 | 35.1 | °API | ρ _B | 848.999 | 848.619 | 848.619 | 848.989 | 848.829 | 848.789 | kg/m ³ | Q _{MM} | 58.025 | 58.100 | 83.332 | 83.434 | 140.250 | 140.222 | MPH | T _{MP_AVG} | 22.874 | 23.016 | 21.506 | 21.517 | 22.833 | 22.911 | °C | P _{MP_AVG} | 1,210.6 | 1,214.2 | 1,303.8 | 1,306.6 | 1,294.1 | 1,298.3 | kPag | Roundtrips | Runs 1-3 | Runs 1-3 | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | - | Repeatability (r) | 0.004 | 0.002 | 0.011 | 0.008 | 0.008 | 0.014 | % | MMF | 0.999 997 7 | 0.999 986 4 | 1.000 055 2 | 1.000 058 6 | 0.999 845 2 | 0.999 865 5 | - | MMF _{SET} | NA | 0.999 992 1 | NA | 1.000 056 9 | NA | 0.999 855 4 | - | ΔMMF | NA | (0.001) | NA | 0.000 | NA | 0.002 | % | ΔMMF _{SET} | | Pass | Pass | | Pass | | | (r) CPV _{RUN} | | Pass | Pass | | Pass | | | (R) CPV _{SET} | | NA | Pass | | Pass | | | ΔQ _{SET} | | NA | Pass | | Pass | | | Selected Set | | Runs 4-6 | Runs 1-3 | | Runs 1-3 | | | CPV _{SET} | | 0.093 817 2 | 0.093 820 1 | | 0.093 820 3 | | | API _{B_SET} | | 35.1 | 35.1 | | 35.1 | | °API | ρ _{B_SET} | | 848.809 | 848.804 | | 848.809 | | kg/m ³ | T _{FP_SET} | | 22.820 | 21.442 | | 22.839 | | °C | P _{FP_SET} | | 1,212.0 | 1,280.0 | | 1,208.0 | | kPag | Q _{MM_SET} | | 111.456 | 83.332 | | 140.247 | | MPH | ΔMMF _{SET} | | (0.001) | 0.000 | | 0.002 | | % | Δρ _{B_SET} | | 0.075 | (0.073) | | 0.008 | | kg/m ³ | ΔT _{P_SET} | | 0.005 | 0.028 | | 0.028 | | °C | ΔP _{P_SET} | | 2.0 | 7.0 | | 3.0 | | kPag | ΔQ _{MM_SET} | | 0.0 | 0.0 | | 0.0 | | % | ΔQ _{between SETS} | | NA | (25.2) | | 40.6 | | % | (r) CPV _{RUN} | | 0.006 | 0.007 | | 0.001 | | % | (R) CPV _{SET} | | NA | 0.003 | | 0.000 | | % |
| Calibration Set I | | | Calibration Set II | | Calibration Set III | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Start | Stop | Start | Stop | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start I | Stop I | Start 2 | Stop 2 | Start 3 | Stop 3 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude | Crude | Crude | Crude | Crude | Crude | Crude | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API _B | 35.0 | 35.1 | 35.1 | 35.0 | 35.1 | 35.1 | °API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ _B | 848.999 | 848.619 | 848.619 | 848.989 | 848.829 | 848.789 | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Q _{MM} | 58.025 | 58.100 | 83.332 | 83.434 | 140.250 | 140.222 | MPH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| T _{MP_AVG} | 22.874 | 23.016 | 21.506 | 21.517 | 22.833 | 22.911 | °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P _{MP_AVG} | 1,210.6 | 1,214.2 | 1,303.8 | 1,306.6 | 1,294.1 | 1,298.3 | kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrips | Runs 1-3 | Runs 1-3 | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Repeatability (r) | 0.004 | 0.002 | 0.011 | 0.008 | 0.008 | 0.014 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MMF | 0.999 997 7 | 0.999 986 4 | 1.000 055 2 | 1.000 058 6 | 0.999 845 2 | 0.999 865 5 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MMF _{SET} | NA | 0.999 992 1 | NA | 1.000 056 9 | NA | 0.999 855 4 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF | NA | (0.001) | NA | 0.000 | NA | 0.002 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF _{SET} | | Pass | Pass | | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) CPV _{RUN} | | Pass | Pass | | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (R) CPV _{SET} | | NA | Pass | | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔQ _{SET} | | NA | Pass | | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Selected Set | | Runs 4-6 | Runs 1-3 | | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| CPV _{SET} | | 0.093 817 2 | 0.093 820 1 | | 0.093 820 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API _{B_SET} | | 35.1 | 35.1 | | 35.1 | | °API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ _{B_SET} | | 848.809 | 848.804 | | 848.809 | | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| T _{FP_SET} | | 22.820 | 21.442 | | 22.839 | | °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P _{FP_SET} | | 1,212.0 | 1,280.0 | | 1,208.0 | | kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Q _{MM_SET} | | 111.456 | 83.332 | | 140.247 | | MPH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF _{SET} | | (0.001) | 0.000 | | 0.002 | | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Δρ _{B_SET} | | 0.075 | (0.073) | | 0.008 | | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔT _{P_SET} | | 0.005 | 0.028 | | 0.028 | | °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔP _{P_SET} | | 2.0 | 7.0 | | 3.0 | | kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔQ _{MM_SET} | | 0.0 | 0.0 | | 0.0 | | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔQ _{between SETS} | | NA | (25.2) | | 40.6 | | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) CPV _{RUN} | | 0.006 | 0.007 | | 0.001 | | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (R) CPV _{SET} | | NA | 0.003 | | 0.000 | | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

This document is not an API Standard; it is under consideration within an API technical committee but has not received all approvals required to become an API Standard. It shall not be reproduced or circulated or quoted, in whole or in part, outside of API committee activities except with the approval of the Chairman of the committee having jurisdiction and staff of the API Standards Dept. Copyright API. All rights reserved.

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|----------------------|---|--|----------|------------------------------|--------------|--------------------|-------------|------|--------------------|-------------|---------|-------|------------------|-------|---------|---------|---|----------------------------|----------------|-------------|-------------------|-------------|---|---|------------|----------------------------|-------------------|---------------------|----------------------------|--------------|-----|---------------|--------------|-------------|----------------|-------------|--------|----------|----------|-----------|-------------------|---------------|-------|--------------|-------|-----------------|---------------------|-----------------|---------------------|----------------|----------------------|-----------------|--------------|-----------------|-------------|------------|---------|----------|--------------|
| BPV Determination using a Master Meter - Standard Method | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| General Data <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="width: 20%;">API Midstream</td><td>Operator</td></tr> <tr><td>Headquarters</td><td>Station Name</td></tr> <tr><td>Washington</td><td>City, Town</td></tr> <tr><td>D.C.</td><td>State, Province</td></tr> <tr><td>USA</td><td>Country</td></tr> <tr><td>Crude</td><td>Fluid, Batch No.</td></tr> <tr><td>Crude</td><td>Ch 11.1</td></tr> <tr><td>15.0</td><td>T_B</td></tr> <tr><td>0.0</td><td>P_B</td></tr> <tr><td>14-Feb-2024</td><td>Start Calibration</td></tr> <tr><td>14-Feb-2024</td><td>Stop Calibration</td></tr> </table> | | | API Midstream | Operator | Headquarters | Station Name | Washington | City, Town | D.C. | State, Province | USA | Country | Crude | Fluid, Batch No. | Crude | Ch 11.1 | 15.0 | T _B | 0.0 | P _B | 14-Feb-2024 | Start Calibration | 14-Feb-2024 | Stop Calibration | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td colspan="2" style="text-align: center;">Field Prover</td></tr> <tr><td style="width: 30%;">Manufacturer</td><td>API</td></tr> <tr><td>Prover Design</td><td>Displacement</td></tr> <tr><td>Flow Design</td><td>Unidirectional</td></tr> <tr><td>Wall Design</td><td>Single</td></tr> <tr><td>Detector</td><td>External</td></tr> <tr><td>Displacer</td><td>Captive Displacer</td></tr> <tr><td>Wall Material</td><td>316SS</td></tr> <tr><td>Rod Material</td><td>316SS</td></tr> <tr><td>GL_P</td><td>0.000 016 02 per °C</td></tr> <tr><td>GL_D</td><td>0.000 016 02 per °C</td></tr> <tr><td>E_P</td><td>193 053 196 per kPag</td></tr> <tr><td>ID_P</td><td>441.960 0 mm</td></tr> <tr><td>WT_P</td><td>46.355 0 mm</td></tr> <tr><td>Serial No.</td><td>8904-02</td></tr> <tr><td>Switches</td><td>9201 to 9202</td></tr> </table> | | | | Field Prover | | Manufacturer | API | Prover Design | Displacement | Flow Design | Unidirectional | Wall Design | Single | Detector | External | Displacer | Captive Displacer | Wall Material | 316SS | Rod Material | 316SS | GL _P | 0.000 016 02 per °C | GL _D | 0.000 016 02 per °C | E _P | 193 053 196 per kPag | ID _P | 441.960 0 mm | WT _P | 46.355 0 mm | Serial No. | 8904-02 | Switches | 9201 to 9202 |
| API Midstream | Operator | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Headquarters | Station Name | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Washington | City, Town | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| D.C. | State, Province | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| USA | Country | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude | Fluid, Batch No. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude | Ch 11.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 15.0 | T _B | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.0 | P _B | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14-Feb-2024 | Start Calibration | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14-Feb-2024 | Stop Calibration | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Field Prover | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Manufacturer | API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Prover Design | Displacement | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow Design | Unidirectional | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Wall Design | Single | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Detector | External | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Displacer | Captive Displacer | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Wall Material | 316SS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Rod Material | 316SS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GL _P | 0.000 016 02 per °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GL _D | 0.000 016 02 per °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| E _P | 193 053 196 per kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ID _P | 441.960 0 mm | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| WT _P | 46.355 0 mm | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Serial No. | 8904-02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Switches | 9201 to 9202 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <div style="background-color: black; color: white; padding: 5px; font-size: 0.8em;"> API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, $r \leq 0.02\%$, for 3 consecutive Calibration Sets Crude Oil - Tables 5A/6A </div> | | | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="width: 20%;">BPV_{NEW}</td><td>0.093 819 2</td><td>M3</td></tr> <tr><td>BPV_{OLD}</td><td>0.093 818 8</td><td>M3</td></tr> <tr><td>ΔBPV</td><td>0.000 000 4</td><td>M3</td></tr> <tr><td>ΔBPV</td><td>0.000 4</td><td>% BPV_{NEW} Bigger / (Smaller)</td></tr> </table> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="width: 20%;">Average CPV_{SET}</td><td>0.093 819 217</td><td>M3</td></tr> </table> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td style="width: 20%;">BPV₆₀</td><td>5,725.352 8</td><td>in³ at 60.0 °F and 0.0 psig</td></tr> <tr><td>BPV₁₅</td><td>93,819.217</td><td>mL at 15.0 °C and 0.0 kPag</td></tr> <tr><td>BPV₂₀</td><td>93,841.764</td><td>mL at 20.0 °C and 0.0 kPag</td></tr> </table> | | | | BPV _{NEW} | 0.093 819 2 | M3 | BPV _{OLD} | 0.093 818 8 | M3 | ΔBPV | 0.000 000 4 | M3 | ΔBPV | 0.000 4 | % BPV _{NEW} Bigger / (Smaller) | Average CPV _{SET} | 0.093 819 217 | M3 | BPV ₆₀ | 5,725.352 8 | in ³ at 60.0 °F and 0.0 psig | BPV ₁₅ | 93,819.217 | mL at 15.0 °C and 0.0 kPag | BPV ₂₀ | 93,841.764 | mL at 20.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV _{NEW} | 0.093 819 2 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV _{OLD} | 0.093 818 8 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔBPV | 0.000 000 4 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔBPV | 0.000 4 | % BPV _{NEW} Bigger / (Smaller) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Average CPV _{SET} | 0.093 819 217 | M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₆₀ | 5,725.352 8 | in ³ at 60.0 °F and 0.0 psig | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₁₅ | 93,819.217 | mL at 15.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₂₀ | 93,841.764 | mL at 20.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Base Prover Volume (BPV _{NEW}) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₆₀ | | | BPV ₁₅ | | BPV ₂₀ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Barrels | U.S. Gallons | Cubic Feet | Cubic Meters | Liters | Cubic Meters | Liters | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | 24.785 1 | - | - | 93.819 2 | - | 93.841 8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | 3.313 28 | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.590 121 | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | 0.093 819 2 | - | 0.093 841 8 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Note: The BPV _{NEW} values (BPV ₆₀ , BPV ₁₅ , BPV ₂₀) shown are reported to 6 significant digits (10 ppm, or, 0.001%). | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | | | Date | | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example A.2 - Calibration Report Summary - 2 of 2

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| Washington, D.C., USA | | | | | | | | | |
|--|---------------------|-----------------|---------------------------------|---------------------------------------|----------------|---------------------------|--------------------|-------------------|-------------------|
| BPV Determination using Master Meter - Calibration Set I | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start I | Stop I | |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | 14-Feb-24 | 14-Feb-24 | |
| Fluid or Batch | Crude | | Flow Design | Unidirectional | | Time | 8:21:18 AM | 11:21:18 AM | |
| Ch 11.1 | Crude | | Wall Design | Single | | Totalizer | 2,342,501.020 | 2,343,601.020 | M3 |
| T _B | 15.0 °C | | Detector | External | | Fluid, Batch No. | Crude | Crude | |
| P _B | 0.0 kPag | | Displacer | Captive Displacer | | API ₆₀ | 35.1 | 35.2 | °API |
| Master Meter | | | Wall Material | 316SS | | ρ ₆₀ | 848.597 | 848.217 | kg/m ³ |
| Flowmeter ID | 200 | | Rod Material | Invar | | API ₁₅ | 35.0 | 35.1 | °API |
| Manufacturer | API | | GL _P | 0.000 016 02 per °C | | ρ ₁₅ | 848.999 | 848.619 | kg/m ³ |
| Model | Turbine | | GL _D | 0.000 016 02 per °C | | API ₂₀ | 35.6 | 35.7 | °API |
| Nominal Size | 75 mm | | E _P | 193 053 196 per kPag | | ρ ₂₀ | 845.377 | 844.995 | kg/m ³ |
| Type | Turbine | | ID _P | 441.960 0 mm | | Flowrate, Q _{av} | 58.025 | 58.100 | MPH |
| Proving Result | MMF | | WT _P | 46.355 0 mm | | T _{MP_AVG} | 22.874 | 23.016 | °C |
| T _F Comp | No | | Serial No. | 8904-02 | | P _{MP_AVG} | 1210.6 | 1214.2 | kPag |
| P _F Comp | No | | Switches | 9201 to 9202 | | Trips per Run | 1 | 1 | |
| NKF | 4,382.111 0 P / M3 | | | | | Roundtrips | Runs 1-3 | Runs 1-3 | |
| Cartridge No. | API-0011 | | | | | Repeatability (r) | 0.004 | 0.002 | % |
| Density Method | | | Calibration Set Criteria | | | Allowable (r) | 0.007 | 0.007 | % |
| ρ _{obs} Method | Spot Sample | | ΔMMF _{SET} | ≤ 0.02 % | | (r) Pass/Fail | Pass | Pass | |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 % | | MMF | 0.999 997 7 | 0.999 986 4 | |
| DMF | 0.000 0 | | (r) CPV _{RUN} | ≤ 0.02 % | | ΔMMF | NA | (0.001) | % |
| HYC Factor | No | | Spot Sample | | | Allowable ± ΔMMF | NA | 0.020 | % |
| API Chapter 12.4.2 | | | ρ _{60_START} | 848.597 000 000 000 kg/m ³ | | ΔMMF Pass/Fail | NA | Pass | |
| SI_15 Measurement Units | | | ρ _{60_STOP} | 848.216 823 342 456 kg/m ³ | | | | | |
| Sampling Method - Spot | | | ρ _{60_SET} | 848.406 911 671 228 kg/m ³ | | | | | |
| BPV - Standard Method | | | MMF _{SET} | 0.999 992 1 | | | | | |
| Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs | | | | | | | | | |
| Crude Oil - Tables 5A/6A | | | | | | | | | |
| Prior vs Current | | | | | | | | | |
| | | | | | | ΔQ _{av} | 0.02 | % | |
| | | | | | | ΔT _P | 0.222 | °C | |
| Roundtrip Measurements | | | | | | | | | |
| ρ _{obs} | T _{dm} | P _{dm} | T _{P_INLET} | T _{P_OUTLET} | T _M | T _D | Base Density | | |
| kg/m ³ | °C | kPag | °C | °C | °C | °C | ρ _B | kg/m ³ | Run |
| | | | 23.044 | 22.978 | 22.894 | 23.900 | 848.809 | | 1 |
| | | | 23.061 | 23.017 | 22.933 | 23.967 | 848.809 | | 2 |
| | | | 23.039 | 22.956 | 22.906 | 23.956 | 848.809 | | 3 |
| | | | 22.817 | 22.817 | 23.000 | 23.900 | 848.809 | | 4 |
| | | | 22.811 | 22.828 | 23.056 | 23.967 | 848.809 | | 5 |
| | | | 22.811 | 22.833 | 23.011 | 23.956 | 848.809 | | 6 |
| | | | 22.931 | 22.905 | 22.967 | 23.941 | 848.809 | | Avg |
| Roundtrip Measurements | | | | | | | | | |
| Ch 11.1 Iteration Results | N or N _i | Q _M | P _{P_INLET} | P _{P_OUTLET} | P _M | T _{P_RUN} | P _{P_RUN} | | |
| | Pulses | MPH | kPag | kPag | kPag | °C | kPag | | Run |
| Crude Oil, JP-4 | 411.103 | 111.468 | 1,214.0 | 1,198.0 | 1,278.0 | 23.011 0 | 1,206.00 | | 1 |
| Crude Oil, JP-4 | 411.174 | 111.447 | 1,218.0 | 1,200.0 | 1,282.0 | 23.039 0 | 1,209.00 | | 2 |
| Crude Oil, JP-4 | 411.383 | 111.449 | 1,215.0 | 1,200.0 | 1,285.0 | 22.997 5 | 1,207.50 | | 3 |
| Crude Oil, JP-4 | 411.357 | 111.452 | 1,219.0 | 1,202.0 | 1,285.0 | 22.817 0 | 1,210.50 | | 4 |
| Crude Oil, JP-4 | 411.353 | 111.450 | 1,220.0 | 1,204.0 | 1,287.0 | 22.819 5 | 1,212.00 | | 5 |
| Crude Oil, JP-4 | 411.358 | 111.466 | 1,220.0 | 1,205.0 | 1,279.0 | 22.822 0 | 1,212.50 | | 6 |
| | 411.288 0 | 111.456 | 1,218.0 | 1,202.0 | 1,283.0 | 22.918 0 | 1,210.00 | | Avg |

Example A.2 - Calibration Set I - 1 of 2

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|---|--|------------------------------|-----------------------------|--------------------------|-------------------|--|--------------------------|--------------------------------|--|---------------------------|-----------------------------|--------------------------|------------------------------|--------------------------|--------------------------|-----------------|---------------|---------------|---------------|------------------|---------------|---------------|---|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|-------|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|-----|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|------|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|---|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|---|-----------|---------------|---------------|---------------|---------------|---------------|---------------|-----|
| BPV Determination using Master Meter - Calibration Set I | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Crude Oil - Tables 5A/6A | <div style="display: flex; justify-content: space-between;"> <div> ΔMMF_{SET} Pass $(r) ICPV_{RUN}$ Pass $(r) CPV_{RUN}$ Pass </div> <div style="border-left: 1px solid black; padding-left: 10px;">-</div> </div> | | | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start</td> <td style="text-align: center;">Stop</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">14-Feb-24</td> <td style="text-align: center;">14-Feb-24</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">08:21:18</td> <td style="text-align: center;">11:21:18</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">Crude</td> <td style="text-align: center;">Crude</td> </tr> </tbody> </table> | | | Prior | Current | Report No. | Start | Stop | Date | 14-Feb-24 | 14-Feb-24 | Time | 08:21:18 | 11:21:18 | Fluid, Batch No. | Crude | Crude | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 08:21:18 | 11:21:18 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Crude | Crude | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>N or N_i Pulses</th> <th>NKF P / M3</th> <th>IV_M</th> <th>CTL_M</th> <th>CPL_M</th> <th>CTPL_M</th> <th style="background-color: #f4a460;">GSV_M M3</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>411.103</td><td>4,382.111 0</td><td>0.093 813 9</td><td>0.993 256 491</td><td>1.000 973 171</td><td>0.994 223 099</td><td>0.093 271 210</td><td>1</td></tr> <tr><td>411.174</td><td>4,382.111 0</td><td>0.093 830 1</td><td>0.993 223 109</td><td>1.000 976 451</td><td>0.994 192 942</td><td>0.093 284 486</td><td>2</td></tr> <tr><td>411.383</td><td>4,382.111 0</td><td>0.093 877 8</td><td>0.993 246 220</td><td>1.000 978 578</td><td>0.994 218 188</td><td>0.093 334 279</td><td>3</td></tr> <tr><td>411.357</td><td>4,382.111 0</td><td>0.093 871 9</td><td>0.993 165 759</td><td>1.000 979 136</td><td>0.994 138 203</td><td>0.093 320 905</td><td>4</td></tr> <tr><td>411.353</td><td>4,382.111 0</td><td>0.093 871 0</td><td>0.993 117 823</td><td>1.000 980 994</td><td>0.994 092 066</td><td>0.093 315 679</td><td>5</td></tr> <tr><td>411.358</td><td>4,382.111 0</td><td>0.093 872 1</td><td>0.993 156 343</td><td>1.000 974 624</td><td>0.994 124 298</td><td>0.093 319 798</td><td>6</td></tr> <tr><td>411.288 0</td><td>4,382.111 0</td><td>0.093 856 1</td><td>0.993 194 291</td><td>1.000 977 159</td><td>0.994 164 800</td><td>0.093 307 726</td><td>Avg</td></tr> </tbody> </table> | | | | | | | | N or N _i Pulses | NKF P / M3 | IV _M | CTL _M | CPL _M | CTPL _M | GSV _M M3 | Run | 411.103 | 4,382.111 0 | 0.093 813 9 | 0.993 256 491 | 1.000 973 171 | 0.994 223 099 | 0.093 271 210 | 1 | 411.174 | 4,382.111 0 | 0.093 830 1 | 0.993 223 109 | 1.000 976 451 | 0.994 192 942 | 0.093 284 486 | 2 | 411.383 | 4,382.111 0 | 0.093 877 8 | 0.993 246 220 | 1.000 978 578 | 0.994 218 188 | 0.093 334 279 | 3 | 411.357 | 4,382.111 0 | 0.093 871 9 | 0.993 165 759 | 1.000 979 136 | 0.994 138 203 | 0.093 320 905 | 4 | 411.353 | 4,382.111 0 | 0.093 871 0 | 0.993 117 823 | 1.000 980 994 | 0.994 092 066 | 0.093 315 679 | 5 | 411.358 | 4,382.111 0 | 0.093 872 1 | 0.993 156 343 | 1.000 974 624 | 0.994 124 298 | 0.093 319 798 | 6 | 411.288 0 | 4,382.111 0 | 0.093 856 1 | 0.993 194 291 | 1.000 977 159 | 0.994 164 800 | 0.093 307 726 | Avg |
| N or N _i Pulses | NKF P / M3 | IV _M | CTL _M | CPL _M | CTPL _M | GSV _M M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.103 | 4,382.111 0 | 0.093 813 9 | 0.993 256 491 | 1.000 973 171 | 0.994 223 099 | 0.093 271 210 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.174 | 4,382.111 0 | 0.093 830 1 | 0.993 223 109 | 1.000 976 451 | 0.994 192 942 | 0.093 284 486 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.383 | 4,382.111 0 | 0.093 877 8 | 0.993 246 220 | 1.000 978 578 | 0.994 218 188 | 0.093 334 279 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.357 | 4,382.111 0 | 0.093 871 9 | 0.993 165 759 | 1.000 979 136 | 0.994 138 203 | 0.093 320 905 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.353 | 4,382.111 0 | 0.093 871 0 | 0.993 117 823 | 1.000 980 994 | 0.994 092 066 | 0.093 315 679 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.358 | 4,382.111 0 | 0.093 872 1 | 0.993 156 343 | 1.000 974 624 | 0.994 124 298 | 0.093 319 798 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.288 0 | 4,382.111 0 | 0.093 856 1 | 0.993 194 291 | 1.000 977 159 | 0.994 164 800 | 0.093 307 726 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Iteraton Results</th> <th>CTS_p</th> <th>CPS_p</th> <th>CTL_p</th> <th>CPL_p</th> <th>CTPL_p</th> <th style="background-color: #f4a460;">CPV_{run} M3</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>Crude Oil, JP-4</td><td>1.000 399 304</td><td>1.000 059 560</td><td>0.993 156 343</td><td>1.000 918 946</td><td>0.994 069 000</td><td>0.093 784 665</td><td>1</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 401 274</td><td>1.000 059 708</td><td>0.993 132 375</td><td>1.000 921 390</td><td>0.994 047 438</td><td>0.093 799 851</td><td>2</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 399 768</td><td>1.000 059 634</td><td>0.993 167 899</td><td>1.000 920 014</td><td>0.994 081 628</td><td>0.093 846 839</td><td>3</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 393 086</td><td>1.000 059 783</td><td>0.993 322 397</td><td>1.000 921 293</td><td>0.994 237 538</td><td>0.093 819 290</td><td>4</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 394 240</td><td>1.000 059 857</td><td>0.993 320 257</td><td>1.000 922 450</td><td>0.994 236 545</td><td>0.093 814 015</td><td>5</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 394 144</td><td>1.000 059 881</td><td>0.993 318 118</td><td>1.000 922 845</td><td>0.994 234 796</td><td>0.093 818 328</td><td>6</td></tr> <tr><td></td><td>1.000 396 969</td><td>1.000 059 737</td><td>0.993 236 232</td><td>1.000 921 156</td><td>0.994 151 158</td><td>0.093 813 831</td><td>Avg</td></tr> </tbody> </table> | | | | | | | | Iteraton Results | CTS _p | CPS _p | CTL _p | CPL _p | CTPL _p | CPV _{run} M3 | Run | Crude Oil, JP-4 | 1.000 399 304 | 1.000 059 560 | 0.993 156 343 | 1.000 918 946 | 0.994 069 000 | 0.093 784 665 | 1 | Crude Oil, JP-4 | 1.000 401 274 | 1.000 059 708 | 0.993 132 375 | 1.000 921 390 | 0.994 047 438 | 0.093 799 851 | 2 | Crude Oil, JP-4 | 1.000 399 768 | 1.000 059 634 | 0.993 167 899 | 1.000 920 014 | 0.994 081 628 | 0.093 846 839 | 3 | Crude Oil, JP-4 | 1.000 393 086 | 1.000 059 783 | 0.993 322 397 | 1.000 921 293 | 0.994 237 538 | 0.093 819 290 | 4 | Crude Oil, JP-4 | 1.000 394 240 | 1.000 059 857 | 0.993 320 257 | 1.000 922 450 | 0.994 236 545 | 0.093 814 015 | 5 | Crude Oil, JP-4 | 1.000 394 144 | 1.000 059 881 | 0.993 318 118 | 1.000 922 845 | 0.994 234 796 | 0.093 818 328 | 6 | | 1.000 396 969 | 1.000 059 737 | 0.993 236 232 | 1.000 921 156 | 0.994 151 158 | 0.093 813 831 | Avg |
| Iteraton Results | CTS _p | CPS _p | CTL _p | CPL _p | CTPL _p | CPV _{run} M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 399 304 | 1.000 059 560 | 0.993 156 343 | 1.000 918 946 | 0.994 069 000 | 0.093 784 665 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 401 274 | 1.000 059 708 | 0.993 132 375 | 1.000 921 390 | 0.994 047 438 | 0.093 799 851 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 399 768 | 1.000 059 634 | 0.993 167 899 | 1.000 920 014 | 0.994 081 628 | 0.093 846 839 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 393 086 | 1.000 059 783 | 0.993 322 397 | 1.000 921 293 | 0.994 237 538 | 0.093 819 290 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 394 240 | 1.000 059 857 | 0.993 320 257 | 1.000 922 450 | 0.994 236 545 | 0.093 814 015 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 394 144 | 1.000 059 881 | 0.993 318 118 | 1.000 922 845 | 0.994 234 796 | 0.093 818 328 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 396 969 | 1.000 059 737 | 0.993 236 232 | 1.000 921 156 | 0.994 151 158 | 0.093 813 831 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>1 means ΔCPV Passed</th> <th>Δp_{B_SET} kg/m³</th> <th>ΔT_{P_SET} °C</th> <th>ΔP_{P_SET} kPag</th> <th>ΔQ_{M_SET} %</th> <th>$r\% ICPV_{run}$</th> <th>CPV_{set}</th> <th style="background-color: #f4a460;">CPV_{set} M3</th> <th></th> </tr> </thead> <tbody> <tr><td></td><td>0.000</td><td>0.041</td><td>3.00</td><td>0.0</td><td>0.066</td><td>-</td><td>0.093 810 452</td><td>Runs 1-3</td></tr> <tr><td></td><td>0.000</td><td>0.222</td><td>3.00</td><td>0.0</td><td>0.050</td><td>-</td><td>0.093 821 993</td><td>Runs 2-4</td></tr> <tr><td></td><td>0.000</td><td>0.181</td><td>4.50</td><td>0.0</td><td>0.035</td><td>-</td><td>0.093 826 714</td><td>Runs 3-5</td></tr> <tr><td>1</td><td>0.000</td><td>0.005</td><td>2.00</td><td>0.0</td><td>0.006</td><td>Pass</td><td>0.093 817 211</td><td>Runs 4-6</td></tr> </tbody> </table> | | | | | | | | 1 means ΔCPV Passed | Δp_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{M_SET} % | $r\% ICPV_{run}$ | CPV _{set} | CPV _{set} M3 | | | 0.000 | 0.041 | 3.00 | 0.0 | 0.066 | - | 0.093 810 452 | Runs 1-3 | | 0.000 | 0.222 | 3.00 | 0.0 | 0.050 | - | 0.093 821 993 | Runs 2-4 | | 0.000 | 0.181 | 4.50 | 0.0 | 0.035 | - | 0.093 826 714 | Runs 3-5 | 1 | 0.000 | 0.005 | 2.00 | 0.0 | 0.006 | Pass | 0.093 817 211 | Runs 4-6 | | | | | | | | | | | | | | | | | | | |
| 1 means ΔCPV Passed | Δp_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{M_SET} % | $r\% ICPV_{run}$ | CPV _{set} | CPV _{set} M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.000 | 0.041 | 3.00 | 0.0 | 0.066 | - | 0.093 810 452 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.000 | 0.222 | 3.00 | 0.0 | 0.050 | - | 0.093 821 993 | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.000 | 0.181 | 4.50 | 0.0 | 0.035 | - | 0.093 826 714 | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | 0.000 | 0.005 | 2.00 | 0.0 | 0.006 | Pass | 0.093 817 211 | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table style="width: 100%;"> <thead> <tr> <th style="text-align: center;">Signature</th> <th style="text-align: center;">Date</th> <th style="text-align: center;">Company</th> </tr> </thead> <tbody> <tr> <td style="height: 40px;"></td> <td></td> <td style="text-align: center;">API Midstream Representative</td> </tr> <tr><td style="height: 40px;"></td><td></td><td></td></tr> <tr><td style="height: 40px;"></td><td></td><td></td></tr> <tr><td style="height: 40px;"></td><td></td><td></td></tr> </tbody> </table> | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example A.2 - Calibration Set I - 2 of 2

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| Washington, D.C., USA | | | | | | | | | |
|--|--------------------|-------------------------------|---------------------------------|---------------------------------------|------------------------|---|----------------------|----------------------|-------|
| BPV Determination using Master Meter - Calibration Set II | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start | Stop | |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | Start 2 | Stop 2 | |
| Fluid or Batch | Crude | | Flow Design | Unidirectional | | Time | 14-Feb-24 | 14-Feb-24 | |
| Ch 11.1 | Crude | | Wall Design | Single | | Totalizer | 10:53:11 AM | 12:40:18 PM | |
| T _B | 15.0 | °C | Detector | External | | Fluid, Batch No. | 2,342,521.020 | 2,343,841.020 | M3 |
| P _B | 0.0 | kPag | Displacer | Captive Displacer | | API ₆₀ | Crude | Crude | |
| Master Meter | | | Wall Material | 316SS | | ρ ₆₀ | 35.2 | 35.1 | °API |
| Flowmeter ID | 200 | | Rod Material | Invar | | API ₁₅ | 848.217 | 848.587 | kg/m3 |
| Manufacturer | API | | GL _P | 0.000 016 02 per °C | | API ₁₅ | 35.1 | 35.0 | °API |
| Model | Turbine | | GL _D | 0.000 016 02 per °C | | ρ ₁₅ | 848.619 | 848.989 | kg/m3 |
| Nominal Size | 75 mm | | E _P | 193 053 196 per kPag | | API ₂₀ | 35.7 | 35.6 | °API |
| Type | Turbine | | ID _P | 441.960 0 mm | | ρ ₂₀ | 844.995 | 845.367 | kg/m3 |
| Proving Result | MMF | | WT _P | 46.355 0 mm | | Flowrate, Q _{av} | 83.332 | 83.434 | MPH |
| T _F Comp | No | | Serial No. | 8904-02 | | T _{MP_AVG} | 21.506 | 21.517 | °C |
| P _F Comp | No | | Switches | 9201 to 9202 | | P _{MP_AVG} | 1303.8 | 1306.6 | kPag |
| NKF | 4,382.111 0 P / M3 | | | | | Trips per Run | 1 | 1 | |
| Cartridge No. | API-0011 | | | | | Roundtrips | Runs 1-5 | Runs 1-5 | |
| Density Method | | | Calibration Set Criteria | | | Repeatability (r) | 0.011 | 0.008 | % |
| ρ _{obs} Method | Spot Sample | | ΔMMF _{SET} | ≤ 0.02 % | | Allowable (r) | 0.020 | 0.020 | % |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 % | | (r) Pass/Fail | Pass | Pass | |
| DMF | 0.000 0 | | (r) CPV _{RUN} | ≤ 0.02 % | | MMF | 1.000 055 2 | 1.000 058 6 | |
| HYC Factor | No | | Spot Sample | | | ΔMMF | NA | 0.000 | % |
| API Chapter 12.4.2 | | | ρ _{60_START} | 848.216 823 342 456 kg/m ³ | | Allowable ± ΔMMF | NA | 0.020 | % |
| SI_15 Measurement Units | | | ρ _{60_STOP} | 848.586 998 731 528 kg/m ³ | | ΔMMF Pass/Fail | NA | Pass | |
| Sampling Method - Spot | | | ρ _{60_SET} | 848.401 911 036 992 kg/m ³ | | | | | |
| BPV - Standard Method | | | MMF _{SET} | 1.000 056 9 | | | | | |
| Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs | | | Prior vs Current | | | | | | |
| Crude Oil - Tables 5A/6A | | | ΔQ _{av} 0.1 % | | | | | | |
| | | | ΔT _P 0.120 °C | | | | | | |
| Roundtrip Measurements | | | | | | | | | |
| ρ _{obs} | T _{dm} | P _{dm} | T _{FP_INLET} | T _{FP_OUTLET} | T _{MM} | T _{FD} | Base Density | Run | |
| kg/m ³ | °C | kPag | °C | °C | °C | °C | ρ _B | | |
| | | | 21.494 | 21.394 | 21.400 | 23.956 | 848.804 | 1 | |
| | | | 21.500 | 21.411 | 21.422 | 23.900 | 848.804 | 2 | |
| | | | 21.494 | 21.361 | 21.461 | 23.967 | 848.804 | 3 | |
| | | | | | | | | 4 | |
| | | | | | | | | 5 | |
| | | | | | | | | 6 | |
| | | | 21.496 | 21.389 | 21.428 | 23.941 | 848.804 | Avg | |
| Ch 11.1 Iteration Results | | | | | | | | | |
| | | Roundtrip Measurements | | | | T_{FP} and P_{FP} Values | | | |
| | | N or N _i | Q _{MM} | P _{FP_INLET} | P _{FP_OUTLET} | P _{MM} | T _{FP} | P _{FP} | Run |
| | | Pulses | MPH | kPag | kPag | kPag | °C | kPag | |
| Crude Oil, JP-4 | | 411.277 | 83.332 | 1,284.0 | 1,279.0 | 1,268.0 | 21.444 0 | 1,281.50 | 1 |
| Crude Oil, JP-4 | | 411.273 | 83.331 | 1,288.0 | 1,278.0 | 1,270.0 | 21.455 5 | 1,283.00 | 2 |
| Crude Oil, JP-4 | | 411.278 | 83.332 | 1,284.0 | 1,268.0 | 1,257.0 | 21.427 5 | 1,276.00 | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| | | 411.276 0 | 83.332 | 1,285.0 | 1,275.0 | 1,265.0 | 21.442 0 | 1,280.00 | Avg |

Example A.2 - Calibration Set II - 1 of 2

| Washington, D.C., USA | | | | | | | | | | | | | | | | | |
|---|--|---|---|--|---|------------------------------|---|-------|---------|-------|------|---------|--------|----------|----------|------------|------------|
| BPV Determination using Master Meter - Calibration Set II | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs Crude Oil - Tables 5A/6A | | | ΔMMF_{SET} Pass $(r) ICPV_{SET}$ Pass $(r) CPV_{SET}$ Pass | | Report Summary <div style="display: flex; justify-content: space-between;"> <div> Report No. Date Time Fluid, Batch No. </div> <div style="display: flex; align-items: center;"> <table border="1" style="font-size: small;"> <thead> <tr> <th>Prior</th> <th>Current</th> </tr> </thead> <tbody> <tr> <td>Start</td> <td>Stop</td> </tr> <tr> <td>Start 2</td> <td>Stop 2</td> </tr> <tr> <td>00:00:00</td> <td>00:00:00</td> </tr> <tr> <td>2342521.02</td> <td>2343841.02</td> </tr> </tbody> </table> </div> </div> | | | Prior | Current | Start | Stop | Start 2 | Stop 2 | 00:00:00 | 00:00:00 | 2342521.02 | 2343841.02 |
| Prior | Current | | | | | | | | | | | | | | | | |
| Start | Stop | | | | | | | | | | | | | | | | |
| Start 2 | Stop 2 | | | | | | | | | | | | | | | | |
| 00:00:00 | 00:00:00 | | | | | | | | | | | | | | | | |
| 2342521.02 | 2343841.02 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | N or N_i <small>Pulses</small> | NKF <small>P / M3</small> | IV_{MM} | CTL_{MM} | CPL_{MM} | CTPL_{MM} | GSV_{MM} <small>M3</small> | | | | | | | | | | |
| | 411.277 | 4,382.111 0 | 0.093 853 6 | 0.994 534 730 | 1.000 956 853 | 0.995 486 354 | 0.093 435 294 | | | | | | | | | | |
| | 411.273 | 4,382.111 0 | 0.093 852 7 | 0.994 515 913 | 1.000 958 492 | 0.995 469 148 | 0.093 432 783 | | | | | | | | | | |
| | 411.278 | 4,382.111 0 | 0.093 853 9 | 0.994 482 555 | 1.000 948 896 | 0.995 426 215 | 0.093 429 948 | | | | | | | | | | |
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| | 411.276 0 | 4,382.111 0 | 0.093 853 4 | 0.994 511 066 | 1.000 954 747 | 0.995 460 573 | 0.093 432 675 | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | Iteration Results | CTS_{FP} | CPS_{FP} | CTL_{FP} | CPL_{FP} | CTPL_{FP} | CPV_{run} <small>M3</small> | | | | | | | | | | |
| | Crude Oil, JP-4 | 1.000 349 981 | 1.000 063 289 | 0.994 497 096 | 1.000 967 309 | 0.995 459 081 | 0.093 822 736 | | | | | | | | | | |
| | Crude Oil, JP-4 | 1.000 349 452 | 1.000 063 363 | 0.994 487 259 | 1.000 968 509 | 0.995 450 430 | 0.093 821 072 | | | | | | | | | | |
| | Crude Oil, JP-4 | 1.000 349 629 | 1.000 063 017 | 0.994 511 209 | 1.000 963 057 | 0.995 468 979 | 0.093 816 493 | | | | | | | | | | |
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| | | | | | | | | | | | | | | | | | |
| | | 1.000 349 687 | 1.000 063 223 | 0.994 498 521 | 1.000 966 292 | 0.995 459 497 | 0.093 820 100 | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | 1 means ΔCPV Passed | ΔP_{B_SET} <small>kg/m³</small> | ΔT_{P_SET} <small>°C</small> | ΔP_{P_SET} <small>kPag</small> | ΔQ_{MM_SET} <small>%</small> | r% ICPV_{run} | CPV_{set} <small>M3</small> | | | | | | | | | | |
| Runs 1-3 | 1 | 0.000 | 0.028 | 7.00 | 0.0 | 0.007 | Pass | | | | | | | | | | |
| Runs 2-4 | NA | NA | NA | NA | NA | - | - | | | | | | | | | | |
| Runs 3-5 | NA | NA | NA | NA | NA | - | - | | | | | | | | | | |
| Runs 4-6 | NA | NA | NA | NA | NA | - | - | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| Signature | | | | Date | | Company | | | | | | | | | | | |
| | | | | | | API Midstream Representative | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
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| Washington, D.C., USA | | | | | | | | | |
|--|---------------------|-----------------|----------------------------------|---------------------------------------|-----------------|---------------------------|----------------------|----------------------|-------------------|
| BPV Determination using Master Meter - Calibration Set III | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start 3 | Stop 3 | |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | 14-Feb-24 | 14-Feb-24 | |
| Fluid or Batch | Crude | | Flow Design | Unidirectional | | Time | 8:21:18 AM | 11:21:18 AM | |
| Ch 11.1 | Crude | | Wall Design | Single | | Totalizer | 2,342,501.020 | 2,343,601.020 | M3 |
| T _B | 15.0 °C | | Detector | External | | Fluid, Batch No. | Crude | Crude | |
| P _B | 0.0 kPag | | Displacer | Captive Displacer | | API ₆₀ | 35.1 | 35.1 | °API |
| Master Meter | | | Wall Material | 316SS | | ρ ₆₀ | 848.427 | 848.387 | kg/m ³ |
| Flowmeter ID | 200 | | Rod Material | Invar | | API ₁₅ | 35.1 | 35.1 | °API |
| Manufacturer | API | | GL _P | 0.000 016 02 per °C | | ρ ₁₅ | 848.829 | 848.789 | kg/m ³ |
| Model | Turbine | | GL _D | 0.000 016 02 per °C | | API ₂₀ | 35.6 | 35.6 | °API |
| Nominal Size | 75 mm | | E _P | 193 053 196 per kPag | | ρ ₂₀ | 845.206 | 845.166 | kg/m ³ |
| Type | Turbine | | ID _P | 441.960 0 mm | | Flowrate, Q _{av} | 140.250 | 140.222 | MPH |
| Proving Result | MMF | | WT _P | 46.355 0 mm | | T _{MP_AVG} | 22.833 | 22.911 | °C |
| T _F Comp | No | | Serial No. | 8904-02 | | P _{MP_AVG} | 1294.1 | 1298.3 | kPag |
| P _F Comp | No | | Switches | 9201 to 9202 | | Trips per Run | 1 | 1 | |
| NKF | 4,382.111 0 P / M3 | | | | | Roundtrips | Runs 1-5 | Runs 1-5 | |
| Cartridge No. | API-0011 | | | | | Repeatability (r) | 0.008 | 0.014 | % |
| Density Method | | | Calibration Set Criteria | | | Allowable (r) | 0.020 | 0.020 | % |
| ρ _{obs} Method | Spot Sample | | ΔMMF _{SET} | ≤ 0.02 % | | (r) Pass/Fail | Pass | Pass | |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 % | | MMF | 0.999 845 2 | 0.999 865 5 | |
| DMF | 0.000 0 | | (r) CPV _{RUN} | ≤ 0.02 % | | ΔMMF | NA | 0.002 | % |
| HYC Factor | No | | Spot Sample | | | Allowable ± ΔMMF | NA | 0.020 | % |
| API Chapter 12.4.2 | | | ρ _{60_START} | 848.426 922 906 387 kg/m ³ | | ΔMMF Pass/Fail | NA | Pass | |
| SI_15 Measurement Units | | | ρ _{60_STOP} | 848.386 903 945 631 kg/m ³ | | | | | |
| Sampling Method - Spot | | | ρ _{60_SET} | 848.406 913 426 009 kg/m ³ | | | | | |
| BPV - Standard Method | | | MMF _{SET} 0.999 855 4 - | | | Prior vs Current | | | |
| Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs | | | | | | ΔQ _{av} | 0.1 % | | |
| Crude Oil - Tables 5A/6A | | | | | | ΔT _P | 0.120 °C | | |
| Roundtrip Measurements | | | | | | | | | |
| ρ _{obs} | T _{dm} | P _{dm} | T _{FP_INLET} | T _{FP_OUTLET} | T _{MM} | T _{FD} | Base Density | | |
| kg/m ³ | °C | kPag | °C | °C | °C | °C | ρ _B | kg/m ³ | Run |
| | | | 22.817 | 22.889 | 22.994 | 23.956 | 848.809 | | 1 |
| | | | 22.806 | 22.844 | 22.994 | 23.900 | 848.809 | | 2 |
| | | | 22.822 | 22.856 | 23.000 | 23.967 | 848.809 | | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| | | | 22.815 | 22.863 | 22.996 | 23.941 | 848.809 | | Avg |
| Roundtrip Measurements | | | | | | | | | |
| Ch 11.1 Iteration Results | N or N _i | Q _{MM} | P _{FP_INLET} | P _{FP_OUTLET} | P _{MM} | T _{FP} | P _{FP} | | |
| | Pulses | MPH | kPag | kPag | kPag | °C | kPag | | Run |
| Crude Oil, JP-4 | 411.407 | 140.247 | 1,214.0 | 1,198.0 | 1,278.0 | 22.853 0 | 1,206.00 | | 1 |
| Crude Oil, JP-4 | 411.413 | 140.248 | 1,218.0 | 1,200.0 | 1,282.0 | 22.825 0 | 1,209.00 | | 2 |
| Crude Oil, JP-4 | 411.408 | 140.247 | 1,215.0 | 1,200.0 | 1,285.0 | 22.839 0 | 1,207.50 | | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| | 411.409 3 | 140.247 | 1,216.0 | 1,199.0 | 1,282.0 | 22.839 0 | 1,208.00 | | Avg |

Example A.2 - Calibration Set III - 1 of 2

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| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|--------------------------------|--|---|-----------------------------|---------------------------|---|--------------------|--------------------------|----------|-------------------------------|--------------------------------|--|---------------------------|-----------------------------|------------------------------|--------------------------|--------------------|--------------------------|---------------|---------------|---------------|------------------|---------------|---------------|-----|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|----|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|----|----|----|----|----|--|---|--|----------|----------|----|----|----|----|----|--|---|--|----------|--|--|--|--|--|---|-----------|---------------|---------------|---------------|---------------|---------------|---------------|-----|
| BPV Determination using Master Meter - Calibration Set III | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 SI_15 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Crude Oil - Tables 5A/6A | | | ΔMMF_{SET} Pass $(r) ICPV_{SET}$ Pass $(r) CPV_{SET}$ Pass | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start</td> <td style="text-align: center;">Stop</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">Start 3</td> <td style="text-align: center;">Stop 3</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">00:00:00</td> <td style="text-align: center;">00:00:00</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">2342501.02</td> <td style="text-align: center;">2343601.02</td> </tr> </tbody> </table> | | | | | Prior | Current | Report No. | Start | Stop | Date | Start 3 | Stop 3 | Time | 00:00:00 | 00:00:00 | Fluid, Batch No. | 2342501.02 | 2343601.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | Start 3 | Stop 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 00:00:00 | 00:00:00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | 2342501.02 | 2343601.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;">N or N_i Pulses</th> <th style="text-align: center;">NKF P / M3</th> <th style="text-align: center;">IV_{MM}</th> <th style="text-align: center;">CTL_{MM}</th> <th style="text-align: center;">CPL_{MM}</th> <th style="text-align: center;">CTPL_{MM}</th> <th style="text-align: center;">GSV_{MM} M3</th> <th style="text-align: center;">Run</th> </tr> </thead> <tbody> <tr> <td>411.407</td> <td>4,382.111 0</td> <td>0.093 883 3</td> <td>0.993 170 895</td> <td>1.000 973 761</td> <td>0.994 138 006</td> <td>0.093 319 461</td> <td style="text-align: center;">1</td> </tr> <tr> <td>411.413</td> <td>4,382.111 0</td> <td>0.093 884 7</td> <td>0.993 170 895</td> <td>1.000 976 812</td> <td>0.994 141 036</td> <td>0.093 321 137</td> <td style="text-align: center;">2</td> </tr> <tr> <td>411.408</td> <td>4,382.111 0</td> <td>0.093 883 5</td> <td>0.993 165 759</td> <td>1.000 979 136</td> <td>0.994 138 203</td> <td>0.093 319 678</td> <td style="text-align: center;">3</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td style="text-align: center;">4</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td style="text-align: center;">5</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td style="text-align: center;">6</td> </tr> <tr> <td>411.409 3</td> <td>4,382.111 0</td> <td>0.093 883 8</td> <td>0.993 169 183</td> <td>1.000 976 570</td> <td>0.994 139 082</td> <td>0.093 320 092</td> <td style="text-align: center;">Avg</td> </tr> </tbody> </table> | | | | | | | | | | N or N _i Pulses | NKF P / M3 | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} M3 | Run | 411.407 | 4,382.111 0 | 0.093 883 3 | 0.993 170 895 | 1.000 973 761 | 0.994 138 006 | 0.093 319 461 | 1 | 411.413 | 4,382.111 0 | 0.093 884 7 | 0.993 170 895 | 1.000 976 812 | 0.994 141 036 | 0.093 321 137 | 2 | 411.408 | 4,382.111 0 | 0.093 883 5 | 0.993 165 759 | 1.000 979 136 | 0.994 138 203 | 0.093 319 678 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | 411.409 3 | 4,382.111 0 | 0.093 883 8 | 0.993 169 183 | 1.000 976 570 | 0.994 139 082 | 0.093 320 092 | Avg |
| N or N _i Pulses | NKF P / M3 | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.407 | 4,382.111 0 | 0.093 883 3 | 0.993 170 895 | 1.000 973 761 | 0.994 138 006 | 0.093 319 461 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.413 | 4,382.111 0 | 0.093 884 7 | 0.993 170 895 | 1.000 976 812 | 0.994 141 036 | 0.093 321 137 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.408 | 4,382.111 0 | 0.093 883 5 | 0.993 165 759 | 1.000 979 136 | 0.994 138 203 | 0.093 319 678 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.409 3 | 4,382.111 0 | 0.093 883 8 | 0.993 169 183 | 1.000 976 570 | 0.994 139 082 | 0.093 320 092 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;">Iteration Results</th> <th style="text-align: center;">CTS_{FP}</th> <th style="text-align: center;">CPS_{FP}</th> <th style="text-align: center;">CTL_{FP}</th> <th style="text-align: center;">CPL_{FP}</th> <th style="text-align: center;">CTPL_{FP}</th> <th style="text-align: center;">CPV_{run} M3</th> <th style="text-align: center;">Run</th> </tr> </thead> <tbody> <tr> <td>Crude Oil, JP-4</td> <td>1.000 395 137</td> <td>1.000 059 560</td> <td>0.993 291 584</td> <td>1.000 918 066</td> <td>0.994 203 491</td> <td>0.093 820 879</td> <td style="text-align: center;">1</td> </tr> <tr> <td>Crude Oil, JP-4</td> <td>1.000 393 342</td> <td>1.000 059 708</td> <td>0.993 315 550</td> <td>1.000 920 195</td> <td>0.994 229 594</td> <td>0.093 820 256</td> <td style="text-align: center;">2</td> </tr> <tr> <td>Crude Oil, JP-4</td> <td>1.000 394 865</td> <td>1.000 059 634</td> <td>0.993 303 567</td> <td>1.000 919 130</td> <td>0.994 216 543</td> <td>0.093 819 885</td> <td style="text-align: center;">3</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td style="text-align: center;">4</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td style="text-align: center;">5</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td style="text-align: center;">6</td> </tr> <tr> <td></td> <td>1.000 394 448</td> <td>1.000 059 634</td> <td>0.993 303 567</td> <td>1.000 919 130</td> <td>0.994 216 543</td> <td>0.093 820 340</td> <td style="text-align: center;">Avg</td> </tr> </tbody> </table> | | | | | | | | | | Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} M3 | Run | Crude Oil, JP-4 | 1.000 395 137 | 1.000 059 560 | 0.993 291 584 | 1.000 918 066 | 0.994 203 491 | 0.093 820 879 | 1 | Crude Oil, JP-4 | 1.000 393 342 | 1.000 059 708 | 0.993 315 550 | 1.000 920 195 | 0.994 229 594 | 0.093 820 256 | 2 | Crude Oil, JP-4 | 1.000 394 865 | 1.000 059 634 | 0.993 303 567 | 1.000 919 130 | 0.994 216 543 | 0.093 819 885 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | | 1.000 394 448 | 1.000 059 634 | 0.993 303 567 | 1.000 919 130 | 0.994 216 543 | 0.093 820 340 | Avg |
| Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} M3 | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 395 137 | 1.000 059 560 | 0.993 291 584 | 1.000 918 066 | 0.994 203 491 | 0.093 820 879 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 393 342 | 1.000 059 708 | 0.993 315 550 | 1.000 920 195 | 0.994 229 594 | 0.093 820 256 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 394 865 | 1.000 059 634 | 0.993 303 567 | 1.000 919 130 | 0.994 216 543 | 0.093 819 885 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 394 448 | 1.000 059 634 | 0.993 303 567 | 1.000 919 130 | 0.994 216 543 | 0.093 820 340 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">1 means ΔCPV Passed</th> <th style="text-align: center;">ΔP_{B_SET} kg/m³</th> <th style="text-align: center;">ΔT_{P_SET} °C</th> <th style="text-align: center;">ΔP_{P_SET} kPag</th> <th style="text-align: center;">ΔQ_{MM_SET} %</th> <th style="text-align: center;">r% ICPV_{run}</th> <th style="text-align: center;">CPV_{set}</th> <th style="text-align: center;">CPV_{set} M3</th> <th></th> </tr> </thead> <tbody> <tr> <td>Runs 1-3</td> <td style="text-align: center;">1</td> <td style="text-align: center;">0.000</td> <td style="text-align: center;">0.028</td> <td style="text-align: center;">3.00</td> <td style="text-align: center;">0.0</td> <td style="text-align: center;">0.001</td> <td style="text-align: center;">Pass</td> <td style="text-align: center;">0.093 820 340</td> <td style="text-align: center;">Runs 1-3</td> </tr> <tr> <td>Runs 2-4</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td></td> <td style="text-align: center;">-</td> <td></td> <td style="text-align: center;">Runs 2-4</td> </tr> <tr> <td>Runs 3-5</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td></td> <td style="text-align: center;">-</td> <td></td> <td style="text-align: center;">Runs 3-5</td> </tr> <tr> <td>Runs 4-6</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> <td></td> <td style="text-align: center;">-</td> <td></td> <td style="text-align: center;">Runs 4-6</td> </tr> </tbody> </table> | | | | | | | | | | | 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{MM_SET} % | r% ICPV _{run} | CPV _{set} | CPV _{set} M3 | | Runs 1-3 | 1 | 0.000 | 0.028 | 3.00 | 0.0 | 0.001 | Pass | 0.093 820 340 | Runs 1-3 | Runs 2-4 | NA | NA | NA | NA | NA | | - | | Runs 2-4 | Runs 3-5 | NA | NA | NA | NA | NA | | - | | Runs 3-5 | Runs 4-6 | NA | NA | NA | NA | NA | | - | | Runs 4-6 | | | | | | | | | | | | | | |
| | 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °C | ΔP_{P_SET} kPag | ΔQ_{MM_SET} % | r% ICPV _{run} | CPV _{set} | CPV _{set} M3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 | 1 | 0.000 | 0.028 | 3.00 | 0.0 | 0.001 | Pass | 0.093 820 340 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 2-4 | NA | NA | NA | NA | NA | | - | | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 3-5 | NA | NA | NA | NA | NA | | - | | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 4-6 | NA | NA | NA | NA | NA | | - | | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="text-align: center;">Signature</th> <th style="text-align: center;">Date</th> <th style="text-align: center;">Company</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td style="text-align: center;">API Midstream Representative</td> </tr> <tr> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> </tbody> </table> | | | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example A.2 - Calibration Set III - 2 of 2

Annex B
(informative)
USC Unit Examples³

Example B.1 – Standard Method

USC Units, Continuous Sampling, Master Prover - Bidirectional Free Displacer, Master Meter - PD, MF r% - Fixed Range, MF Method - IMF, Field Prover - Bidirectional Free Displacer

DRAFT

³ The following examples are for illustration purposes only. Each company should develop its own approach. They are not to be considered exclusive or exhaustive in nature. API makes no warranties, express or implied, for reliance on or any omissions from the information contained in this document.

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| Master Prover | |
|-----------------|--|
| BPV Units | 0 (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) |
| Detector Design | 0 (0-Internal, 1-External) |
| Wall Material | 1 (1-CS, 2-304SS, 3-316SS, 4-17-4PH) |
| Rod Material | 0 (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) |
| Certificate BPV | 30,030.795 3 cubic inches at 60.0 °F, 0.0 psig |

| Base Prover Volume (BPV) | | |
|--------------------------|-------------------|-------------------|
| BPV ₆₀ | BPV ₁₅ | BPV ₂₀ |
| Barrels | Cubic Meters | Cubic Meters |
| 3.095 320 068 027 | 0.492 107 411 000 | 0.492 189 795 000 |

| Decimals | 9 | 10 | 10 |
|------------|------------------------------------|---------------------------------|---------------------------------|
| Conversion | in ³ / Bbl 9.702E+03 | mL / M ³ 1.00E+06 | mL / M ³ 1.00E+06 |
| Rnd'd BPV | 3.095 320 068 000 | 0.492 107 411 000 | 0.492 189 795 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to **10 digits** (the appropriate decimal place) to increase the precision of the Master Prover's BPV, not the uncertainty of the Master Prover's BPV.

| Decimal Base CTS | T _B | °F |
|---------------------------|----------------|-----------------------------------|
| Decimal BPV ₆₀ | 9 | - |
| Decimal BPV _{SI} | 3 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV | 9 | mL at 15.0 °C and 0.0 kPag |

Detector Design,

CTS_P = [1 + (T_P - T_B) x GL_P]³, for detectors mounted in calibrated section
 CTS_P = [1 + (T_P - T_B) x GL_P]² x [1 + (T_D - T_B) x GL_D], for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F

BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig
 BPV₁₅ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C

BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
 BPV₁₅ = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = ROUND(BPV₁₅ x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C

BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
 BPV₁₅ = ROUND(BPV₂₀ x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| T _B | 60.0 °F | 15.0 °C | 20.0 °C |
|-----------------|--------------|--------------|--------------|
| GL _P | 0.000 006 20 | 0.000 011 16 | 0.000 011 16 |
| GL _D | NA | NA | NA |

| Base CTS ₆₀ | 1.000 000 000 | 1.000 018 600 | 0.999 851 207 |
|------------------------|---------------|---------------|---------------|
| Base CTS ₁₅ | 0.999 981 400 | 1.000 000 000 | 0.999 832 609 |
| Base CTS ₂₀ | 1.000 148 807 | 1.000 167 409 | 1.000 000 000 |

| Base Unit Volume | |
|-------------------|--|
| BPV ₆₀ | 30,030.795 3 cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 492,107.411 mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 492,189.795 mL at 20.0 °C and 0.0 kPag |

| API Properties | | |
|---|------------------------------------|---------------------------------------|
| Linear Coefficient of Thermal Expansion, GL | | |
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,3,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar TM | 0.000 001 44 | 0.000 000 80 |

Notes:

(1) The User/Owner should obtain GL values from the prover manufacturer.

(2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.

(3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.

(4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.

(5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Example B.1 - Expanded Discrimination of Master Prover's BPV

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| Washington, D.C., USA | | | | | | | | | |
|--|---------------------|-------------------------------|----------------------------|-----------------------|-----------------------|---|--------------------|---------------------|-------------------|
| Master Meter Proving Report | | | | | | | | | |
| General Data | | | Displacement Prover | | | Report Summary | | | |
| Operator | API Midstream | - | Manufacturer | API | - | Report No. | Start I | Stop I | - |
| Station Name | MPMS | - | Prover Type | Displacement | - | Date | 14-Feb-24 | 14-Feb-24 | - |
| Ch 11.1 | Tables 5B/6B | - | Flow Design | Bidirectional | - | Time | 8:21:18 | 11:21:18 | - |
| T _B | 60.0 | °F | Wall Design | Single | - | Totalizer | 2,342,501.020 | 2,343,601.020 | Bbl |
| P _B | 0.0 | psig | Detector | Internal | - | Fluid, Batch No. | Products | Products | - |
| Master Meter | | | Displacer | Free Sphere | - | API ₆₀ | 60.8 | 60.6 | °API |
| Flowmeter ID | 200 | - | Wall Material | Carbon Steel | - | P ₆₀ | 735.210 | 735.710 | kg/m ³ |
| Manufacturer | API | - | Rod Material | NA | - | API ₁₅ | 60.7 | 60.5 | °API |
| Model | PD | - | GL _P | 0.000 006 20 | per °F | P ₁₅ | 735.715 | 736.216 | kg/m ³ |
| Nominal Size | 4 | inch | GL _D | NA | per °F | API ₂₀ | 61.7 | 61.5 | °API |
| Type | PD | - | E _P | 030 000 000 | per psig | P ₂₀ | 731.158 | 731.660 | kg/m ³ |
| Proving Result | MMF | - | ID _P | 7.981 0 | inch | Flowrate, Q | 700.350 | 700.350 | BPH |
| T _F Comp | No | - | WT _P | 0.322 0 | inch | T _{P_AVG} | 73.090 | 73.093 | °F |
| P _F Comp | No | - | Calibration Date | 2021-09-04 | - | P _{P_AVG} | 170.6 | 175.4 | psig |
| NKF | 8,400.000 0 | P / Bbl | Serial No. | 8904-01 | - | Trips per Run | 1 | 1 | - |
| Cartridge No. | API-0011 | - | Certificate No. | 10101010 | - | Roundtrips | Runs 1-5 | Runs 1-5 | - |
| Density Method | | | Switches | 9201 to 9202 | - | Repeatability (r) | 0.018 | 0.017 | % |
| Sample Method | Continuous | - | BPV | 3.095 320 068 0 | Bbl | Allowable (r) | 0.020 | 0.020 | % |
| ρ _{obs} Device | Densitometer | - | Spot Sample | | | (r) Pass/Fail | Pass | Pass | - |
| DMF | 0.999 8 | - | API _{Ind} | NA | °API | MMF | 0.999 900 0 | 0.999 904 1 | - |
| HYC Factor | NA | - | P _{Ind} | NA | kg/m ³ | ΔMMF | NA | 0.000 | % |
| API MPMS Chapter 12.4.2 | | | T _{obs} | NA | °F | Allowable ± ΔMMF | NA | 0.020 | % |
| Measurement Units - USC | | | P _{obs} | NA | psig | ΔMMF Pass/Fail | NA | Pass | - |
| Sampling Method - Continuous (or Online) | | | Prior vs Current | | | | | | |
| Meter Factor Method - Intermediate (or IMF) | | | ΔQ 0.0 % | | | | | | |
| Repeatability Method (r%) - Fixed, 5 out of 5 Runs | | | ΔT _P 0.003 °F | | | | | | |
| API MPMS Chapter 11.1 - Tables 5B/6B | | | | | | | | | |
| Base Density | | Roundtrip Measurements | | | | | | Base Density | |
| API _B | P _{Ind} | T _{dm} | P _{dm} | T _{P_INLET} | T _{P_OUTLET} | T _M | T _D | ρ _B | Run |
| °API | kg/m ³ | °F | psig | °F | °F | °F | °F | kg/m ³ | |
| 60.7 | 729.543 | 73.840 | 184.6 | 73.070 | 73.200 | 73.390 | | 735.311 | 1 |
| 60.6 | 729.745 | 74.730 | 184.9 | 73.050 | 73.120 | 73.370 | | 735.959 | 2 |
| 60.6 | 729.745 | 74.770 | 186.2 | 73.080 | 73.140 | 73.400 | | 735.770 | 3 |
| 60.6 | 729.545 | 74.750 | 185.8 | 73.060 | 73.070 | 73.350 | | 735.764 | 4 |
| 60.6 | 729.512 | 74.780 | 185.8 | 73.050 | 73.090 | 73.260 | | 735.747 | 5 |
| NA | | | | | | | | | 6 |
| NA | | | | | | | | | 7 |
| NA | | | | | | | | | 8 |
| NA | | | | | | | | | 9 |
| NA | | | | | | | | | 10 |
| 60.6 | 729.578 | 74.574 | 185.5 | NA | NA | 73.354 | NA | 735.710 | Runs 1-5 |
| Commodity Type | | Roundtrip Measurements | | | | T_P and P_P Values | | | |
| | N or N _i | Q _M | P _{P_INLET} | P _{P_OUTLET} | P _M | T _{P_RUN} | P _{P_RUN} | Run | |
| | Pulses | BPH | psig | psig | psig | °F | psig | | |
| Gasoline, Napthene | 26,020.000 | 700.110 0 | 177.9 | 173.2 | 173.5 | 73.135 0 | 175.55 | 1 | |
| Gasoline, Napthene | 26,016.000 | 700.120 0 | 178.2 | 172.9 | 173.4 | 73.085 0 | 175.55 | 2 | |
| Gasoline, Napthene | 26,018.000 | 700.250 0 | 177.2 | 173.4 | 173.0 | 73.110 0 | 175.30 | 3 | |
| Gasoline, Napthene | 26,020.000 | 701.020 0 | 177.6 | 173.7 | 173.5 | 73.065 0 | 175.65 | 4 | |
| Gasoline, Napthene | 26,018.000 | 700.240 0 | 177.2 | 173.0 | 173.8 | 73.070 0 | 175.10 | 5 | |
| NA | | | | | | | | 6 | |
| NA | | | | | | | | 7 | |
| NA | | | | | | | | 8 | |
| NA | | | | | | | | 9 | |
| NA | | | | | | | | 10 | |
| Runs 1-5 | 26,018.400 0 | 700.350 0 | NA | NA | 173.4 | 73.093 0 | 175.40 | Runs 1-5 | |

Example B.1 - Calibration Set I - Stop Proving Report - 1 of 2

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | |
|---|---|--------------------|------------------|--|----------------------|-----------------------|-------------------------|----------|--|--|-------|---------|------------|---------|--------|------|-----------|-----------|------|----------|----------|------------------|----------|----------|
| Master Meter Proving Report | | | | | | | | | | | | | | | | | | | | | | | | |
| API MPMS Chapter 12.4.2 Measurement Units - USC Sampling Method - Continuous (or Online) Meter Factor Method - Intermediate (or IMF) Repeatability Method (r%) - Fixed, 5 out of 5 Runs API MPMS Chapter 11.1 - Tables 5B/6B | | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start I</td> <td style="text-align: center;">Stop I</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">14-Feb-24</td> <td style="text-align: center;">14-Feb-24</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">08:21:18</td> <td style="text-align: center;">11:21:18</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">Products</td> <td style="text-align: center;">Products</td> </tr> </tbody> </table> | | | | | | | Prior | Current | Report No. | Start I | Stop I | Date | 14-Feb-24 | 14-Feb-24 | Time | 08:21:18 | 11:21:18 | Fluid, Batch No. | Products | Products |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start I | Stop I | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | |
| Time | 08:21:18 | 11:21:18 | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Products | Products | | | | | | | | | | | | | | | | | | | | | | |
| Run | BPV Bbl | CTS _p | CPS _p | Rnd CTL _p | Rnd CPL _p | Rnd CTPL _p | GSV _p Bbl | Run | | | | | | | | | | | | | | | | |
| 1 | 3.095 320 068 0 | 1.000 244 331 | 1.000 145 038 | 0.990 943 192 | 1.001 436 670 | 0.992 366 851 | 3.072 889 158 0 | 1 | | | | | | | | | | | | | | | | |
| 2 | 3.095 320 068 0 | 1.000 243 401 | 1.000 145 038 | 0.990 989 845 | 1.001 431 843 | 0.992 408 787 | 3.073 016 158 0 | 2 | | | | | | | | | | | | | | | | |
| 3 | 3.095 320 068 0 | 1.000 243 866 | 1.000 144 831 | 0.990 969 051 | 1.001 431 272 | 0.992 387 398 | 3.072 950 717 0 | 3 | | | | | | | | | | | | | | | | |
| 4 | 3.095 320 068 0 | 1.000 243 029 | 1.000 145 120 | 0.991 000 024 | 1.001 433 887 | 0.992 421 006 | 3.073 053 104 0 | 4 | | | | | | | | | | | | | | | | |
| 5 | 3.095 320 068 0 | 1.000 243 122 | 1.000 144 666 | 0.990 996 239 | 1.001 429 546 | 0.992 412 914 | 3.073 026 937 0 | 5 | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | 8 | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | |
| Runs 1-5 | 3.095 320 068 0 | 1.000 243 550 | 1.000 144 939 | 0.990 979 670 | 1.001 432 644 | 0.992 399 391 | 3.072 987 215 0 | Runs 1-5 | | | | | | | | | | | | | | | | |
| Run | N or N _i | NKF P / Bbl | IV _M | Rnd CTL _M | Rnd CPL _M | Rnd CTPL _M | ISV _M Bbl | Run | | | | | | | | | | | | | | | | |
| 1 | 26,020.000 | 8,400.000 0 | 3.097 619 048 0 | 0.990 766 899 | 1.001 421 479 | 0.992 175 254 | 3.073 380 964 0 | 1 | | | | | | | | | | | | | | | | |
| 2 | 26,016.000 | 8,400.000 0 | 3.097 142 857 0 | 0.990 793 079 | 1.001 416 072 | 0.992 196 113 | 3.072 973 105 0 | 2 | | | | | | | | | | | | | | | | |
| 3 | 26,018.000 | 8,400.000 0 | 3.097 380 952 0 | 0.990 768 752 | 1.001 414 286 | 0.992 169 983 | 3.073 128 405 0 | 3 | | | | | | | | | | | | | | | | |
| 4 | 26,020.000 | 8,400.000 0 | 3.097 619 048 0 | 0.990 803 180 | 1.001 418 104 | 0.992 208 242 | 3.073 483 150 0 | 4 | | | | | | | | | | | | | | | | |
| 5 | 26,018.000 | 8,400.000 0 | 3.097 380 952 0 | 0.990 865 007 | 1.001 420 115 | 0.992 272 149 | 3.073 444 854 0 | 5 | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | 8 | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | |
| Runs 1-5 | 26,018.400 0 | 8,400.000 0 | 3.097 428 571 0 | 0.990 799 383 | 1.001 418 011 | 0.992 204 348 | 3.073 282 096 0 | Runs 1-5 | | | | | | | | | | | | | | | | |
| Run | '1' indicates Repeatability (r%) criteria satisfied | Repeatability (r%) | | Meter Factor Method - Intermediate (or IMF) | | | IMF | Run | | | | | | | | | | | | | | | | |
| | | Actual | Allowable | | | | | | | | | | | | | | | | | | | | | |
| NA | | NA | NA | | | | 0.999 839 98 | 1 | | | | | | | | | | | | | | | | |
| NA | | NA | NA | | | | 1.000 014 01 | 2 | | | | | | | | | | | | | | | | |
| NA | NA | NA | NA | Repeatability Method (r%) - Fixed, 5 out of 5 Runs | | | 0.999 942 18 | 3 | | | | | | | | | | | | | | | | |
| NA | NA | NA | NA | | | | 0.999 860 08 | 4 | | | | | | | | | | | | | | | | |
| Runs 1-5 | 1 | 0.017 | 0.020 | | | | 0.999 864 02 | 5 | | | | | | | | | | | | | | | | |
| Runs 2-6 | | | 0.020 | | | | | 6 | | | | | | | | | | | | | | | | |
| Runs 3-7 | | | 0.020 | | | | | 7 | | | | | | | | | | | | | | | | |
| Runs 4-8 | | | 0.020 | | | | | 8 | | | | | | | | | | | | | | | | |
| Runs 5-9 | | | 0.020 | | | | | 9 | | | | | | | | | | | | | | | | |
| Runs 6-10 | | | 0.020 | | | | | 10 | | | | | | | | | | | | | | | | |
| | Pass | 0.017 | | | | | 0.999 904 10 | MMF | | | | | | | | | | | | | | | | |
| MMF Rounded to 7 decimal places | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |

Example B.1 - Calibration Set I - Stop Proving Report - 2 of 2

| Field Prover | |
|--|--|
| Measurement Units | 0 (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) |
| Detector Design | 0 (0-Internal, 1-External) |
| Wall Material | 1 (1-CS, 2-304SS, 3-316SS, 4-17-4PH) |
| Rod Material | 0 (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) |
| Source for GL _{MP} , GL _{md} , E _{MP} | 1 (0-Prover Manufacturer, 1-API Table) |
| BPV _P | 115,481.685 8 cubic inches at 60.0 °F, 0.0 psig |

| Base Prover Volume (BPV) | | |
|--------------------------|-------------------|-------------------|
| BPV ₆₀ | BPV ₁₅ | BPV ₂₀ |
| Barrels | Cubic Meters | Cubic Meters |
| 11.902 874 232 117 | 1.892 370 577 000 | 1.892 687 379 000 |

| Decimals | 4 | 5 | 5 |
|------------|------------------------------------|---------------------------------|---------------------------------|
| Conversion | in ³ / Bbl 9.702E+03 | mL / M ³ 1.00E+06 | mL / M ³ 1.00E+06 |
| Rnd'd BPV | 11.902 900 000 000 | 1.892 370 000 000 | 1.892 690 000 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to 6 digits (the appropriate decimal place).

| T _B | 60.0 | °F |
|---------------------------|------|-----------------------------------|
| Decimal Base CTS | 9 | - |
| Decimal BPV ₆₀ | 4 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV _{SI} | 3 | mL at 15.0 °C and 0.0 kPag |
| Decimal BPV | 4 | Barrels |
| Decimal BPV | 5 | Cubic Meters |

Detector Design,
 $CTS_P = [1 + (T_P - T_B) \times GL_P]^3$, for detectors mounted in calibrated section
 $CTS_P = [1 + (T_P - T_B) \times GL_P]^2 \times [1 + (T_D - T_B) \times GL_d]$, for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F
 BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig
 BPV₁₅ = ROUND(BPV₆₀ × 16.387 064 × Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = ROUND(BPV₆₀ × 16.387 064 × Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C
 BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 × Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
 BPV₁₅ = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = ROUND(BPV₁₅ × Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C
 BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 × Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig
 BPV₁₅ = ROUND(BPV₂₀ × Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag
 BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| GL _P | 0.000 006 20 | 0.000 011 16 | 0.000 011 16 |
|-----------------|--------------|--------------|--------------|
| GL _D | NA | NA | NA |
| T _B | 60.0 | 15.0 | 20.0 |

| Base CTS ₂₀ | 1.000 000 000 | 1.000 018 600 | 0.999 851 207 |
|------------------------|---------------|---------------|---------------|
| Base CTS ₁₅ | 0.999 981 400 | 1.000 000 000 | 0.999 832 609 |
| Base CTS ₂₀ | 1.000 148 807 | 1.000 167 409 | 1.000 000 000 |

| Base Unit Volume | |
|-------------------|---|
| BPV ₆₀ | 115,481.685 8 cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 1,892,370.577 0 mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 1,892,687.379 0 mL at 20.0 °C and 0.0 kPag |

in³ = mL / 16.387 064
 U.S. Gallons = in³ / 2.31E+02
 Bbl = in³ / 9.702E+03
 Cubic Feet = in³ / 1.728E+03

mL = M³ × 1E+06
 mL = in³ × 16.387 064

M³ = mL × 1E-06
 L = mL × 1E-03

| API Properties | | |
|---|------------------------------------|---------------------------------------|
| Linear Coefficient of Thermal Expansion, GL | | |
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,3,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar TM | 0.000 001 44 | 0.000 000 80 |

Notes:
 (1) The User/Owner should obtain GL values from the prover manufacturer.
 (2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.
 (3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.
 (4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.
 (5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Example B.1 - Field Prover's BPV Conversion

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| Washington, D.C., USA | | | | | | | | | |
|---|-------------------|---------------------|--------------------------|-------------|---------------------------|---------------------|----------------------------|-------------|-------------------|
| BPV Determination using a Master Meter - Standard Method | | | | | | | | | |
| General Data | | | Master Meter | | | Field Prover | | | |
| API Midstream | Operator | Flowmeter ID | 200 | - | Manufacturer | API | - | | |
| Headquarters | Station Name | Manufacturer | API | - | Prover Design | Displacement | - | | |
| Washington | City, Town | Model | API-PD | - | Flow Design | Bidirectional | - | | |
| D.C. | State, Province | Nominal Size | 4 | inch | Wall Design | Single | - | | |
| USA | Country | Type | PD | - | Detector | Internal | - | | |
| RBOB | Fluid, Batch No. | Proving Result | MMF | - | Displacer | Free Sphere | - | | |
| Products | Ch 11.1 | T _F Comp | No | - | Wall Material | Carbon Steel | - | | |
| 60.0 | T _B | P _F Comp | No | - | Rod Material | NA | - | | |
| 0.0 | P _B | NKF | 8,400.000 0 | P / Bbl | GL _P | 0.000 006 20 | per °F | | |
| 14-Feb-2024 | Start Calibration | Cartridge No. | API-0011 | - | GL _D | NA | per °F | | |
| 14-Feb-2024 | Stop Calibration | | | - | E _P | 030 000 000 | per psig | | |
| API Chapter 12.4.2 USC 60 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r \leq 0.02\%$, for 3 consecutive Calibration Sets Refined Product - Tables 5B/6B | | | Density Method | | | ID _P | 21.562 0 | inch | |
| | | | Continuous | | | WT _P | 1.219 0 | inch | |
| | | | Online Density | | | Trips per Run | 1 | - | |
| | | | DMF 0.999 8 | | | Serial No. | Bidi-SI-001 | - | |
| | | | HYC Factor No | | | Switches | 9206 to 9236 | - | |
| | | | Calibration Set I | | Calibration Set II | | Calibration Set III | | |
| | | | Start | Stop | Start | Stop | Start | Stop | |
| Report No. | Start 1 | Stop 1 | Start 2 | Stop 2 | 1 | Stop 1 | | | |
| Date | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | | | |
| Products | Products | Products | 84RBOB | 84RBOB | Products | Products | | | |
| API _B | 60.8 | 60.6 | 61.0 | 61.0 | 60.8 | 60.6 | °API | | |
| ρ _B | 735.210 | 735.710 | 734.457 | 734.419 | 735.210 | 735.710 | kg/m ³ | | |
| Q _{MM} | 700.350 | 700.350 | 524.145 | 524.785 | 882.146 | 881.970 | BPH | | |
| T _{MP_AVG} | 73.090 | 70.093 | 70.710 | 70.730 | 73.100 | 73.240 | °F | | |
| P _{MP_AVG} | 170.6 | 175.4 | 189.1 | 189.5 | 187.7 | 188.3 | psig | | |
| Roundtrips | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | | | |
| Repeatability (r) | 0.018 | 0.017 | 0.011 | 0.008 | 0.018 | 0.017 | % | | |
| MMF | 0.999 900 0 | 0.999 904 1 | 0.999 974 0 | 0.999 999 0 | 1.000 099 0 | 1.000 154 0 | | | |
| MMF _{SET} | NA | 0.999 902 1 | NA | 0.999 986 5 | NA | 1.000 126 5 | | | |
| ΔMMF | NA | 0.000 | NA | 0.003 | NA | 0.006 | % | | |
| | | | Pass | | Pass | | Pass | | |
| ΔMMF _{SET} | | | Pass | | Pass | | Pass | | |
| (r) CPV _{RUN} | | | Pass | | Pass | | Pass | | |
| (R) CPV _{SET} | | | Pass | | Pass | | Pass | | |
| ΔQ _{SET} | | | Pass | | Pass | | Pass | | |
| Selected Set | | | Runs 1-3 | | Runs 1-3 | | Runs 1-3 | | |
| CPV _{SET} | | | 11.903 715 5 | | 11.902 465 7 | | 11.903 036 5 | | Bbls |
| API _{B_SET} | | | 60.7 | | 61.1 | | 60.7 | | °API |
| ρ _{B_SET} | | | 735.456 | | 734.016 | | 735.383 | | kg/m ³ |
| T _{FP_SET} | | | 73.080 | | 70.600 | | 73.110 | | °F |
| P _{FP_SET} | | | 175.7 | | 185.7 | | 175.1 | | psig |
| Q _{MM_SET} | | | 701.040 | | 524.142 | | 882.128 | | BPH |
| ΔMMF _{SET} | | | 0.000 | | 0.003 | | 0.006 | | % |
| Δρ _{B_SET} | | | 0.072 | | 0.292 | | 0.278 | | kg/m ³ |
| ΔT _{P_SET} | | | 0.010 | | 0.050 | | 0.050 | | °F |
| ΔP _{P_SET} | | | 0.3 | | 1.1 | | 0.4 | | psig |
| ΔQ _{MM_SET} | | | 0.0 | | 0.0 | | 0.0 | | % |
| ΔQ _{between SETS} | | | NA | | (25.2) | | 40.6 | | % |
| (r) CPV _{RUN} | | | 0.004 | | 0.015 | | 0.006 | | % |
| (R) CPV _{SET} | | | NA | | 0.011 | | 0.005 | | % |
| CPV_{SET} Stability Parameters | | | | | | | | | |

Example B.1 - Calibration Report Summary - 1 of 2

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|-------------------|---|--------------------|---------------|---|--------------------|---------------|----------------------------|-------------------|-----------------|----------------------------|---------|---------|---|---|---------|------|----------------|----------------------------|----------------|-------------|-------------------|-------------|------------------|---|--|--|--|--------------|-----|---|---------------|--------------|---|-------------|---------------|---|-------------|--------|---|----------|----------|---|-----------|-------------|---|---------------|--------------|---|--------------|----|---|-----------------|--------------|--------|-----------------|----|--------|----------------|-------------|----------|-----------------|----------|------|-----------------|---------|------|------------|-------------|---|----------|--------------|---|
| BPV Determination using a Master Meter - Standard Method | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| General Data <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; border-right: 1px solid black; padding: 2px;">API Midstream</td> <td style="padding: 2px;">Operator</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Headquarters</td> <td style="padding: 2px;">Station Name</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Washington</td> <td style="padding: 2px;">City, Town</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">D.C.</td> <td style="padding: 2px;">State, Province</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">USA</td> <td style="padding: 2px;">Country</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">RBOB</td> <td style="padding: 2px;">Fluid, Batch No.</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Products</td> <td style="padding: 2px;">Ch 11.1</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">60.0</td> <td style="padding: 2px;">T_B</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">0.0</td> <td style="padding: 2px;">P_B</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">14-Feb-2024</td> <td style="padding: 2px;">Start Calibration</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">14-Feb-2024</td> <td style="padding: 2px;">Stop Calibration</td> </tr> </table> | | | API Midstream | Operator | Headquarters | Station Name | Washington | City, Town | D.C. | State, Province | USA | Country | RBOB | Fluid, Batch No. | Products | Ch 11.1 | 60.0 | T _B | 0.0 | P _B | 14-Feb-2024 | Start Calibration | 14-Feb-2024 | Stop Calibration | Field Prover <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; border-right: 1px solid black; padding: 2px;">Manufacturer</td> <td style="padding: 2px;">API</td> <td style="width: 5%; text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Prover Design</td> <td style="padding: 2px;">Displacement</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Flow Design</td> <td style="padding: 2px;">Bidirectional</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Wall Design</td> <td style="padding: 2px;">Single</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Detector</td> <td style="padding: 2px;">Internal</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Displacer</td> <td style="padding: 2px;">Free Sphere</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Wall Material</td> <td style="padding: 2px;">Carbon Steel</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Rod Material</td> <td style="padding: 2px;">NA</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">GL_P</td> <td style="padding: 2px;">0.000 006 20</td> <td style="text-align: right;">per °F</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">GL_D</td> <td style="padding: 2px;">NA</td> <td style="text-align: right;">per °F</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">E_P</td> <td style="padding: 2px;">030 000 000</td> <td style="text-align: right;">per psig</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">ID_P</td> <td style="padding: 2px;">21.562 0</td> <td style="text-align: right;">inch</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">WT_P</td> <td style="padding: 2px;">1.219 0</td> <td style="text-align: right;">inch</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Serial No.</td> <td style="padding: 2px;">Bidi-SI-001</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">Switches</td> <td style="padding: 2px;">9206 to 9236</td> <td style="text-align: right;">-</td> </tr> </table> | | | | Manufacturer | API | - | Prover Design | Displacement | - | Flow Design | Bidirectional | - | Wall Design | Single | - | Detector | Internal | - | Displacer | Free Sphere | - | Wall Material | Carbon Steel | - | Rod Material | NA | - | GL _P | 0.000 006 20 | per °F | GL _D | NA | per °F | E _P | 030 000 000 | per psig | ID _P | 21.562 0 | inch | WT _P | 1.219 0 | inch | Serial No. | Bidi-SI-001 | - | Switches | 9206 to 9236 | - |
| API Midstream | Operator | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Headquarters | Station Name | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Washington | City, Town | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| D.C. | State, Province | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| USA | Country | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RBOB | Fluid, Batch No. | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Products | Ch 11.1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 60.0 | T _B | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.0 | P _B | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14-Feb-2024 | Start Calibration | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 14-Feb-2024 | Stop Calibration | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Manufacturer | API | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Prover Design | Displacement | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flow Design | Bidirectional | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Wall Design | Single | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Detector | Internal | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Displacer | Free Sphere | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Wall Material | Carbon Steel | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Rod Material | NA | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GL _P | 0.000 006 20 | per °F | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GL _D | NA | per °F | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| E _P | 030 000 000 | per psig | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ID _P | 21.562 0 | inch | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| WT _P | 1.219 0 | inch | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Serial No. | Bidi-SI-001 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Switches | 9206 to 9236 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; border-right: 1px solid black; padding: 2px;">BPV_{NEW}</td> <td style="padding: 2px;">11.903 100 0</td> <td style="padding: 2px;">Bbls</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">BPV_{OLD}</td> <td style="padding: 2px;">11.902 900 0</td> <td style="padding: 2px;">Bbls</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">ΔBPV</td> <td style="padding: 2px;">0.000 200 0</td> <td style="padding: 2px;">Bbls</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">ΔBPV</td> <td style="padding: 2px;">0.001 7</td> <td style="padding: 2px;">% BPV_{NEW} Bigger / (Smaller)</td> </tr> </table> | | | BPV _{NEW} | 11.903 100 0 | Bbls | BPV _{OLD} | 11.902 900 0 | Bbls | ΔBPV | 0.000 200 0 | Bbls | ΔBPV | 0.001 7 | % BPV _{NEW} Bigger / (Smaller) | <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; border-right: 1px solid black; padding: 2px;">Average CPV_{SET}</td> <td style="padding: 2px;">11.903 072 600</td> <td style="padding: 2px;">Bbls</td> </tr> </table> | | | | Average CPV _{SET} | 11.903 072 600 | Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV _{NEW} | 11.903 100 0 | Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV _{OLD} | 11.902 900 0 | Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔBPV | 0.000 200 0 | Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔBPV | 0.001 7 | % BPV _{NEW} Bigger / (Smaller) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Average CPV _{SET} | 11.903 072 600 | Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; border-right: 1px solid black; padding: 2px;">BPV₆₀</td> <td style="padding: 2px;">115,483.610 4</td> <td style="padding: 2px;">in³ at 60.0 °F and 0.0 psig</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">BPV₁₅</td> <td style="padding: 2px;">1,892,402.115</td> <td style="padding: 2px;">mL at 15.0 °C and 0.0 kPag</td> </tr> <tr> <td style="border-right: 1px solid black; padding: 2px;">BPV₂₀</td> <td style="padding: 2px;">1,892,718.922</td> <td style="padding: 2px;">mL at 20.0 °C and 0.0 kPag</td> </tr> </table> | | | BPV ₆₀ | 115,483.610 4 | in ³ at 60.0 °F and 0.0 psig | BPV ₁₅ | 1,892,402.115 | mL at 15.0 °C and 0.0 kPag | BPV ₂₀ | 1,892,718.922 | mL at 20.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₆₀ | 115,483.610 4 | in ³ at 60.0 °F and 0.0 psig | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₁₅ | 1,892,402.115 | mL at 15.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₂₀ | 1,892,718.922 | mL at 20.0 °C and 0.0 kPag | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Base Prover Volume (BPV _{NEW}) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| BPV ₆₀ | | | BPV ₁₅ | | BPV ₂₀ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Barrels | U.S. Gallons | Cubic Feet | Cubic Meters | Liters | Cubic Meters | Liters | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | 1,892.40 | - | 1,892.72 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | 499.929 | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 11.903 1 | - | 66.830 8 | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | 1.892 40 | - | 1.892 72 | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| - | - | - | - | - | - | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Note: The BPV_{NEW} values (BPV₆₀, BPV₁₅, BPV₂₀) shown are reported to 6 significant digits (10 ppm, or, 0.001%).

| Signature | Date | Company |
|-----------|------|------------------------------|
| | | API Midstream Representative |
| | | |
| | | |
| | | |

Example B.1 - Calibration Report Summary - 2 of 2

This document is not an API Standard; it is under consideration within an API technical committee but has not received all approvals required to become an API Standard. It shall not be reproduced or circulated or quoted, in whole or in part, outside of API committee activities except with the approval of the Chairman of the committee having jurisdiction and staff of the API Standards Dept. Copyright API. All rights reserved.

| Washington, D.C., USA | | | | | | | | | | |
|--|-----------------------|-------------------------------|---------------------------------|------------------------------|-------------------------------|---------------------------|---|--------|----------------------------|--|
| BPV Determination using Master Meter - Calibration Set I | | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start 1 | | Stop 1 | |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | 14-Feb-24 | | 14-Feb-24 | |
| Fluid or Batch | RBOB | | Flow Design | Bidirectional | | Time | 8:21:18 AM | | 11:21:18 AM | |
| Ch 11.1 | Products | | Wall Design | Single | | Totalizer | 2,342,501.020 | | 2,343,601.020 | |
| T _B | 60.0 °F | | Detector | Internal | | Fluid, Batch No. | Products | | Products | |
| P _B | 0.0 psig | | Displacer | Free Sphere | | API ₆₀ | 60.8 | | 60.6 | |
| Master Meter | | | Wall Material | 300 SS | | ρ ₆₀ | 735.210 | | 735.710 | |
| Flowmeter ID | 200 | | Rod Material | NA | | API ₁₅ | 60.7 | | 60.5 | |
| Manufacturer | API | | GL _P | 0.000 006 20 | | ρ ₁₅ | 735.715 | | 736.216 | |
| Model | API-PD | | GL _D | NA | | API ₂₀ | 61.7 | | 61.5 | |
| Nominal Size | 4 inch | | E _P | 030 000 000 | | ρ ₂₀ | 731.158 | | 731.660 | |
| Type | PD | | ID _P | 21.562 0 | | Flowrate, Q _{av} | 700.350 | | 700.350 | |
| Proving Result | MMF | | WT _P | 1.219 0 | | T _{MP_AVG} | 73.090 | | 70.093 | |
| T _F Comp | No | | Serial No. | Bidi-SI-001 | | P _{MP_AVG} | 170.6 | | 175.4 | |
| P _F Comp | No | | Switches | 9206 to 9236 | | Trips per Run | 1 | | 1 | |
| NKF | 8,400.000 0 P / Bbl | | | | | Roundtrips | Runs 1-5 | | Runs 1-5 | |
| Cartridge No. | API-0011 | | | | | Repeatability (r) | 0.018 | | 0.017 | |
| Density Method | | | Calibration Set Criteria | | | Allowable (r) | 0.020 | | 0.020 | |
| ρ _{obs} Method | Continuous | | ΔMMF _{SET} | ≤ 0.02 % | | (r) Pass/Fail | Pass | | Pass | |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 % | | MMF | 0.999 900 0 | | 0.999 904 1 | |
| DMF | 0.999 8 | | (r) CPV _{RUN} | ≤ 0.02 % | | ΔMMF | NA | | 0.000 | |
| HYC Factor | No | | Spot Sample | | | Allowable ± ΔMMF | NA | | 0.020 | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs Refined Product - Tables 5B/6B | | | ρ _{60_START} | NA kg/m ³ | | ΔMMF Pass/Fail | NA | | Pass | |
| | | | ρ _{60_STOP} | NA kg/m ³ | | | | | | |
| | | | ρ _{60_SET} | NA kg/m ³ | | | | | | |
| | | | MMF _{SET} | 0.999 902 1 | | | | | | |
| Roundtrip Measurements | | | | | | | | | | |
| ρ _{obs} kg/m ³ | T _{dm} °F | P _{dm} psig | T _{P_INLET} °F | T _{P_OUTLET} °F | T _M °F | T _D °F | Base Density ρ _B kg/m ³ | | Run | |
| 729.748 | 73.230 | 174.5 | 73.070 | 73.200 | 73.390 | | 735.415 | | 1 | |
| 729.843 | 73.230 | 175.2 | 73.050 | 73.120 | 73.390 | | 735.506 | | 2 | |
| 729.545 | 73.270 | 175.2 | 73.080 | 73.140 | 73.400 | | 735.228 | | 3 | |
| 729.748 | 73.240 | 175.5 | 73.070 | 73.070 | 73.400 | | 735.414 | | 4 | |
| 729.799 | 73.240 | 174.8 | 73.060 | 73.090 | 73.500 | | 735.469 | | 5 | |
| 729.823 | 73.230 | 175.1 | 73.060 | 73.100 | 73.420 | | 735.486 | | 6 | |
| 729.751 | 73.240 | 175.1 | 73.070 | 73.120 | 73.420 | | 735.420 | | Avg | |
| Ch 11.1 Iteration Results | | | | | | | | | | |
| | | Roundtrip Measurements | | | | | | Run | | |
| | | N or N _i Pulses | Q _M BPH | P _{P_INLET} psig | P _{P_OUTLET} psig | P _M psig | T _{P_RUN} °F | | P _{P_RUN} psig | |
| Gasoline, Napthene | | 100,015.000 | 701.110 | 176.1 | 173.8 | 185.4 | 73.135 0 | 174.95 | 1 | |
| Gasoline, Napthene | | 100,001.000 | 700.982 | 176.7 | 174.0 | 185.9 | 73.085 0 | 175.35 | 2 | |
| Gasoline, Napthene | | 100,022.000 | 700.995 | 176.2 | 174.0 | 186.4 | 73.110 0 | 175.10 | 3 | |
| Gasoline, Napthene | | 100,051.000 | 701.014 | 176.8 | 174.3 | 186.4 | 73.070 0 | 175.55 | 4 | |
| Gasoline, Napthene | | 100,054.000 | 701.002 | 176.9 | 174.6 | 186.7 | 73.075 0 | 175.75 | 5 | |
| Gasoline, Napthene | | 100,052.000 | 701.103 | 176.9 | 174.8 | 185.5 | 73.080 0 | 175.85 | 6 | |
| | | 100,032.500 0 | 701.034 | 176.6 | 174.3 | 186.1 | 73.090 0 | 175.40 | Avg | |

Example B.1 - Calibration Set I - 1 of 2

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|--|------------------------------|-----------------------------|--|-------------------|----------------------------|----------------------------|-------------------------------|--|---------------------------|-----------------------------|--------------------------|------------------------------|----------------------------|----------------------------|--------------------|---------------|---------------|---------------|------------------|---------------|----------------|---|--------------------|---------------|---------------|---------------|---------------|---------------|----------------|-------|--------------------|----------------|---------------|---------------|---------------|---------------|----------------|-----|--------------------|---------------|----------------|---------------|---------------|---------------|----------------|------|--------------------|---------------|---------------|----------------|---------------|---------------|----------------|---|--------------------|---------------|---------------|---------------|---------------|---------------|----------------|---|---------------|---------------|---------------|---------------|---------------|---------------|----------------|-----|
| BPV Determination using Master Meter - Calibration Set I | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Refined Product - Tables 5B/6B | ΔMMF_{SET} Pass - (r) ICPV_{RUN} Pass - (r) CPV_{RUN} Pass - | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start</td> <td style="text-align: center;">Stop</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">14-Feb-24</td> <td style="text-align: center;">14-Feb-24</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">08:21:18</td> <td style="text-align: center;">11:21:18</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">Products</td> <td style="text-align: center;">Products</td> </tr> </tbody> </table> | | | | | Prior | Current | Report No. | Start | Stop | Date | 14-Feb-24 | 14-Feb-24 | Time | 08:21:18 | 11:21:18 | Fluid, Batch No. | Products | Products | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 08:21:18 | 11:21:18 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Products | Products | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>N or N_i Pulses</th> <th>NKF P / Bbl</th> <th>IV_M</th> <th>CTL_M</th> <th>CPL_M</th> <th>CTPL_M</th> <th>GSV_M Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>100,015.000</td><td>8,400.000 0</td><td>11.906 547 6</td><td>0.990 768 877</td><td>1.001 518 360</td><td>0.992 273 221</td><td>11.813 391 700</td><td>1</td></tr> <tr><td>100,001.000</td><td>8,400.000 0</td><td>11.904 881 0</td><td>0.990 770 609</td><td>1.001 521 790</td><td>0.992 278 354</td><td>11.811 799 200</td><td>2</td></tr> <tr><td>100,022.000</td><td>8,400.000 0</td><td>11.907 381 0</td><td>0.990 758 393</td><td>1.001 528 016</td><td>0.992 272 288</td><td>11.814 207 500</td><td>3</td></tr> <tr><td>100,051.000</td><td>8,400.000 0</td><td>11.910 833 3</td><td>0.990 761 947</td><td>1.001 526 637</td><td>0.992 274 480</td><td>11.817 658 900</td><td>4</td></tr> <tr><td>100,054.000</td><td>8,400.000 0</td><td>11.911 190 5</td><td>0.990 693 883</td><td>1.001 529 367</td><td>0.992 209 018</td><td>11.817 233 600</td><td>5</td></tr> <tr><td>100,052.000</td><td>8,400.000 0</td><td>11.910 952 4</td><td>0.990 749 505</td><td>1.001 518 856</td><td>0.992 254 311</td><td>11.817 536 800</td><td>6</td></tr> <tr><td>100,032.500 0</td><td>8,400.000 0</td><td>11.908 631 0</td><td>0.990 750 536</td><td>1.001 523 838</td><td>0.992 260 279</td><td>11.815 304 600</td><td>Avg</td></tr> </tbody> </table> | | | | | | | | N or N _i Pulses | NKF P / Bbl | IV _M | CTL _M | CPL _M | CTPL _M | GSV _M Bbls | Run | 100,015.000 | 8,400.000 0 | 11.906 547 6 | 0.990 768 877 | 1.001 518 360 | 0.992 273 221 | 11.813 391 700 | 1 | 100,001.000 | 8,400.000 0 | 11.904 881 0 | 0.990 770 609 | 1.001 521 790 | 0.992 278 354 | 11.811 799 200 | 2 | 100,022.000 | 8,400.000 0 | 11.907 381 0 | 0.990 758 393 | 1.001 528 016 | 0.992 272 288 | 11.814 207 500 | 3 | 100,051.000 | 8,400.000 0 | 11.910 833 3 | 0.990 761 947 | 1.001 526 637 | 0.992 274 480 | 11.817 658 900 | 4 | 100,054.000 | 8,400.000 0 | 11.911 190 5 | 0.990 693 883 | 1.001 529 367 | 0.992 209 018 | 11.817 233 600 | 5 | 100,052.000 | 8,400.000 0 | 11.910 952 4 | 0.990 749 505 | 1.001 518 856 | 0.992 254 311 | 11.817 536 800 | 6 | 100,032.500 0 | 8,400.000 0 | 11.908 631 0 | 0.990 750 536 | 1.001 523 838 | 0.992 260 279 | 11.815 304 600 | Avg |
| N or N _i Pulses | NKF P / Bbl | IV _M | CTL _M | CPL _M | CTPL _M | GSV _M Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,015.000 | 8,400.000 0 | 11.906 547 6 | 0.990 768 877 | 1.001 518 360 | 0.992 273 221 | 11.813 391 700 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,001.000 | 8,400.000 0 | 11.904 881 0 | 0.990 770 609 | 1.001 521 790 | 0.992 278 354 | 11.811 799 200 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,022.000 | 8,400.000 0 | 11.907 381 0 | 0.990 758 393 | 1.001 528 016 | 0.992 272 288 | 11.814 207 500 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,051.000 | 8,400.000 0 | 11.910 833 3 | 0.990 761 947 | 1.001 526 637 | 0.992 274 480 | 11.817 658 900 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,054.000 | 8,400.000 0 | 11.911 190 5 | 0.990 693 883 | 1.001 529 367 | 0.992 209 018 | 11.817 233 600 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,052.000 | 8,400.000 0 | 11.910 952 4 | 0.990 749 505 | 1.001 518 856 | 0.992 254 311 | 11.817 536 800 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,032.500 0 | 8,400.000 0 | 11.908 631 0 | 0.990 750 536 | 1.001 523 838 | 0.992 260 279 | 11.815 304 600 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Iteration Results</th> <th>CTS_p</th> <th>CPS_p</th> <th>CTL_p</th> <th>CPL_p</th> <th>CTPL_p</th> <th>CPV_{run} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>Gasoline, Napthene</td><td>1.000 244 331</td><td>1.000 103 152</td><td>0.990 945 132</td><td>1.001 431 033</td><td>0.992 363 208</td><td>11.900 167 000</td><td>1</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 243 401</td><td>1.000 103 388</td><td>0.990 981 383</td><td>1.001 433 360</td><td>0.992 401 816</td><td>11.898 108 100</td><td>2</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 243 866</td><td>1.000 103 241</td><td>0.990 958 917</td><td>1.001 433 403</td><td>0.992 379 360</td><td>11.900 799 500</td><td>3</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 243 122</td><td>1.000 103 506</td><td>0.990 990 040</td><td>1.001 435 540</td><td>0.992 412 646</td><td>11.903 882 700</td><td>4</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 243 215</td><td>1.000 103 624</td><td>0.990 987 612</td><td>1.001 436 825</td><td>0.992 411 488</td><td>11.903 465 600</td><td>5</td></tr> <tr><td>Gasoline, Napthene</td><td>1.000 243 308</td><td>1.000 103 683</td><td>0.990 984 476</td><td>1.001 437 557</td><td>0.992 409 073</td><td>11.903 798 200</td><td>6</td></tr> <tr><td></td><td>1.000 243 541</td><td>1.000 103 432</td><td>0.990 974 593</td><td>1.001 434 620</td><td>0.992 396 265</td><td>11.901 703 500</td><td>Avg</td></tr> </tbody> </table> | | | | | | | | Iteration Results | CTS _p | CPS _p | CTL _p | CPL _p | CTPL _p | CPV _{run} Bbls | Run | Gasoline, Napthene | 1.000 244 331 | 1.000 103 152 | 0.990 945 132 | 1.001 431 033 | 0.992 363 208 | 11.900 167 000 | 1 | Gasoline, Napthene | 1.000 243 401 | 1.000 103 388 | 0.990 981 383 | 1.001 433 360 | 0.992 401 816 | 11.898 108 100 | 2 | Gasoline, Napthene | 1.000 243 866 | 1.000 103 241 | 0.990 958 917 | 1.001 433 403 | 0.992 379 360 | 11.900 799 500 | 3 | Gasoline, Napthene | 1.000 243 122 | 1.000 103 506 | 0.990 990 040 | 1.001 435 540 | 0.992 412 646 | 11.903 882 700 | 4 | Gasoline, Napthene | 1.000 243 215 | 1.000 103 624 | 0.990 987 612 | 1.001 436 825 | 0.992 411 488 | 11.903 465 600 | 5 | Gasoline, Napthene | 1.000 243 308 | 1.000 103 683 | 0.990 984 476 | 1.001 437 557 | 0.992 409 073 | 11.903 798 200 | 6 | | 1.000 243 541 | 1.000 103 432 | 0.990 974 593 | 1.001 434 620 | 0.992 396 265 | 11.901 703 500 | Avg |
| Iteration Results | CTS _p | CPS _p | CTL _p | CPL _p | CTPL _p | CPV _{run} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 244 331 | 1.000 103 152 | 0.990 945 132 | 1.001 431 033 | 0.992 363 208 | 11.900 167 000 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 243 401 | 1.000 103 388 | 0.990 981 383 | 1.001 433 360 | 0.992 401 816 | 11.898 108 100 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 243 866 | 1.000 103 241 | 0.990 958 917 | 1.001 433 403 | 0.992 379 360 | 11.900 799 500 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 243 122 | 1.000 103 506 | 0.990 990 040 | 1.001 435 540 | 0.992 412 646 | 11.903 882 700 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 243 215 | 1.000 103 624 | 0.990 987 612 | 1.001 436 825 | 0.992 411 488 | 11.903 465 600 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 243 308 | 1.000 103 683 | 0.990 984 476 | 1.001 437 557 | 0.992 409 073 | 11.903 798 200 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 243 541 | 1.000 103 432 | 0.990 974 593 | 1.001 434 620 | 0.992 396 265 | 11.901 703 500 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>1 means ΔCPV Passed</th> <th>ΔP_{B-SET} kg/m³</th> <th>ΔT_{P-SET} °F</th> <th>ΔP_{P-SET} psig</th> <th>ΔQ_{M-SET} %</th> <th>r% CPV</th> <th>CPV_{set}</th> <th>CPV_{set} Bbls</th> <th></th> </tr> </thead> <tbody> <tr><td></td><td>0.278</td><td>0.050</td><td>0.40</td><td>0.0</td><td>0.023</td><td>-</td><td>11.899 691 500</td><td>Runs 1-3</td></tr> <tr><td></td><td>0.278</td><td>0.040</td><td>0.45</td><td>0.0</td><td>0.049</td><td>-</td><td>11.900 930 100</td><td>Runs 2-4</td></tr> <tr><td></td><td>0.241</td><td>0.040</td><td>0.65</td><td>0.0</td><td>0.026</td><td>-</td><td>11.902 715 900</td><td>Runs 3-5</td></tr> <tr><td>1</td><td>0.072</td><td>0.010</td><td>0.30</td><td>0.0</td><td>0.004</td><td>Pass</td><td>11.903 715 500</td><td>Runs 4-6</td></tr> </tbody> </table> | | | | | | | | 1 means ΔCPV Passed | ΔP _{B-SET} kg/m ³ | ΔT _{P-SET} °F | ΔP _{P-SET} psig | ΔQ _{M-SET} % | r% CPV | CPV _{set} | CPV _{set} Bbls | | | 0.278 | 0.050 | 0.40 | 0.0 | 0.023 | - | 11.899 691 500 | Runs 1-3 | | 0.278 | 0.040 | 0.45 | 0.0 | 0.049 | - | 11.900 930 100 | Runs 2-4 | | 0.241 | 0.040 | 0.65 | 0.0 | 0.026 | - | 11.902 715 900 | Runs 3-5 | 1 | 0.072 | 0.010 | 0.30 | 0.0 | 0.004 | Pass | 11.903 715 500 | Runs 4-6 | | | | | | | | | | | | | | | | | | | |
| 1 means ΔCPV Passed | ΔP _{B-SET} kg/m ³ | ΔT _{P-SET} °F | ΔP _{P-SET} psig | ΔQ _{M-SET} % | r% CPV | CPV _{set} | CPV _{set} Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.278 | 0.050 | 0.40 | 0.0 | 0.023 | - | 11.899 691 500 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.278 | 0.040 | 0.45 | 0.0 | 0.049 | - | 11.900 930 100 | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.241 | 0.040 | 0.65 | 0.0 | 0.026 | - | 11.902 715 900 | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | 0.072 | 0.010 | 0.30 | 0.0 | 0.004 | Pass | 11.903 715 500 | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 40%;">Signature</th> <th style="width: 20%;">Date</th> <th style="width: 40%;">Company</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td style="text-align: center;">API Midstream Representative</td> </tr> <tr><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td></tr> </tbody> </table> | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example B.1 - Calibration Set I - 2 of 2

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|--|-------------------------------|-------------------------|--|--------------------------------|-------------------------|--|-------------------------------------|--------------|-----|---------------------|--------|------|-------------------------|---------|--------|------------------------|-----------|-----------|------|-------------|-------------|-----------|---------------|---------------|------------------|--------|--------|-------------------|------|------|-----------------|---------|---------|-------------------|------|------|-----------------|---------|---------|-------------------|------|------|-----------------|---------|---------|---------------------------|---------|---------|---------------------|--------|--------|---------------------|-------|-------|---------------|---|---|------------|----------|----------|-------------------|-------|-------|---------------|-------|-------|---------------|------|------|-----|-------------|-------------|------|----|-------|------------------|----|-------|----------------|----|------|
| BPV Determination using Master Meter - Calibration Set II | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| General Data Operator: API Midstream Station Name: Headquarters Fluid or Batch: RBOB Ch 11.1 Products: 60.0 °F T _B : 0.0 psig P _B : 0.0 psig | | | Field Prover Prover Manufacturer: API Prover Design: Displacement Flow Design: Bidirectional Wall Design: Single Detector: Internal Displacer: Free Sphere Wall Material: 300 SS Rod Material: NA GL _P : 0.000 006 20 per °F GL _D : NA per °F E _P : 030 000 000 per psig ID _P : 21.562 0 inch W/T _P : 1.219 0 inch Serial No.: Bidi-SI-001 Switches: 9206 to 9236 | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="background-color: #d9ead3;">Start</th> <th style="background-color: #d9ead3;">Stop</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td>Start 2</td> <td>Stop 2</td> </tr> <tr> <td>Date</td> <td>14-Feb-24</td> <td>14-Feb-24</td> </tr> <tr> <td>Time</td> <td>10:53:11 AM</td> <td>12:40:18 PM</td> </tr> <tr> <td>Totalizer</td> <td>2,342,521.020</td> <td>2,343,841.020</td> </tr> <tr> <td>Fluid, Batch No.</td> <td>84RBOB</td> <td>84RBOB</td> </tr> <tr> <td>API₆₀</td> <td>61.0</td> <td>61.0</td> </tr> <tr> <td>ρ₆₀</td> <td>734.457</td> <td>734.419</td> </tr> <tr> <td>API₁₅</td> <td>60.9</td> <td>60.9</td> </tr> <tr> <td>ρ₁₅</td> <td>734.963</td> <td>734.924</td> </tr> <tr> <td>API₂₀</td> <td>61.9</td> <td>61.9</td> </tr> <tr> <td>ρ₂₀</td> <td>730.402</td> <td>730.364</td> </tr> <tr> <td>Flowrate, Q_{av}</td> <td>524.145</td> <td>524.785</td> </tr> <tr> <td>T_{MP_AVG}</td> <td>70.710</td> <td>70.730</td> </tr> <tr> <td>P_{MP_AVG}</td> <td>189.1</td> <td>189.5</td> </tr> <tr> <td>Trips per Run</td> <td>1</td> <td>1</td> </tr> <tr> <td>Roundtrips</td> <td>Runs 1-5</td> <td>Runs 1-5</td> </tr> <tr> <td>Repeatability (r)</td> <td>0.011</td> <td>0.008</td> </tr> <tr> <td>Allowable (r)</td> <td>0.020</td> <td>0.020</td> </tr> <tr> <td>(r) Pass/Fail</td> <td>Pass</td> <td>Pass</td> </tr> <tr> <td>MMF</td> <td>0.999 974 0</td> <td>0.999 999 0</td> </tr> <tr> <td>ΔMMF</td> <td>NA</td> <td>0.003</td> </tr> <tr> <td>Allowable ± ΔMMF</td> <td>NA</td> <td>0.020</td> </tr> <tr> <td>ΔMMF Pass/Fail</td> <td>NA</td> <td>Pass</td> </tr> </tbody> </table> | | | | | Start | Stop | Report No. | Start 2 | Stop 2 | Date | 14-Feb-24 | 14-Feb-24 | Time | 10:53:11 AM | 12:40:18 PM | Totalizer | 2,342,521.020 | 2,343,841.020 | Fluid, Batch No. | 84RBOB | 84RBOB | API ₆₀ | 61.0 | 61.0 | ρ ₆₀ | 734.457 | 734.419 | API ₁₅ | 60.9 | 60.9 | ρ ₁₅ | 734.963 | 734.924 | API ₂₀ | 61.9 | 61.9 | ρ ₂₀ | 730.402 | 730.364 | Flowrate, Q _{av} | 524.145 | 524.785 | T _{MP_AVG} | 70.710 | 70.730 | P _{MP_AVG} | 189.1 | 189.5 | Trips per Run | 1 | 1 | Roundtrips | Runs 1-5 | Runs 1-5 | Repeatability (r) | 0.011 | 0.008 | Allowable (r) | 0.020 | 0.020 | (r) Pass/Fail | Pass | Pass | MMF | 0.999 974 0 | 0.999 999 0 | ΔMMF | NA | 0.003 | Allowable ± ΔMMF | NA | 0.020 | ΔMMF Pass/Fail | NA | Pass |
| | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start 2 | Stop 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 10:53:11 AM | 12:40:18 PM | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Totalizer | 2,342,521.020 | 2,343,841.020 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | 84RBOB | 84RBOB | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₆₀ | 61.0 | 61.0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ ₆₀ | 734.457 | 734.419 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₁₅ | 60.9 | 60.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ ₁₅ | 734.963 | 734.924 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₂₀ | 61.9 | 61.9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ ₂₀ | 730.402 | 730.364 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flowrate, Q _{av} | 524.145 | 524.785 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| T _{MP_AVG} | 70.710 | 70.730 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P _{MP_AVG} | 189.1 | 189.5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Trips per Run | 1 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrips | Runs 1-5 | Runs 1-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Repeatability (r) | 0.011 | 0.008 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Allowable (r) | 0.020 | 0.020 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) Pass/Fail | Pass | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MMF | 0.999 974 0 | 0.999 999 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF | NA | 0.003 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Allowable ± ΔMMF | NA | 0.020 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF Pass/Fail | NA | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Master Meter Flowmeter ID: 200 Manufacturer: API Model: API-PD Nominal Size: 4 inch Type: PD Proving Result: MMF T _F Comp: No P _F Comp: No NKF: 8,400.000 0 P / Bbl Cartridge No.: API-0011 | | | Density Method ρ _{obs} Method: Continuous ρ _{obs} Device: Online Density DMF: 0.999 8 HYC Factor: No | | | Calibration Set Criteria <table border="1" style="width: 100%; border-collapse: collapse;"> <tbody> <tr> <td>ΔMMF_{SET}</td> <td>≤ 0.02</td> <td>%</td> </tr> <tr> <td>(r) ICPV_{RUN}</td> <td>≤ 0.02</td> <td>%</td> </tr> <tr> <td>(r) CPV_{RUN}</td> <td>≤ 0.02</td> <td>%</td> </tr> </tbody> </table> | | | | ΔMMF _{SET} | ≤ 0.02 | % | (r) ICPV _{RUN} | ≤ 0.02 | % | (r) CPV _{RUN} | ≤ 0.02 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF _{SET} | ≤ 0.02 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) ICPV _{RUN} | ≤ 0.02 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) CPV _{RUN} | ≤ 0.02 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Spot Sample P _{60_START} : NA kg/m ³ P _{60_STOP} : NA kg/m ³ P _{60_SET} : NA kg/m ³ MMF _{SET} : 0.999 986 5 | | | Prior vs Current ΔQ _{av} : 0.1 % ΔT _P : 0.120 °C | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | Base Density | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ _{obs} kg/m ³ | T _{dm} °F | P _{dm} psig | T _{FP_INLET} °F | T _{FP_OUTLET} °F | T _{MM} °F | T _{FD} °F | ρ _B kg/m ³ | | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.748 | 70.710 | 188.6 | 70.690 | 70.510 | 70.520 | | 734.061 | | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.843 | 70.690 | 189.7 | 70.700 | 70.540 | 70.560 | | 734.139 | | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.545 | 70.690 | 188.7 | 70.690 | 70.450 | 70.630 | | 733.847 | | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 729.712 | 70.700 | 189.0 | 70.690 | 70.500 | 70.570 | | 734.016 | | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Ch 11.1 Iteration Results | N or N _i Pulses | Q _{MM} BPH | P _{FP_INLET} psig | P _{FP_OUTLET} psig | P _{MM} psig | T _{FP} °F | P _{FP} psig | | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,015.000 | 524.145 | 186.2 | 185.5 | 183.9 | 70.600 0 | 185.85 | | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,001.000 | 524.139 | 186.8 | 185.4 | 184.2 | 70.620 0 | 186.10 | | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 100,022.000 | 524.141 | 186.2 | 183.9 | 182.3 | 70.570 0 | 185.05 | | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 100,012.700 0 | 524.142 | 186.4 | 184.9 | 183.5 | 70.600 0 | 185.70 | | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Example B.1 - Calibration Set II - 1 of 2

This document is not an API Standard; it is under consideration within an API technical committee but has not received all approvals required to become an API Standard. It shall not be reproduced or circulated or quoted, in whole or in part, outside of API committee activities except with the approval of the Chairman of the committee having jurisdiction and staff of the API Standards Dept. Copyright API. All rights reserved.

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|--|--|-----------------------------|---------------------------|---|---------------------|---------------------|--------------------------------|--|---------------------------|-----------------------------|---------------------------|------------------------------|---------------------|---------------------|--------------------|--|---------------|---------------|------------------|---------------|----------------|-------|--------------------|----------------|---------------|---------------|---------------|---------------|----------------|----|--------------------|---------------|---------------|---------------|---------------|---------------|----------------|----|----|---|---|----------|--|----|----|----|----|----|---|---|----------|--|--|---|--|--|--|--|--|----------|--|---|---------------|---------------|---------------|---------------|---------------|---------------|----------------|-----|
| BPV Determination using Master Meter - Calibration Set II | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Refined Product - Tables 5B/6B | | <div style="display: flex; justify-content: space-around;"> <div> ΔMMF_{SET} Pass $(r) ICPV_{SET}$ Pass $(r) CPV_{SET}$ Pass </div> <div style="border-left: 1px solid black; padding-left: 5px;">-</div> </div> | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start</td> <td style="text-align: center;">Stop</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">Start 2</td> <td style="text-align: center;">Stop 2</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">00:00:00</td> <td style="text-align: center;">00:00:00</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">2342521.02</td> <td style="text-align: center;">2343841.02</td> </tr> </tbody> </table> | | | | Prior | Current | Report No. | Start | Stop | Date | Start 2 | Stop 2 | Time | 00:00:00 | 00:00:00 | Fluid, Batch No. | 2342521.02 | 2343841.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | Start 2 | Stop 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 00:00:00 | 00:00:00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | 2342521.02 | 2343841.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| N or N_j Pulses | NKF P / Bbl | IV_{MM} | CTL_{MM} | CPL_{MM} | $CTPL_{MM}$ | GSV_{MM} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,015.000 | 8,400.000 0 | 11.906 547 6 | 0.992 731 258 | 1.001 496 747 | 0.994 217 126 | 11.837 533 700 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,001.000 | 8,400.000 0 | 11.904 881 0 | 0.992 704 747 | 1.001 498 890 | 0.994 192 702 | 11.835 586 000 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 100,012.700 0 | 8,400.000 0 | 11.906 269 9 | 0.992 695 948 | 1.001 493 870 | 0.994 178 907 | 11.836 802 500 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Iteration Results</th> <th>CTS_{FP}</th> <th>CPS_{FP}</th> <th>CTL_{FP}</th> <th>CPL_{FP}</th> <th>$CTPL_{FP}$</th> <th>CPV_{run} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr> <td>Gasoline, Napthene</td> <td>1.000 197 173</td> <td>1.000 109 579</td> <td>0.992 675 865</td> <td>1.001 513 182</td> <td>0.994 177 964</td> <td>11.903 204 300</td> <td>1</td> </tr> <tr> <td>Gasoline, Napthene</td> <td>1.000 197 545</td> <td>1.000 109 726</td> <td>0.992 663 209</td> <td>1.001 514 779</td> <td>0.994 166 874</td> <td>11.901 372 300</td> <td>2</td> </tr> <tr> <td>Gasoline, Napthene</td> <td>1.000 196 615</td> <td>1.000 109 107</td> <td>0.992 693 402</td> <td>1.001 508 020</td> <td>0.994 190 403</td> <td>11.902 820 400</td> <td>3</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>4</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>5</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>6</td> </tr> <tr> <td></td> <td>1.000 197 111</td> <td>1.000 109 471</td> <td>0.992 677 492</td> <td>1.001 511 994</td> <td>0.994 178 414</td> <td>11.902 465 700</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | Iteration Results | CTS_{FP} | CPS_{FP} | CTL_{FP} | CPL_{FP} | $CTPL_{FP}$ | CPV_{run} Bbls | Run | Gasoline, Napthene | 1.000 197 173 | 1.000 109 579 | 0.992 675 865 | 1.001 513 182 | 0.994 177 964 | 11.903 204 300 | 1 | Gasoline, Napthene | 1.000 197 545 | 1.000 109 726 | 0.992 663 209 | 1.001 514 779 | 0.994 166 874 | 11.901 372 300 | 2 | Gasoline, Napthene | 1.000 196 615 | 1.000 109 107 | 0.992 693 402 | 1.001 508 020 | 0.994 190 403 | 11.902 820 400 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | | 1.000 197 111 | 1.000 109 471 | 0.992 677 492 | 1.001 511 994 | 0.994 178 414 | 11.902 465 700 | Avg |
| Iteration Results | CTS_{FP} | CPS_{FP} | CTL_{FP} | CPL_{FP} | $CTPL_{FP}$ | CPV_{run} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 197 173 | 1.000 109 579 | 0.992 675 865 | 1.001 513 182 | 0.994 177 964 | 11.903 204 300 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 197 545 | 1.000 109 726 | 0.992 663 209 | 1.001 514 779 | 0.994 166 874 | 11.901 372 300 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | 1.000 197 111 | 1.000 109 471 | 0.992 677 492 | 1.001 511 994 | 0.994 178 414 | 11.902 465 700 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>1 means ΔCPV Passed</th> <th>ΔP_{B_SET} kg/m³</th> <th>ΔT_{P_SET} °F</th> <th>ΔP_{P_SET} psig</th> <th>ΔQ_{MM_SET} %</th> <th>r% CPV</th> <th>CPV_{set}</th> <th>CPV_{set} Bbls</th> <th></th> </tr> </thead> <tbody> <tr> <td>Runs 1-3 Runs 2-4 Runs 3-5 Runs 4-6</td> <td>1</td> <td>0.292</td> <td>0.050</td> <td>1.05</td> <td>0.0</td> <td>0.015</td> <td>Pass</td> <td>11.902 465 700</td> </tr> <tr> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>Runs 1-3</td> </tr> <tr> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>Runs 2-4</td> </tr> <tr> <td></td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>Runs 3-5</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>Runs 4-6</td> </tr> </tbody> </table> | | | | | | | | 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{MM_SET} % | r% CPV | CPV_{set} | CPV_{set} Bbls | | Runs 1-3 Runs 2-4 Runs 3-5 Runs 4-6 | 1 | 0.292 | 0.050 | 1.05 | 0.0 | 0.015 | Pass | 11.902 465 700 | | NA | NA | NA | NA | NA | - | - | Runs 1-3 | | NA | NA | NA | NA | NA | - | - | Runs 2-4 | | NA | NA | NA | NA | NA | - | - | Runs 3-5 | | | | | | | | | Runs 4-6 | | | | | | | | | | |
| 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{MM_SET} % | r% CPV | CPV_{set} | CPV_{set} Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 Runs 2-4 Runs 3-5 Runs 4-6 | 1 | 0.292 | 0.050 | 1.05 | 0.0 | 0.015 | Pass | 11.902 465 700 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | NA | NA | NA | NA | NA | - | - | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | NA | NA | NA | NA | NA | - | - | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | NA | NA | NA | NA | NA | - | - | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example B.1 - Calibration Set II - 2 of 2

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| Washington, D.C., USA | | | | | | | | | |
|--|---------------------------------------|------------------------|---------------------------------|--------------------------------|------------------------------|---------------------------|-------------------------|---|---------------|
| BPV Determination using Master Meter - Calibration Set III | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start | | Stop |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | 1 | | Stop 1 |
| Fluid or Batch | RBOB | | Flow Design | Bidirectional | | Time | 14-Feb-24 | | 14-Feb-24 |
| Ch 11.1 | Products | | Wall Design | Single | | Totalizer | 8:21:18 AM | | 11:21:18 AM |
| T _B | 60.0 °F | | Detector | Internal | | Fluid, Batch No. | 2,342,501.020 | | 2,343,601.020 |
| P _B | 0.0 psig | | Displacer | Free Sphere | | API ₆₀ | Products | | Products |
| Master Meter | | | Wall Material | 300 SS | | ρ ₆₀ | 60.8 | | 60.6 |
| Flowmeter ID | 200 | | Rod Material | NA | | API ₁₅ | 735.210 | | 735.710 |
| Manufacturer | API | | GL _P | 0.000 006 20 | | per °F | 60.7 | | 60.5 |
| Model | API-PD | | GL _D | NA | | per °F | 735.715 | | 736.216 |
| Nominal Size | 4 inch | | E _P | 030 000 000 | | per psig | 61.7 | | 61.5 |
| Type | PD | | ID _P | 21.562 0 | | inch | 731.158 | | 731.660 |
| Proving Result | MMF | | WT _P | 1.219 0 | | inch | 882.146 | | 881.970 |
| T _F Comp | No | | Serial No. | Bidi-SI-001 | | Flowrate, Q _{av} | 73.100 | | 73.240 |
| P _F Comp | No | | Switches | 9206 to 9236 | | T _{MP_AVG} | 187.7 | | 188.3 |
| NKF | 8,400.000 0 P / Bbl | | | | | P _{MP_AVG} | 1 | | 1 |
| Cartridge No. | API-0011 | | | | | Trips per Run | Runs 1-5 | | Runs 1-5 |
| Density Method | | | Calibration Set Criteria | | | Roundtrips | 0.018 | | 0.017 |
| ρ _{obs} Method | Continuous | | ΔMMF _{SET} | ≤ 0.02 % | | Repeatability (r) | 0.020 | | 0.020 |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 % | | Allowable (r) | Pass | | Pass |
| DMF | 0.999 8 | | (r) CPV _{RUN} | ≤ 0.02 % | | (r) Pass/Fail | 1.000 099 0 | | 1.000 154 0 |
| HYC Factor | No | | | | | MMF | NA | | 0.006 |
| API Chapter 12.4.2 | | | Spot Sample | | | Allowable ± ΔMMF | NA | | 0.020 |
| USC_60 Measurement Units | | | ρ _{60_START} | NA kg/m ³ | | ΔMMF Pass/Fail | NA | | Pass |
| Sampling Method - Continuous | | | ρ _{60_STOP} | NA kg/m ³ | | | | | |
| BPV - Standard Method | | | ρ _{60_SET} | NA kg/m ³ | | | | | |
| Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs | | | MMF _{SET} | 1.000 126 5 | | | | | |
| Refined Product - Tables 5B/6B | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | | |
| | ρ _{obs} kg/m ³ | T _{dm} °F | P _{dm} psig | T _{FP_INLET} °F | T _{FP_OUTLET} °F | T _{MM} °F | T _{FD} °F | Base Density ρ _B kg/m ³ | Run |
| | 729.748 | 73.230 | 174.5 | 73.070 | 73.200 | 73.390 | | 735.415 | 1 |
| | 729.843 | 73.230 | 175.2 | 73.050 | 73.120 | 73.390 | | 735.506 | 2 |
| | 729.545 | 73.270 | 175.2 | 73.080 | 73.140 | 73.400 | | 735.228 | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| | 729.712 | 73.240 | 175.0 | 73.070 | 73.150 | 73.390 | | 735.383 | Avg |
| Ch 11.1 Iteration Results | | | | | | | | | |
| | N or N _i Pulses | Q _{MM} BPH | P _{FP_INLET} psig | P _{FP_OUTLET} psig | P _{MM} psig | T _{FP} °F | P _{FP} psig | | Run |
| | Gasoline, Napthene | 100,015.000 | 882.125 | 176.1 | 173.8 | 185.4 | 73.135 0 | 174.95 | 1 |
| | Gasoline, Napthene | 100,018.000 | 882.131 | 176.7 | 174.0 | 185.9 | 73.085 0 | 175.35 | 2 |
| | Gasoline, Napthene | 100,022.000 | 882.129 | 176.2 | 174.0 | 186.4 | 73.110 0 | 175.10 | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| | 100,018.300 0 | 882.128 | 176.3 | 173.9 | 185.9 | 73.110 0 | 175.10 | | Avg |

Example B.1 - Calibration Set III - 1 of 2

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|---|--|--|-----------------------------|---------------------------|--------------------|----------------------------|----------------------------|-------------------------------|--|---------------------------|-----------------------------|---------------------------|--|----------------------------|----------------------------|--------------------|----------------|---------------|---------------|---------------|---------------|----------------|-------|--------------------|----------------|---------------|------------------|---------------|---------------|----------------|----|--------------------|---------------|---------------|---------------|---------------|---------------|----------------|----|----|---|---|----------|----------|----|----|----|----|----|---|---|----------|--|--|---|--|--|--|--|--|--|--|---|---------------|---------------|---------------|---------------|---------------|---------------|----------------|-----|
| BPV Determination using Master Meter - Calibration Set III | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Continuous BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Refined Product - Tables 5B/6B | | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; text-align: right;">ΔMMF_{SET}</td> <td style="width: 50%; text-align: center;">Pass</td> <td style="width: 50%; text-align: right;">-</td> </tr> <tr> <td style="text-align: right;">(r) ICPV_{SET}</td> <td style="text-align: center;">Pass</td> <td style="text-align: right;">-</td> </tr> <tr> <td style="text-align: right;">(r) CPV_{SET}</td> <td style="text-align: center;">Pass</td> <td style="text-align: right;">-</td> </tr> </table> | | ΔMMF_{SET} | Pass | - | (r) ICPV _{SET} | Pass | - | (r) CPV _{SET} | Pass | - | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="2" style="text-align: center;">Report Summary</th> </tr> <tr> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> <tr> <td>Report No.</td> <td>Start</td> </tr> <tr> <td>Date</td> <td>Stop</td> </tr> <tr> <td>Time</td> <td>1-Jan-00</td> </tr> <tr> <td>Fluid, Batch No.</td> <td>00:00:00</td> </tr> <tr> <td></td> <td>2342501.02</td> </tr> <tr> <td></td> <td>2343601.02</td> </tr> </table> | | | | Report Summary | | Prior | Current | Report No. | Start | Date | Stop | Time | 1-Jan-00 | Fluid, Batch No. | 00:00:00 | | 2342501.02 | | 2343601.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF_{SET} | Pass | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) ICPV _{SET} | Pass | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) CPV _{SET} | Pass | - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report Summary | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 1-Jan-00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | 00:00:00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 2342501.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 2343601.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>N or N_i Pulses</th> <th>NKF P / Bbl</th> <th>IV_{MM}</th> <th>CTL_{MM}</th> <th>CPL_{MM}</th> <th>CTPL_{MM}</th> <th>GSV_{MM} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr> <td>100,015.000</td> <td>8,400.000 0</td> <td>11.906 547 6</td> <td>0.990 768 877</td> <td>1.001 518 360</td> <td>0.992 273 221</td> <td>11.816 042 900</td> <td>1</td> </tr> <tr> <td>100,018.000</td> <td>8,400.000 0</td> <td>11.906 904 8</td> <td>0.990 770 609</td> <td>1.001 521 790</td> <td>0.992 278 354</td> <td>11.816 458 500</td> <td>2</td> </tr> <tr> <td>100,022.000</td> <td>8,400.000 0</td> <td>11.907 381 0</td> <td>0.990 758 393</td> <td>1.001 528 016</td> <td>0.992 272 288</td> <td>11.816 858 800</td> <td>3</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>4</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>5</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>6</td> </tr> <tr> <td>100,018.300 0</td> <td>8,400.000 0</td> <td>11.906 944 5</td> <td>0.990 765 960</td> <td>1.001 522 722</td> <td>0.992 274 621</td> <td>11.816 453 400</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | N or N _i Pulses | NKF P / Bbl | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} Bbls | Run | 100,015.000 | 8,400.000 0 | 11.906 547 6 | 0.990 768 877 | 1.001 518 360 | 0.992 273 221 | 11.816 042 900 | 1 | 100,018.000 | 8,400.000 0 | 11.906 904 8 | 0.990 770 609 | 1.001 521 790 | 0.992 278 354 | 11.816 458 500 | 2 | 100,022.000 | 8,400.000 0 | 11.907 381 0 | 0.990 758 393 | 1.001 528 016 | 0.992 272 288 | 11.816 858 800 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | 100,018.300 0 | 8,400.000 0 | 11.906 944 5 | 0.990 765 960 | 1.001 522 722 | 0.992 274 621 | 11.816 453 400 | Avg |
| N or N _i Pulses | NKF P / Bbl | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,015.000 | 8,400.000 0 | 11.906 547 6 | 0.990 768 877 | 1.001 518 360 | 0.992 273 221 | 11.816 042 900 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,018.000 | 8,400.000 0 | 11.906 904 8 | 0.990 770 609 | 1.001 521 790 | 0.992 278 354 | 11.816 458 500 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,022.000 | 8,400.000 0 | 11.907 381 0 | 0.990 758 393 | 1.001 528 016 | 0.992 272 288 | 11.816 858 800 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 100,018.300 0 | 8,400.000 0 | 11.906 944 5 | 0.990 765 960 | 1.001 522 722 | 0.992 274 621 | 11.816 453 400 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Iteration Results</th> <th>CTS_{FP}</th> <th>CPS_{FP}</th> <th>CTL_{FP}</th> <th>CPL_{FP}</th> <th>CTPL_{FP}</th> <th>CPV_{run} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr> <td>Gasoline, Napthene</td> <td>1.000 244 331</td> <td>1.000 103 152</td> <td>0.990 945 132</td> <td>1.001 431 033</td> <td>0.992 363 208</td> <td>11.902 837 700</td> <td>1</td> </tr> <tr> <td>Gasoline, Napthene</td> <td>1.000 243 401</td> <td>1.000 103 388</td> <td>0.990 981 383</td> <td>1.001 433 360</td> <td>0.992 401 816</td> <td>11.902 801 500</td> <td>2</td> </tr> <tr> <td>Gasoline, Napthene</td> <td>1.000 243 866</td> <td>1.000 103 241</td> <td>0.990 958 917</td> <td>1.001 433 403</td> <td>0.992 378 360</td> <td>11.903 470 300</td> <td>3</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>4</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>5</td> </tr> <tr> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>6</td> </tr> <tr> <td></td> <td>1.000 243 866</td> <td>1.000 103 260</td> <td>0.990 961 811</td> <td>1.001 432 599</td> <td>0.992 381 461</td> <td>11.903 036 500</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} Bbls | Run | Gasoline, Napthene | 1.000 244 331 | 1.000 103 152 | 0.990 945 132 | 1.001 431 033 | 0.992 363 208 | 11.902 837 700 | 1 | Gasoline, Napthene | 1.000 243 401 | 1.000 103 388 | 0.990 981 383 | 1.001 433 360 | 0.992 401 816 | 11.902 801 500 | 2 | Gasoline, Napthene | 1.000 243 866 | 1.000 103 241 | 0.990 958 917 | 1.001 433 403 | 0.992 378 360 | 11.903 470 300 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | | 1.000 243 866 | 1.000 103 260 | 0.990 961 811 | 1.001 432 599 | 0.992 381 461 | 11.903 036 500 | Avg |
| Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 244 331 | 1.000 103 152 | 0.990 945 132 | 1.001 431 033 | 0.992 363 208 | 11.902 837 700 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 243 401 | 1.000 103 388 | 0.990 981 383 | 1.001 433 360 | 0.992 401 816 | 11.902 801 500 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Gasoline, Napthene | 1.000 243 866 | 1.000 103 241 | 0.990 958 917 | 1.001 433 403 | 0.992 378 360 | 11.903 470 300 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | 1.000 243 866 | 1.000 103 260 | 0.990 961 811 | 1.001 432 599 | 0.992 381 461 | 11.903 036 500 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>1 means ΔCPV Passed</th> <th>ΔP_{B_SET} kg/m³</th> <th>ΔT_{P_SET} °F</th> <th>ΔP_{P_SET} psig</th> <th>ΔQ_{MM_SET} %</th> <th>r% CPV</th> <th>CPV_{set}</th> <th>CPV_{set} Bbls</th> <th></th> </tr> </thead> <tbody> <tr> <td>Runs 1-3</td> <td>1</td> <td>0.278</td> <td>0.050</td> <td>0.40</td> <td>0.0</td> <td>0.006</td> <td>Pass</td> <td>11.903 036 500</td> </tr> <tr> <td>Runs 2-4</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>Runs 1-3</td> </tr> <tr> <td>Runs 3-5</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>Runs 2-4</td> </tr> <tr> <td>Runs 4-6</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>Runs 3-5</td> </tr> </tbody> </table> | | | | | | | | 1 means Δ CPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{MM_SET} % | r% CPV | CPV _{set} | CPV _{set} Bbls | | Runs 1-3 | 1 | 0.278 | 0.050 | 0.40 | 0.0 | 0.006 | Pass | 11.903 036 500 | Runs 2-4 | NA | NA | NA | NA | NA | - | - | Runs 1-3 | Runs 3-5 | NA | NA | NA | NA | NA | - | - | Runs 2-4 | Runs 4-6 | NA | NA | NA | NA | NA | - | - | Runs 3-5 | | | | | | | | | | | | | | | | | | | |
| 1 means Δ CPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{MM_SET} % | r% CPV | CPV _{set} | CPV _{set} Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 | 1 | 0.278 | 0.050 | 0.40 | 0.0 | 0.006 | Pass | 11.903 036 500 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 2-4 | NA | NA | NA | NA | NA | - | - | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 3-5 | NA | NA | NA | NA | NA | - | - | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 4-6 | NA | NA | NA | NA | NA | - | - | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 40%;">Signature</th> <th style="width: 20%;">Date</th> <th style="width: 40%;">Company</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td>API Midstream Representative</td> </tr> <tr> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> <tr> <td></td> <td></td> <td></td> </tr> </tbody> </table> | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example B.1 - Calibration Set III - 2 of 2

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Example B.2 – Standard Method

USC Units, Spot Sampling, Master Prover - Unidirectional Captive Displacer, Master Meter - Turbine,
MF r% - Moving Range, MF Method - IMF, Field Prover - Unidirectional Captive Displacer

DRAFT

| Master Prover | |
|-----------------|--|
| BPV Units | 0 (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) |
| Detector Design | 1 (0-Internal, 1-External) |
| Wall Material | 3 (1-CS, 2-304SS, 3-316SS, 4-17-4PH) |
| Rod Material | 3 (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) |
| Certificate BPV | 5,725.326 1 cubic inches at 60.0 °F, 0.0 psig |

| Base Prover Volume (BPV) | | | |
|--------------------------|------------------------------------|-----------------------------------|-----------------------------------|
| | BPV ₆₀ Barrels | BPV ₁₅ Cubic Meters | BPV ₂₀ Cubic Meters |
| | 0.590 118 130 282 | 0.093 818 780 000 | 0.093 841 327 000 |
| Decimals | 10 | 11 | 11 |
| Conversion | in ³ / Bbl 9.702E+03 | mL / M ³ 1.00E+06 | mL / M ³ 1.00E+06 |
| Rnd'd BPV | 0.590 118 130 300 | 0.093 818 780 000 | 0.093 841 327 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to 10 digits (the appropriate decimal place) to increase the precision of the Master Prover's BPV, not the uncertainty of the Master Prover's BPV.

| | T _B | |
|---------------------------|----------------|-----------------------------------|
| Decimal Base CTS | 60.0 | °F |
| Decimal BPV ₆₀ | 9 | - |
| Decimal BPV _{SI} | 4 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV | 3 | mL at 15.0 °C and 0.0 kPag |
| | 10 | Barrels |

Detector Design,

CTS_P = [1 + (T_P - T_B) x GL_P]³, for detectors mounted in calibrated section

CTS_P = [1 + (T_P - T_B) x GL_P]² x [1 + (T_D - T_B) x GL_D], for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F

BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig

BPV₁₅ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C

BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig

BPV₁₅ = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = ROUND(BPV₁₅ x Base CTS₂₀, 3) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C

BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 x Base CTS₆₀, 4) = in³ at 60.0 °F, 0.0 psig

BPV₁₅ = ROUND(BPV₂₀ x Base CTS₁₅, 3) = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| T _B | 60.0 °F | 15.0 °C | 20.0 °C |
|-----------------|--------------|--------------|--------------|
| GL _P | 0.000 008 90 | 0.000 016 02 | 0.000 016 02 |
| GL _D | 0.000 008 90 | 0.000 016 02 | 0.000 016 02 |

| | Base CTS ₆₀ | Base CTS ₁₅ | Base CTS ₂₀ |
|------------------------|------------------------|------------------------|------------------------|
| Base CTS ₆₀ | 1.000 000 000 | 1.000 026 700 | 0.999 786 415 |
| Base CTS ₁₅ | 0.999 973 300 | 1.000 000 000 | 0.999 759 719 |
| Base CTS ₂₀ | 1.000 213 615 | 1.000 240 319 | 1.000 000 000 |

| Base Unit Volume | |
|-------------------|---|
| BPV ₆₀ | 5,725.326 1 cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 93,818.780 mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 93,841.327 mL at 20.0 °C and 0.0 kPag |

| API Properties | | |
|---|------------------------------------|---------------------------------------|
| Linear Coefficient of Thermal Expansion, GL | | |
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,3,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar TM | 0.000 001 44 | 0.000 000 80 |

Notes:

(1) The User/Owner should obtain GL values from the prover manufacturer.

(2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.

(3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.

(4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.

(5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Example B.2 - Expanded Discrimination of Master Prover's BPV

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| Washington, D.C., USA | | | | | | | | | |
|---|-------------------|-------------------------------|----------------------------|--------------------------|-----------------------|-----------------------|---|---------------------|-------------------|
| Master Meter Proving Report | | | | | | | | | |
| General Data | | | Displacement Prover | | | Report Summary | | | |
| Operator | API Midstream | | Manufacturer | API | | Report No. | Start | Stop | |
| Station Name | MPMS | | Prover Type | Displacement | | Date | Start I | Stop I | |
| Ch 11.1 | Tables 5A/6A | | Flow Design | Unidirectional | | Time | 14-Feb-24 | 14-Feb-24 | |
| T _B | 60.0 °F | | Wall Design | Single | | Totalizer | 8:21:18 | 11:21:18 | |
| P _B | 0.0 psig | | Detector | External | | Fluid, Batch No. | 2,342,501.020 | 2,343,601.020 | Bbl |
| Master Meter | | | Displacer | Captive Displacer | | API ₆₀ | Crude | Crude | |
| Flowmeter ID | 400 | | Wall Material | 316SS | | API ₁₅ | 35.1 | 35.2 | °API |
| Manufacturer | API | | Rod Material | 316SS | | ρ ₆₀ | 848.597 | 848.217 | kg/m ³ |
| Model | Turbine | | GL _P | 0.000 008 90 | | API ₁₅ | 35.0 | 35.1 | °API |
| Nominal Size | 3 inch | | GL _D | 0.000 008 90 | | ρ ₁₅ | 848.999 | 848.619 | kg/m ³ |
| Type | Turbine | | E _P | 028 000 000 | | API ₂₀ | 35.6 | 35.7 | °API |
| Proving Result | MMF | | ID _P | 17.400 0 | | ρ ₂₀ | 845.377 | 844.995 | kg/m ³ |
| T _F Comp | No | | WT _P | 1.825 0 | | Flowrate, Q | 364.966 | 365.440 | BPH |
| P _F Comp | No | | Calibration Date | 2021-09-04 | | T _{P,AVG} | 73.090 | 73.428 | °F |
| NKF | 696.700 0 P / Bbl | | Serial No. | 8904-04 | | P _{P,AVG} | 170.6 | 176.1 | psig |
| Cartridge No. | API-0011 | | Certificate No. | 10101010 | | Trips per Run | 1 | 1 | |
| Density Method | | | Switches | 9201 to 9202 | | Roundtrips | Runs 1-3 | Runs 1-3 | |
| Sample Method | Spot Sample | | BPV | 0.590 118 130 3 Bbl | | Repeatability (r) | 0.004 | 0.002 | % |
| ρ _{obs} Device | Hydrometer | | Spot Sample | | | Allowable (r) | 0.007 | 0.007 | % |
| DMF | NA | | API _{ind} | 848.217 °API | | (r) Pass/Fail | Pass | Pass | |
| HYC Factor | Yes | | ρ _{ind} | 60.000 kg/m ³ | | MMF | 0.999 997 8 | 0.999 986 5 | % |
| API MPMS Chapter 12.4.2 Measurement Units - USC Sampling Method - Spot Meter Factor Method - Intermediate (or IMF) Repeatability Method (r%) - Moving Range API MPMS Chapter 11.1 - Tables 5A/6A | | | T _{obs} | 0.0 °F | | ΔMMF | NA | (0.001) | % |
| | | | P _{obs} | 0.0 psig | | Allowable ± ΔMMF | NA | 0.020 | % |
| | | | | | ΔMMF Pass/Fail | NA | Pass | | |
| | | | | | | | | | |
| Prior vs Current | | | | | | | | | |
| ΔQ | | | | | | | | | 0.1 % |
| ΔT _P | | | | | | | | | 0.338 °F |
| Base Density | | Roundtrip Measurements | | | | | | Base Density | |
| API _B | ρ _{ind} | T _{dm} | P _{dm} | T _{P,INLET} | T _{P,OUTLET} | T _M | T _D | ρ _B | Run |
| °API | kg/m ³ | °F | psig | °F | °F | °F | °F | kg/m ³ | |
| 35.2 | | | | 73.480 | 73.360 | 73.210 | 75.020 | 848.217 | 1 |
| 35.2 | | | | 73.510 | 73.430 | 73.280 | 75.140 | 848.217 | 2 |
| 35.2 | | | | 73.470 | 73.320 | 73.230 | 75.120 | 848.217 | 3 |
| NA | | | | | | | | | 4 |
| NA | | | | | | | | | 5 |
| NA | | | | | | | | | 6 |
| NA | | | | | | | | | 7 |
| NA | | | | | | | | | 8 |
| NA | | | | | | | | | 9 |
| NA | | | | | | | | | 10 |
| 35.2 | NA | NA | NA | NA | NA | 73.240 | 75.090 | 848.217 | Runs 1-3 |
| Commodity Type | | Roundtrip Measurements | | | | | T_P and P_P Values | | |
| | | N or N _i | Q _M | P _{P,INLET} | P _{P,OUTLET} | P _M | T _{P,RUN} | P _{P,RUN} | Run |
| | | Pulses | BPH | psig | psig | psig | °F | psig | |
| Crude Oil, JP-4 | | 411.278 | 365.408 0 | 177.9 | 174.2 | 173.5 | 73.420 0 | 176.05 | 1 |
| Crude Oil, JP-4 | | 411.291 | 365.287 0 | 178.0 | 174.3 | 173.6 | 73.470 0 | 176.15 | 2 |
| Crude Oil, JP-4 | | 411.294 | 365.618 0 | 177.9 | 174.2 | 173.5 | 73.395 0 | 176.05 | 3 |
| NA | | | | | | | | | 4 |
| NA | | | | | | | | | 5 |
| NA | | | | | | | | | 6 |
| NA | | | | | | | | | 7 |
| NA | | | | | | | | | 8 |
| NA | | | | | | | | | 9 |
| NA | | | | | | | | | 10 |
| Runs 1-3 | | 411.287 7 | 365.440 0 | NA | NA | 173.5 | 73.428 3 | 176.08 | Runs 1-3 |

Example B.2 - Calibration Set I - Stop Proving Report - 1 of 2

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| Washington, D.C., USA Master Meter Proving Report | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|---|---|------------------|---|----------------------|------------------------------|-------------------------|----------|----|----|-------|---------|------------|---------|--------|------|-----------|-----------|-------|----------|----------|------------------|-------|-------|-------|--|-------|--|--|--|---|--|--------------|--------------|--------------|--|--|--|--|--|--|--|--------------|------------|-----|
| API MPMS Chapter 12.4.2 Measurement Units - USC Sampling Method - Spot Meter Factor Method - Intermediate (or IMF) Repeatability Method (r%) - Moving Range API MPMS Chapter 11.1 - Tables 5A/6A | | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse; margin-top: 5px;"> <thead> <tr> <th></th> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start I</td> <td style="text-align: center;">Stop I</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">14-Feb-24</td> <td style="text-align: center;">14-Feb-24</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">08:21:18</td> <td style="text-align: center;">11:21:18</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">Crude</td> <td style="text-align: center;">Crude</td> </tr> </tbody> </table> | | | | | | | Prior | Current | Report No. | Start I | Stop I | Date | 14-Feb-24 | 14-Feb-24 | Time | 08:21:18 | 11:21:18 | Fluid, Batch No. | Crude | Crude | | | | | | | | | | | | | | | | | | | | | |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start I | Stop I | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 08:21:18 | 11:21:18 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Crude | Crude | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run | BPV Bbl | CTS _p | CPS _p | Rnd CTL _p | Rnd CPL _p | Rnd CTPL _p | GSV _p Bbl | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | 0.590 118 130 3 | 1.000 372 600 | 1.000 059 947 | 0.993 624 077 | 1.000 925 468 | 0.994 543 644 | 0.587 152 110 0 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 | 0.590 118 130 3 | 1.000 374 559 | 1.000 059 981 | 0.993 600 277 | 1.000 926 150 | 0.994 520 500 | 0.587 139 616 0 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 | 0.590 118 130 3 | 1.000 373 045 | 1.000 059 947 | 0.993 635 976 | 1.000 925 390 | 0.994 555 477 | 0.587 159 356 8 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 | 0.590 118 130 3 | 1.000 373 401 | 1.000 059 958 | 0.993 620 110 | 1.000 925 669 | 0.994 539 874 | 0.587 150 360 9 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run | N or N _i | NKF P / Bbl | IV _M | Rnd CTL _M | Rnd CPL _M | Rnd CTPL _M | ISV _M Bbl | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | 411.278 | 696.700 0 | 0.590 322 951 1 | 0.993 724 032 | 1.000 911 405 | 0.994 629 717 | 0.587 152 749 8 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 | 411.291 | 696.700 0 | 0.590 341 610 4 | 0.993 690 714 | 1.000 912 146 | 0.994 597 105 | 0.587 152 056 7 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 | 411.294 | 696.700 0 | 0.590 345 916 5 | 0.993 714 512 | 1.000 911 467 | 0.994 620 250 | 0.587 170 003 0 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | 8 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 | 411.287 7 | 696.700 0 | 0.590 336 826 0 | 0.993 709 753 | 1.000 911 673 | 0.994 615 691 | 0.587 158 269 8 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run | '1' indicates Repeatability (r%) criteria satisfied | Repeatability (r%) <table border="1" style="width: 100%; border-collapse: collapse; margin-top: 5px;"> <thead> <tr> <th style="width: 50%;"></th> <th style="width: 50%;"></th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">Actual</td> <td style="text-align: center;">Allowable</td> </tr> <tr> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> </tr> <tr> <td style="text-align: center;">NA</td> <td style="text-align: center;">NA</td> </tr> <tr> <td style="text-align: center;">0.002</td> <td style="text-align: center;">0.007</td> </tr> <tr> <td></td> <td style="text-align: center;">0.014</td> </tr> <tr> <td></td> <td style="text-align: center;">0.020</td> </tr> <tr> <td></td> <td style="text-align: center;">0.025</td> </tr> <tr> <td></td> <td style="text-align: center;">0.031</td> </tr> <tr> <td></td> <td style="text-align: center;">0.036</td> </tr> <tr> <td></td> <td style="text-align: center;">0.041</td> </tr> <tr> <td></td> <td style="text-align: center;">0.045</td> </tr> </tbody> </table> | | | | Actual | Allowable | NA | NA | NA | NA | 0.002 | 0.007 | | 0.014 | | 0.020 | | 0.025 | | 0.031 | | 0.036 | | 0.041 | | 0.045 | Meter Factor Method - Intermediate (or IMF) <table border="1" style="width: 100%; border-collapse: collapse; margin-top: 5px;"> <thead> <tr> <th style="width: 100%;"></th> </tr> </thead> <tbody> <tr> <td style="text-align: center;">Repeatability Method (r%) - Moving Range</td> </tr> </tbody> </table> | | | Repeatability Method (r%) - Moving Range | IMF <table border="1" style="width: 100%; border-collapse: collapse; margin-top: 5px;"> <tbody> <tr><td style="text-align: center;">0.999 998 91</td></tr> <tr><td style="text-align: center;">0.999 978 81</td></tr> <tr><td style="text-align: center;">0.999 981 87</td></tr> <tr><td></td></tr> <tr><td></td></tr> <tr><td></td></tr> <tr><td></td></tr> <tr><td></td></tr> <tr><td></td></tr> <tr><td></td></tr> <tr> <td style="text-align: center;">0.999 986 50</td> <td style="text-align: center;">MMF</td> </tr> </tbody> </table> | 0.999 998 91 | 0.999 978 81 | 0.999 981 87 | | | | | | | | 0.999 986 50 | MMF | Run |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Actual | Allowable | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NA | NA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| NA | NA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.002 | 0.007 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.014 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.020 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.025 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.031 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.036 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.041 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.045 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| Repeatability Method (r%) - Moving Range | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.999 998 91 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.999 978 81 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.999 981 87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 0.999 986 50 | MMF | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | | | | | | | | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3 | | | | | | | | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | 7 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 9 | | | | | | | | 9 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | 10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Pass | | 0.002 | | | | | | MMF | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MMF Rounded to 7 decimal places | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example B.2 - Calibration Set I - Stop Proving Report - 2 of 2

| Field Prover | |
|--|--|
| Measurement Units | 0 (0-USC ₆₀ , 1-SI ₁₅ , 2-SI ₂₀) |
| Detector Design | 1 (0-Internal, 1-External) |
| Wall Material | 3 (1-CS, 2-304SS, 3-316SS, 4-17-4PH) |
| Rod Material | 3 (0-NA, 1-CS, 2-304SS, 3-316SS, 4-17-4PH, 5-Invar) |
| Source for GL _{MP} , GL _{md} , E _{MP} | 1 (0-Prover Manufacturer, 1-API Table) |
| BPV _P | 5,725.326 1 cubic inches at 60.0 °F, 0.0 psig |

| Base Prover Volume (BPV) | | | |
|--------------------------|------------------------------------|-----------------------------------|-----------------------------------|
| | BPV ₆₀ Barrels | BPV ₁₅ Cubic Meters | BPV ₂₀ Cubic Meters |
| | 0.590 118 130 282 | 0.093 818 780 000 | 0.093 841 327 000 |
| Decimals | 6 | 7 | 7 |
| Conversion | in ³ / Bbl 9.702E+03 | mL / M ³ 1.00E+06 | mL / M ³ 1.00E+06 |
| Rnd'd BPV | 0.590 118 000 000 | 0.093 818 800 000 | 0.093 841 300 000 |

Note: This Worksheet produces a BPV₆₀ or BPV_{SI} to 6 digits (the appropriate decimal place).

| | T _B | |
|---------------------------|----------------|-----------------------------------|
| Decimal Base CTS | 60.0 | °F |
| Decimal BPV ₆₀ | 9 | - |
| Decimal BPV _{SI} | 4 | cubic inches at 60.0 °F, 0.0 psig |
| Decimal BPV | 3 | mL at 15.0 °C and 0.0 kPag |
| Decimal BPV | 6 | Barrels, 6 digits |
| Decimal BPV | 7 | Cubic Meters, 6 digits |

Detector Design,

CTS_P = [1 + (T_P - T_B) x GL_P]³, for detectors mounted in calibrated section

CTS_P = [1 + (T_P - T_B) x GL_P]² x [1 + (T_D - T_B) x GL_d], for detectors mounted on external shaft

If Measurement Units = 0, then BPV in cubic inches, T_B is 60.0 °F

BPV₆₀ = cubic inches at 60.0 °F, 0.0 psig

BPV₁₅ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₁₅, 12) = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = ROUND(BPV₆₀ x 16.387 064 x Base CTS₂₀, 12) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 1, then BPV in mL, T_B is 15.0 °C

BPV₆₀ = ROUND(BPV₁₅ / 16.387 064 x Base CTS₆₀, 12) = in³ at 60.0 °F, 0.0 psig

BPV₁₅ = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = ROUND(BPV₁₅ x Base CTS₂₀, 12) = mL at 20.0 °C, 0.0 kPag

If Measurement Units = 2, then BPV in mL, T_B is 20.0 °C

BPV₆₀ = ROUND(BPV₂₀ / 16.387 064 x Base CTS₆₀, 12) = in³ at 60.0 °F, 0.0 psig

BPV₁₅ = ROUND(BPV₂₀ x Base CTS₁₅, 12) = mL at 15.0 °C, 0.0 kPag

BPV₂₀ = mL at 20.0 °C, 0.0 kPag

| | GL _P | GL _D | T _B |
|--|-----------------|-----------------|----------------|
| | 0.000 008 90 | 0.000 016 02 | 0.000 016 02 |
| | 0.000 008 90 | 0.000 016 020 | 0.000 016 020 |
| | 60.0 | 15.0 | 20.0 |

| | Base CTS ₆₀ | Base CTS ₁₅ | Base CTS ₂₀ |
|--|------------------------|------------------------|------------------------|
| | 1.000 000 000 | 1.000 026 700 | 0.999 786 415 |
| | 0.999 973 300 | 1.000 000 000 | 0.999 759 719 |
| | 1.000 213 615 | 1.000 240 319 | 1.000 000 000 |

| | Base Unit Volume |
|-------------------|---|
| BPV ₆₀ | 5,725.326 1 cubic inches at 60.0 °F, 0.0 psig |
| BPV ₁₅ | 93,818.780 mL at 15.0 °C and 0.0 kPag |
| BPV ₂₀ | 93,841.327 mL at 20.0 °C and 0.0 kPag |

| API Properties | | |
|---|------------------------------------|---------------------------------------|
| Linear Coefficient of Thermal Expansion, GL | | |
| | SI Unit ^{2,4} (per °C) | USC Unit ^{2,3,5} (per °F) |
| Mild Carbon | 0.000 011 16 | 0.000 006 20 |
| 304 SS | 0.000 017 28 | 0.000 009 60 |
| 316 SS | 0.000 016 02 | 0.000 008 90 |
| 17-4PH | 0.000 010 80 | 0.000 006 00 |
| Invar TM | 0.000 001 44 | 0.000 000 80 |

Notes:

(1) The User/Owner should obtain GL values from the prover manufacturer.

(2) The GL values shown above are a function of the materials, operating temperature range, calibration temperature range. Values in **bold face** were obtained from American Society of Metals (ASM) International, 2020 edition.

(3) GL values shown above are applicable from 0 °C to 100 °C (32 °F to 212 °F). If operating outside this range, the GL values depicted are not appropriate.

(4) The SI values of GL per °C **not in bold face**, was obtained by multiplying the USC values, GL per °F, times 1.8.

(5) The USC values per °F **not in bold face**, was obtained by dividing the SI values, GL per °C, by 1.8.

Example B.2 - Field Prover's BPV Conversion

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| Washington, D.C., USA | | | | | | | | | |
|---|----------------------------|--------------------------|-------------------------|---------------------------|-------------------|----------------------------|-------------------|------|--|
| BPV Determination using a Master Meter - Standard Method | | | | | | | | | |
| General Data | | | Master Meter | | | Field Prover | | | |
| API Midstream | Operator | Flowmeter ID | 400 | - | Manufacturer | API | - | | |
| Headquarters | Station Name | Manufacturer | API | - | Prover Design | Displacement | - | | |
| Washington | City, Town | Model | Turbine | - | Flow Design | Unidirectional | - | | |
| D.C. | State, Province | Nominal Size | 3 | inch | Wall Design | Single | - | | |
| USA | Country | Type | PD | - | Detector | External | - | | |
| Crude | Fluid, Batch No. | Proving Result | MMF | - | Displacer | Captive Displacer | - | | |
| Crude | Ch 11.1 | T _F Comp | No | - | Wall Material | 316SS | - | | |
| 60.0 | T _B | P _F Comp | No | - | Rod Material | 316SS | - | | |
| 0.0 | P _B | NKF | 696.700 0 | P / Bbl | GL _P | 0.000 008 90 | per °F | | |
| 14-Feb-2024 | Start Calibration | Cartridge No. | API-0011 | - | GL _D | 0.000 008 90 | per °F | | |
| 14-Feb-2024 | Stop Calibration | | | - | E _P | 028 000 000 | per psig | | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, $r \leq 0.02\%$, for 3 consecutive Calibration Sets Crude Oil - Tables 5A/6A | | | Density Method | | | ID _P | 17.400 0 | inch | |
| | | | ρ _{obs} Method | Spot Sample | - | WT _P | 1.825 0 | inch | |
| | | | ρ _{obs} Device | Online Density | - | Trips per Run | 1 | - | |
| | | | DMF | 0.000 0 | - | Serial No. | Uni-USC-004 | - | |
| | | | HYC Factor | No | - | Switches | 9204 to 9234 | - | |
| | | Calibration Set I | | Calibration Set II | | Calibration Set III | | | |
| | Start | Stop | Start | Stop | Start | Stop | | | |
| Report No. | Start I | Stop I | Start 2 | Stop 2 | Start 3 | Stop 3 | | | |
| Date | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | 14-Feb-24 | | | |
| Crude | Crude | Crude | Crude | Crude | Crude | Crude | | | |
| API _B | 35.1 | 35.2 | 35.2 | 35.1 | 35.1 | 35.1 | °API | | |
| ρ _B | 848.597 | 848.217 | 848.217 | 848.587 | 848.427 | 848.387 | kg/m ³ | | |
| Q _{MM} | 354.990 | 365.438 | 524.145 | 524.785 | 882.146 | 881.970 | BPH | | |
| T _{MP_AVG} | 73.090 | 70.093 | 70.710 | 70.730 | 73.100 | 73.240 | °F | | |
| P _{MP_AVG} | 170.6 | 175.4 | 189.1 | 189.5 | 187.7 | 188.3 | psig | | |
| Roundtrips | Runs 1-3 | Runs 1-3 | Runs 1-5 | Runs 1-5 | Runs 1-5 | Runs 1-5 | | | |
| Repeatability (r) | 0.004 | 0.002 | 0.011 | 0.008 | 0.008 | 0.014 | % | | |
| MMF | 0.999 997 8 | 0.999 986 5 | 1.000 055 2 | 1.000 058 6 | 0.999 845 2 | 0.999 865 5 | - | | |
| MMF _{SET} | NA | 0.999 992 2 | NA | 1.000 056 9 | NA | 0.999 855 4 | - | | |
| ΔMMF | NA | (0.001) | NA | 0.000 | NA | 0.002 | % | | |
| | ΔMMF _{SET} | Pass | | Pass | | Pass | | | |
| | (r) CPV _{RUN} | Pass | | Pass | | Pass | | | |
| | (R) CPV _{SET} | NA | | Pass | | Pass | | | |
| | ΔQ _{SET} | NA | | Pass | | Pass | | | |
| | Selected Set | Runs 4-6 | | Runs 1-3 | | Runs 1-3 | | | |
| | CPV _{SET} | 0.590 108 4 | Bbls | 0.590 126 5 | Bbls | 0.590 127 7 | Bbls | | |
| | API _{B_SET} | 35.1 | °API | 35.1 | °API | 35.1 | °API | | |
| | ρ _{B_SET} | 848.407 | kg/m ³ | 848.402 | kg/m ³ | 848.407 | kg/m ³ | | |
| | T _{FP_SET} | 73.080 | °F | 70.600 | °F | 73.110 | °F | | |
| | P _{FP_SET} | 175.7 | psig | 185.7 | psig | 175.1 | psig | | |
| | Q _{MM_SET} | 701.040 | BPH | 524.142 | BPH | 882.128 | BPH | | |
| | ΔMMF _{SET} | (0.001) | % | 0.000 | % | 0.002 | % | | |
| CPV_{SET} Stability Parameters | Δρ _{B_SET} | 0.075 | kg/m ³ | (0.073) | kg/m ³ | 0.008 | kg/m ³ | | |
| | ΔT _{P_SET} | 0.010 | °F | 0.050 | °F | 0.050 | °F | | |
| | ΔP _{P_SET} | 0.3 | psig | 1.1 | psig | 0.4 | psig | | |
| | ΔQ _{MM_SET} | 0.0 | % | 0.0 | % | 0.0 | % | | |
| | ΔQ _{between SETS} | NA | % | (25.2) | % | 40.6 | % | | |
| | (r) CPV _{RUN} | 0.006 | % | 0.007 | % | 0.001 | % | | |
| | (R) CPV _{SET} | NA | % | 0.003 | % | 0.000 | % | | |

Example B.2 - Calibration Report Summary - 1 of 2

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| Washington, D.C., USA | | | | | | |
|---|--------------|------------|---|----------|------------------------------|----------|
| BPV Determination using a Master Meter - Standard Method | | | | | | |
| General Data <div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> API Midstream Headquarters Washington D.C. USA Crude Crude 60.0 0.0 14-Feb-2024 14-Feb-2024 </div> <div style="width: 45%;"> Operator Station Name City, Town State, Province Country Fluid, Batch No. Ch 11.1 T_B P_B Start Calibration Stop Calibration </div> </div> | | | Field Prover <div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> Manufacturer Prover Design Flow Design Wall Design Detector Displacer Wall Material Rod Material GL_P GL_D E_P ID_P WT_P Serial No. Switches </div> <div style="width: 45%;"> API Displacement Unidirectional Single External Captive Displacer 316SS 316SS 0.000 008 90 0.000 008 90 028 000 000 17.400 0 1.825 0 Uni-USC-004 9204 to 9234 </div> </div> | | | |
| <div style="background-color: black; color: white; padding: 5px;"> API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, $r \leq 0.02\%$, for 3 consecutive Calibration Sets Crude Oil - Tables 5A/6A </div> | | | <div style="display: flex; justify-content: space-between;"> <div style="width: 45%;"> BPV_{NEW} 0.590 121 0 Bbls BPV_{OLD} 0.590 118 0 Bbls ΔBPV 0.000 003 0 Bbls ΔBPV 0.000 5 % BPV_{NEW} Bigger / (Smaller) </div> <div style="width: 45%;"> Average CPV_{SET} 0.590 120 829 Bbls BPV₆₀ 5,725.352 3 in³ at 60.0 °F and 0.0 psig BPV₁₅ 93,819.209 mL at 15.0 °C and 0.0 kPag BPV₂₀ 93,841.756 mL at 20.0 °C and 0.0 kPag </div> </div> | | | |
| Base Prover Volume (BPV _{NEW}) | | | | | | |
| BPV ₆₀ | | | BPV ₁₅ | | BPV ₂₀ | |
| Barrels | U.S. Gallons | Cubic Feet | Cubic Meters | Liters | Cubic Meters | Liters |
| - | - | - | - | - | - | - |
| - | - | - | - | - | - | - |
| - | - | - | - | - | - | - |
| - | 24.785 1 | - | - | 93.819 2 | - | 93.841 8 |
| - | - | 3.313 28 | - | - | - | - |
| 0.590 121 | - | - | - | - | - | - |
| - | - | - | 0.093 819 2 | - | 0.093 841 8 | - |
| Note: The BPV _{NEW} values (BPV ₆₀ , BPV ₁₅ , BPV ₂₀) shown are reported to 6 significant digits (10 ppm, or, 0.001%). | | | | | | |
| Signature | | | Date | | Company | |
| | | | | | API Midstream Representative | |
| | | | | | | |
| | | | | | | |
| | | | | | | |

Example B.2 - Calibration Report Summary - 2 of 2

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| Washington, D.C., USA | | | | | | | | | |
|--|---------------------------------------|-----------------------|---------------------------------|-------------------------------|-----------------------------|---------------------------|----------------------------|---|-------|
| BPV Determination using Master Meter - Calibration Set I | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start | Stop | |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | Start I | Stop I | |
| Fluid or Batch | Crude | | Flow Design | Unidirectional | | Time | 14-Feb-24 | 14-Feb-24 | |
| Ch 11.1 | Crude | | Wall Design | Single | | Totalizer | 8:21:18 AM | 11:21:18 AM | |
| T _B | 60.0 | °F | Detector | External | | Fluid, Batch No. | 2,342,501.020 | 2,343,601.020 | Bbl |
| P _B | 0.0 | psig | Displacer | Captive Displacer | | API ₆₀ | Crude | Crude | |
| Master Meter | | | Wall Material | 316SS | | ρ ₆₀ | 35.1 | 35.2 | °API |
| Flowmeter ID | 400 | | Rod Material | Invar | | API ₁₅ | 848.597 | 848.217 | kg/m3 |
| Manufacturer | API | | GL _P | 0.000 008 90 | per °F | ρ ₁₅ | 35.0 | 35.1 | °API |
| Model | Turbine | | GL _D | 0.000 008 90 | per °F | ρ ₁₅ | 848.999 | 848.619 | kg/m3 |
| Nominal Size | 3 | | E _P | 028 000 000 | per psig | API ₂₀ | 35.6 | 35.7 | °API |
| Type | PD | | ID _P | 17.400 0 | inch | ρ ₂₀ | 845.377 | 844.995 | kg/m3 |
| Proving Result | MMF | | WT _P | 1.825 0 | inch | Flowrate, Q _{av} | 354.990 | 365.438 | BPH |
| T _F Comp | No | | Serial No. | Uni-USC-004 | | T _{MP_AVG} | 73.090 | 70.093 | °F |
| P _F Comp | No | | Switches | 9204 to 9234 | | P _{MP_AVG} | 170.6 | 175.4 | psig |
| NKF | 696.700 0 | | | | | Trips per Run | 1 | 1 | |
| Cartridge No. | API-0011 | | | | | Roundtrips | Runs 1-3 | Runs 1-3 | |
| Density Method | | | Calibration Set Criteria | | | Repeatability (r) | 0.004 | 0.002 | % |
| ρ _{obs} Method | Spot Sample | | ΔMMF _{SET} | ≤ 0.02 | % | Allowable (r) | 0.007 | 0.007 | % |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 | % | (r) Pass/Fail | Pass | Pass | |
| DMF | 0.000 0 | | (r) CPV _{RUN} | ≤ 0.02 | % | MMF | 0.999 997 8 | 0.999 986 5 | |
| HYC Factor | No | | | | | ΔMMF | NA | (0.001) | % |
| API Chapter 12.4.2 | | | Spot Sample | | | Allowable ± ΔMMF | NA | 0.020 | % |
| USC_60 Measurement Units | | | ρ _{60_START} | 848.597 000 000 000 | kg/m ³ | ΔMMF Pass/Fail | NA | Pass | |
| Sampling Method - Spot | | | ρ _{60_STOP} | 848.216 823 342 456 | kg/m ³ | | | | |
| BPV - Standard Method | | | ρ _{60_SET} | 848.406 911 671 228 | kg/m ³ | | | | |
| Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs | | | MMF _{SET} | 0.999 992 2 | | | | | |
| Crude Oil - Tables 5A/6A | | | | | | Prior vs Current | | | |
| | | | | | | ΔQ _{av} | 0.02 | % | |
| | | | | | | ΔT _P | 0.400 | °C | |
| Roundtrip Measurements | | | | | | | | | |
| | ρ _{obs} kg/m ³ | T _{dm} °F | P _{dm} psig | T _{P_INLET} °F | T _{P_OUTLET} °F | T _M °F | T _D °F | Base Density ρ _B kg/m ³ | Run |
| | | | | 73.480 | 73.360 | 73.210 | 75.020 | 848.407 | 1 |
| | | | | 73.510 | 73.430 | 73.280 | 75.140 | 848.407 | 2 |
| | | | | 73.470 | 73.320 | 73.230 | 75.120 | 848.407 | 3 |
| | | | | 73.070 | 73.070 | 73.400 | 75.020 | 848.407 | 4 |
| | | | | 73.060 | 73.090 | 73.500 | 75.140 | 848.407 | 5 |
| | | | | 73.060 | 73.100 | 73.420 | 75.120 | 848.407 | 6 |
| | | | | 73.280 | 73.230 | 73.340 | 75.090 | 848.407 | Avg |
| Ch 11.1 Iteration Results | | | | | | | | | |
| | N or N _i Pulses | Q _M BPH | P _{P_INLET} psig | P _{P_OUTLET} psig | P _M psig | T _{P_RUN} °F | P _{P_RUN} psig | | Run |
| | Crude Oil, JP-4 | 411.103 | 701.110 | 176.1 | 173.8 | 185.4 | 73.420 0 | 174.95 | 1 |
| | Crude Oil, JP-4 | 411.174 | 700.982 | 176.7 | 174.0 | 185.9 | 73.470 0 | 175.35 | 2 |
| | Crude Oil, JP-4 | 411.383 | 700.995 | 176.2 | 174.0 | 186.4 | 73.395 0 | 175.10 | 3 |
| | Crude Oil, JP-4 | 411.357 | 701.014 | 176.8 | 174.3 | 186.4 | 73.070 0 | 175.55 | 4 |
| | Crude Oil, JP-4 | 411.353 | 701.002 | 176.9 | 174.6 | 186.7 | 73.075 0 | 175.75 | 5 |
| | Crude Oil, JP-4 | 411.358 | 701.103 | 176.9 | 174.8 | 185.5 | 73.080 0 | 175.85 | 6 |
| | | 411.288 0 | 701.034 | 176.6 | 174.3 | 186.1 | 73.250 0 | 175.40 | Avg |

Example B.2 - Calibration Set I - 1 of 2

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|---|--|------------------------------|---|--------------------------|------------------------|---|----------------------------|----------|--|--------------------------------|--|---------------------------|-----------------------------|--------------------------|------------------------------|----------------------------|----------------------------|-----------------|---------------|---------------|---------------|------------------|---------------|---------------|---|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|-------|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|-----|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|------|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|---|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|---|-----------|---------------|---------------|---------------|---------------|---------------|---------------|-----|
| BPV Determination using Master Meter - Calibration Set I | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Crude Oil - Tables 5A/6A | | | ΔMMF_{SET} Pass $(r) ICPV_{RUN}$ Pass $(r) CPV_{RUN}$ Pass | | | Report Summary <table border="1" style="margin: auto; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;"><i>Prior</i></th> <th style="text-align: center;"><i>Current</i></th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start</td> <td style="text-align: center;">Stop</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">14-Feb-24</td> <td style="text-align: center;">14-Feb-24</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">08:21:18</td> <td style="text-align: center;">11:21:18</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">Crude</td> <td style="text-align: center;">Crude</td> </tr> </tbody> </table> | | | | | <i>Prior</i> | <i>Current</i> | Report No. | Start | Stop | Date | 14-Feb-24 | 14-Feb-24 | Time | 08:21:18 | 11:21:18 | Fluid, Batch No. | Crude | Crude | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | <i>Prior</i> | <i>Current</i> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 08:21:18 | 11:21:18 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Crude | Crude | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr style="background-color: #f4a460;"> <th>N or N_i Pulses</th> <th>NKF P / Bbl</th> <th>IV_M</th> <th>CTL_M</th> <th>CPL_M</th> <th>CTPL_M</th> <th>GSV_M Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>411.103</td><td>696.700 0</td><td>0.590 071 8</td><td>0.993 726 846</td><td>1.000 973 393</td><td>0.994 694 133</td><td>0.586 936 379</td><td>1</td></tr> <tr><td>411.174</td><td>696.700 0</td><td>0.590 173 7</td><td>0.993 693 543</td><td>1.000 976 251</td><td>0.994 663 638</td><td>0.587 019 740</td><td>2</td></tr> <tr><td>411.383</td><td>696.700 0</td><td>0.590 473 7</td><td>0.993 717 331</td><td>1.000 978 714</td><td>0.994 689 896</td><td>0.587 333 642</td><td>3</td></tr> <tr><td>411.357</td><td>696.700 0</td><td>0.590 436 3</td><td>0.993 636 452</td><td>1.000 979 275</td><td>0.994 609 495</td><td>0.587 248 970</td><td>4</td></tr> <tr><td>411.353</td><td>696.700 0</td><td>0.590 430 6</td><td>0.993 588 874</td><td>1.000 981 183</td><td>0.994 563 767</td><td>0.587 216 301</td><td>5</td></tr> <tr><td>411.358</td><td>696.700 0</td><td>0.590 437 8</td><td>0.993 626 936</td><td>1.000 974 608</td><td>0.994 595 333</td><td>0.587 242 100</td><td>6</td></tr> <tr style="background-color: #f4a460;"><td>411.288 0</td><td>696.700 0</td><td>0.590 337 3</td><td>0.993 664 997</td><td>1.000 977 237</td><td>0.994 636 044</td><td>0.587 166 189</td><td>Avg</td></tr> </tbody> </table> | | | | | | | | | | N or N _i Pulses | NKF P / Bbl | IV _M | CTL _M | CPL _M | CTPL _M | GSV _M Bbls | Run | 411.103 | 696.700 0 | 0.590 071 8 | 0.993 726 846 | 1.000 973 393 | 0.994 694 133 | 0.586 936 379 | 1 | 411.174 | 696.700 0 | 0.590 173 7 | 0.993 693 543 | 1.000 976 251 | 0.994 663 638 | 0.587 019 740 | 2 | 411.383 | 696.700 0 | 0.590 473 7 | 0.993 717 331 | 1.000 978 714 | 0.994 689 896 | 0.587 333 642 | 3 | 411.357 | 696.700 0 | 0.590 436 3 | 0.993 636 452 | 1.000 979 275 | 0.994 609 495 | 0.587 248 970 | 4 | 411.353 | 696.700 0 | 0.590 430 6 | 0.993 588 874 | 1.000 981 183 | 0.994 563 767 | 0.587 216 301 | 5 | 411.358 | 696.700 0 | 0.590 437 8 | 0.993 626 936 | 1.000 974 608 | 0.994 595 333 | 0.587 242 100 | 6 | 411.288 0 | 696.700 0 | 0.590 337 3 | 0.993 664 997 | 1.000 977 237 | 0.994 636 044 | 0.587 166 189 | Avg |
| N or N _i Pulses | NKF P / Bbl | IV _M | CTL _M | CPL _M | CTPL _M | GSV _M Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.103 | 696.700 0 | 0.590 071 8 | 0.993 726 846 | 1.000 973 393 | 0.994 694 133 | 0.586 936 379 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.174 | 696.700 0 | 0.590 173 7 | 0.993 693 543 | 1.000 976 251 | 0.994 663 638 | 0.587 019 740 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.383 | 696.700 0 | 0.590 473 7 | 0.993 717 331 | 1.000 978 714 | 0.994 689 896 | 0.587 333 642 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.357 | 696.700 0 | 0.590 436 3 | 0.993 636 452 | 1.000 979 275 | 0.994 609 495 | 0.587 248 970 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.353 | 696.700 0 | 0.590 430 6 | 0.993 588 874 | 1.000 981 183 | 0.994 563 767 | 0.587 216 301 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.358 | 696.700 0 | 0.590 437 8 | 0.993 626 936 | 1.000 974 608 | 0.994 595 333 | 0.587 242 100 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.288 0 | 696.700 0 | 0.590 337 3 | 0.993 664 997 | 1.000 977 237 | 0.994 636 044 | 0.587 166 189 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr style="background-color: #f4a460;"> <th>Iteration Results</th> <th>CTS_p</th> <th>CPS_p</th> <th>CTL_p</th> <th>CPL_p</th> <th>CTPL_p</th> <th>CPV_{run} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>Crude Oil, JP-4</td><td>1.000 372 600</td><td>1.000 059 572</td><td>0.993 626 936</td><td>1.000 919 128</td><td>0.994 540 206</td><td>0.589 903 570</td><td>1</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 374 559</td><td>1.000 059 708</td><td>0.993 603 147</td><td>1.000 921 386</td><td>0.994 518 640</td><td>0.589 998 911</td><td>2</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 373 045</td><td>1.000 059 623</td><td>0.993 638 831</td><td>1.000 919 839</td><td>0.994 552 818</td><td>0.590 295 063</td><td>3</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 366 369</td><td>1.000 059 776</td><td>0.993 793 449</td><td>1.000 921 196</td><td>0.994 708 928</td><td>0.590 121 184</td><td>4</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 367 526</td><td>1.000 059 844</td><td>0.993 791 071</td><td>1.000 922 262</td><td>0.994 707 606</td><td>0.590 088 417</td><td>5</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 367 437</td><td>1.000 059 878</td><td>0.993 788 692</td><td>1.000 922 803</td><td>0.994 705 763</td><td>0.590 115 468</td><td>6</td></tr> <tr style="background-color: #f4a460;"><td></td><td>1.000 370 256</td><td>1.000 059 734</td><td>0.993 707 021</td><td>1.000 921 102</td><td>0.994 622 327</td><td>0.590 087 102</td><td>Avg</td></tr> </tbody> </table> | | | | | | | | | | Iteration Results | CTS _p | CPS _p | CTL _p | CPL _p | CTPL _p | CPV _{run} Bbls | Run | Crude Oil, JP-4 | 1.000 372 600 | 1.000 059 572 | 0.993 626 936 | 1.000 919 128 | 0.994 540 206 | 0.589 903 570 | 1 | Crude Oil, JP-4 | 1.000 374 559 | 1.000 059 708 | 0.993 603 147 | 1.000 921 386 | 0.994 518 640 | 0.589 998 911 | 2 | Crude Oil, JP-4 | 1.000 373 045 | 1.000 059 623 | 0.993 638 831 | 1.000 919 839 | 0.994 552 818 | 0.590 295 063 | 3 | Crude Oil, JP-4 | 1.000 366 369 | 1.000 059 776 | 0.993 793 449 | 1.000 921 196 | 0.994 708 928 | 0.590 121 184 | 4 | Crude Oil, JP-4 | 1.000 367 526 | 1.000 059 844 | 0.993 791 071 | 1.000 922 262 | 0.994 707 606 | 0.590 088 417 | 5 | Crude Oil, JP-4 | 1.000 367 437 | 1.000 059 878 | 0.993 788 692 | 1.000 922 803 | 0.994 705 763 | 0.590 115 468 | 6 | | 1.000 370 256 | 1.000 059 734 | 0.993 707 021 | 1.000 921 102 | 0.994 622 327 | 0.590 087 102 | Avg |
| Iteration Results | CTS _p | CPS _p | CTL _p | CPL _p | CTPL _p | CPV _{run} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 372 600 | 1.000 059 572 | 0.993 626 936 | 1.000 919 128 | 0.994 540 206 | 0.589 903 570 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 374 559 | 1.000 059 708 | 0.993 603 147 | 1.000 921 386 | 0.994 518 640 | 0.589 998 911 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 373 045 | 1.000 059 623 | 0.993 638 831 | 1.000 919 839 | 0.994 552 818 | 0.590 295 063 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 366 369 | 1.000 059 776 | 0.993 793 449 | 1.000 921 196 | 0.994 708 928 | 0.590 121 184 | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 367 526 | 1.000 059 844 | 0.993 791 071 | 1.000 922 262 | 0.994 707 606 | 0.590 088 417 | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 367 437 | 1.000 059 878 | 0.993 788 692 | 1.000 922 803 | 0.994 705 763 | 0.590 115 468 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 370 256 | 1.000 059 734 | 0.993 707 021 | 1.000 921 102 | 0.994 622 327 | 0.590 087 102 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr style="background-color: #f4a460;"> <th>1 means ΔCPV Passed</th> <th>ΔP_{B_SET} kg/m³</th> <th>ΔT_{P_SET} °F</th> <th>ΔP_{P_SET} psig</th> <th>ΔQ_{M_SET} %</th> <th>r% ICPV_{run}</th> <th>CPV_{set}</th> <th>CPV_{set} Bbls</th> <th></th> </tr> </thead> <tbody> <tr><td></td><td>0.000</td><td>0.075</td><td>0.40</td><td>0.0</td><td>0.066</td><td>-</td><td>0.590 065 848</td><td>Runs 1-3</td></tr> <tr><td></td><td>0.000</td><td>0.400</td><td>0.45</td><td>0.0</td><td>0.050</td><td>-</td><td>0.590 138 386</td><td>Runs 2-4</td></tr> <tr><td></td><td>0.000</td><td>0.325</td><td>0.65</td><td>0.0</td><td>0.035</td><td>-</td><td>0.590 168 221</td><td>Runs 3-5</td></tr> <tr style="background-color: #f4a460;"><td>1</td><td>0.000</td><td>0.010</td><td>0.30</td><td>0.0</td><td>0.006</td><td>Pass</td><td>0.590 108 356</td><td>Runs 4-6</td></tr> </tbody> </table> | | | | | | | | | | 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{M_SET} % | r% ICPV _{run} | CPV _{set} | CPV _{set} Bbls | | | 0.000 | 0.075 | 0.40 | 0.0 | 0.066 | - | 0.590 065 848 | Runs 1-3 | | 0.000 | 0.400 | 0.45 | 0.0 | 0.050 | - | 0.590 138 386 | Runs 2-4 | | 0.000 | 0.325 | 0.65 | 0.0 | 0.035 | - | 0.590 168 221 | Runs 3-5 | 1 | 0.000 | 0.010 | 0.30 | 0.0 | 0.006 | Pass | 0.590 108 356 | Runs 4-6 | | | | | | | | | | | | | | | | | | | |
| 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{M_SET} % | r% ICPV _{run} | CPV _{set} | CPV _{set} Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.000 | 0.075 | 0.40 | 0.0 | 0.066 | - | 0.590 065 848 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.000 | 0.400 | 0.45 | 0.0 | 0.050 | - | 0.590 138 386 | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 0.000 | 0.325 | 0.65 | 0.0 | 0.035 | - | 0.590 168 221 | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1 | 0.000 | 0.010 | 0.30 | 0.0 | 0.006 | Pass | 0.590 108 356 | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 40%;">Signature</th> <th style="width: 20%;">Date</th> <th style="width: 40%;">Company</th> </tr> </thead> <tbody> <tr> <td style="height: 40px;"></td> <td></td> <td style="text-align: center;">API Midstream Representative</td> </tr> <tr><td style="height: 40px;"></td><td></td><td></td></tr> <tr><td style="height: 40px;"></td><td></td><td></td></tr> <tr><td style="height: 40px;"></td><td></td><td></td></tr> </tbody> </table> | | | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example B.2 - Calibration Set I - 2 of 2

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| Washington, D.C., USA | | | | | | | | | |
|--|---------------------------------------|------------------------|---------------------------------|---------------------------------------|------------------------------|--|-------------------------|---|---------------|
| BPV Determination using Master Meter - Calibration Set II | | | | | | | | | |
| General Data | | | Field Prover | | | Report Summary | | | |
| Operator | API Midstream | | Prover Manufacturer | API | | Report No. | Start 2 | | Stop 2 |
| Station Name | Headquarters | | Prover Design | Displacement | | Date | 14-Feb-24 | | 14-Feb-24 |
| Fluid or Batch | Crude | | Flow Design | Unidirectional | | Time | 10:53:11 AM | | 12:40:18 PM |
| Ch 11.1 | Crude | | Wall Design | Single | | Totalizer | 2,342,521.020 | | 2,343,841.020 |
| T _B | 60.0 °F | | Detector | External | | Fluid, Batch No. | Crude | | Crude |
| P _B | 0.0 psig | | Displacer | Captive Displacer | | API ₆₀ | 35.2 | | 35.1 |
| Master Meter | | | Wall Material | 316SS | | ρ ₆₀ | 848.217 | | 848.587 |
| Flowmeter ID | 400 | | Rod Material | Invar | | API ₁₅ | 35.1 | | 35.0 |
| Manufacturer | API | | GL _P | 0.000 008 90 per °F | | ρ ₁₅ | 848.619 | | 848.989 |
| Model | Turbine | | GL _D | 0.000 008 90 per °F | | API ₂₀ | 35.7 | | 35.6 |
| Nominal Size | 3 inch | | E _P | 028 000 000 per psig | | ρ ₂₀ | 844.995 | | 845.367 |
| Type | PD | | ID _P | 17.400 0 inch | | Flowrate, Q _{av} | 524.145 | | 524.785 |
| Proving Result | MMF | | WT _P | 1.825 0 inch | | T _{MP_AVG} | 70.710 | | 70.730 |
| T _F Comp | No | | Serial No. | Uni-USC-004 | | P _{MP_AVG} | 189.1 | | 189.5 |
| P _F Comp | No | | Switches | 9204 to 9234 | | Trips per Run | 1 | | 1 |
| NKF | 696.700 0 P / Bbl | | | | | Roundtrips | Runs 1-5 | | Runs 1-5 |
| Cartridge No. | API-0011 | | | | | Repeatability (r) | 0.011 | | 0.008 |
| Density Method | | | Calibration Set Criteria | | | Allowable (r) | 0.020 | | 0.020 |
| ρ _{obs} Method | Spot Sample | | ΔMMF _{SET} | ≤ 0.02 % | | (r) Pass/Fail | Pass | | Pass |
| ρ _{obs} Device | Online Density | | (r) ICPV _{RUN} | ≤ 0.02 % | | MMF | 1.000 055 2 | | 1.000 058 6 |
| DMF | 0.000 0 | | (r) CPV _{RUN} | ≤ 0.02 % | | ΔMMF | NA | | 0.000 |
| HYC Factor | No | | Spot Sample | | | Allowable ± ΔMMF | NA | | 0.020 |
| API Chapter 12.4.2 | | | ρ _{60_START} | 848.216 823 342 456 kg/m ³ | | ΔMMF Pass/Fail | NA | | Pass |
| USC_60 Measurement Units | | | ρ _{60_STOP} | 848.586 998 731 528 kg/m ³ | | | | | |
| Sampling Method - Spot | | | ρ _{60_SET} | 848.401 911 036 992 kg/m ³ | | | | | |
| BPV - Standard Method | | | MMF _{SET} | 1.000 056 9 | | | | | |
| Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs | | | | | | Prior vs Current | | | |
| Crude Oil - Tables 5A/6A | | | | | | ΔQ _{av} | 0.1 % | | |
| | | | | | | ΔT _P | 0.120 °C | | |
| Roundtrip Measurements | | | | | | | | | |
| | ρ _{obs} kg/m ³ | T _{dm} °F | P _{dm} psig | T _{FP_INLET} °F | T _{FP_OUTLET} °F | T _{MM} °F | T _{FD} °F | Base Density ρ _B kg/m ³ | Run |
| | | | | 70.690 | 70.510 | 70.520 | 75.120 | 848.402 | 1 |
| | | | | 70.700 | 70.540 | 70.560 | 75.020 | 848.402 | 2 |
| | | | | 70.690 | 70.450 | 70.630 | 75.140 | 848.402 | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| | | | | 70.690 | 70.500 | 70.570 | 75.090 | 848.402 | Avg |
| Roundtrip Measurements | | | | | | | | | |
| Ch 11.1 Iteration Results | N or N _i Pulses | Q _{MM} BPH | P _{FP_INLET} psig | P _{FP_OUTLET} psig | P _{MM} psig | T _{FP} and P _{FP} Values | | | Run |
| | | | | | | T _{FP} °F | P _{FP} psig | | |
| | Crude Oil, JP-4 | 411.277 | 524.145 | 186.2 | 185.5 | 183.9 | 70.600 0 | 185.85 | 1 |
| | Crude Oil, JP-4 | 411.273 | 524.139 | 186.8 | 185.4 | 184.2 | 70.620 0 | 186.10 | 2 |
| | Crude Oil, JP-4 | 411.278 | 524.141 | 186.2 | 183.9 | 182.3 | 70.570 0 | 185.05 | 3 |
| | | | | | | | | | 4 |
| | | | | | | | | | 5 |
| | | | | | | | | | 6 |
| | 411.276 0 | 524.142 | 186.4 | 184.9 | 183.5 | 70.600 0 | 185.70 | | Avg |

Example B.2 - Calibration Set II - 1 of 2

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|--|--|------------------------------|---|---------------------------|------------------------|----------------------------|---|---------------|----------|--------------------------------|--|---------------------------|-----------------------------|---------------------------|------------------------------|----------------------------|----------------------------|-----------------|---------------|---------------|---------------|------------------|---------------|---------------|-------|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|----|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|----|----|----|----|---|---|---|----------|----------|----|----|----|----|----|---|---|---|----------|--|--|--|--|--|--|---|-----------|---------------|---------------|---------------|---------------|---------------|---------------|-----|
| BPV Determination using Master Meter - Calibration Set II | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Crude Oil - Tables 5A/6A | | | <div style="display: flex; justify-content: space-between;"> <div> ΔMMF_{SET} Pass $(r) ICPV_{SET}$ Pass $(r) CPV_{SET}$ Pass </div> <div style="border-left: 1px solid black; padding-left: 5px;">-</div> </div> | | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="text-align: center;">Prior</th> <th style="text-align: center;">Current</th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td style="text-align: center;">Start</td> <td style="text-align: center;">Stop</td> </tr> <tr> <td>Date</td> <td style="text-align: center;">Start 2</td> <td style="text-align: center;">Stop 2</td> </tr> <tr> <td>Time</td> <td style="text-align: center;">00:00:00</td> <td style="text-align: center;">00:00:00</td> </tr> <tr> <td>Fluid, Batch No.</td> <td style="text-align: center;">2342521.02</td> <td style="text-align: center;">2343841.02</td> </tr> </tbody> </table> | | | | Prior | Current | Report No. | Start | Stop | Date | Start 2 | Stop 2 | Time | 00:00:00 | 00:00:00 | Fluid, Batch No. | 2342521.02 | 2343841.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Prior | Current | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | Start 2 | Stop 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 00:00:00 | 00:00:00 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | 2342521.02 | 2343841.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>N or N_i Pulses</th> <th>NKF P / Bbl</th> <th>IV_{MM}</th> <th>CTL_{MM}</th> <th>CPL_{MM}</th> <th>CTPL_{MM}</th> <th>GSV_{MM} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>411.277</td><td>696.700 0</td><td>0.590 321 5</td><td>0.995 006 077</td><td>1.000 956 812</td><td>0.995 958 111</td><td>0.587 968 940</td><td>1</td></tr> <tr><td>411.273</td><td>696.700 0</td><td>0.590 315 8</td><td>0.994 987 061</td><td>1.000 958 504</td><td>0.995 940 760</td><td>0.587 953 019</td><td>2</td></tr> <tr><td>411.278</td><td>696.700 0</td><td>0.590 323 0</td><td>0.994 953 782</td><td>1.000 948 831</td><td>0.995 897 825</td><td>0.587 934 844</td><td>3</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>4</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>6</td></tr> <tr> <td>411.276 0</td> <td>696.700 0</td> <td>0.590 320 1</td> <td>0.994 982 307</td> <td>1.000 954 716</td> <td>0.995 932 232</td> <td>0.587 952 268</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | | | N or N _i Pulses | NKF P / Bbl | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} Bbls | Run | 411.277 | 696.700 0 | 0.590 321 5 | 0.995 006 077 | 1.000 956 812 | 0.995 958 111 | 0.587 968 940 | 1 | 411.273 | 696.700 0 | 0.590 315 8 | 0.994 987 061 | 1.000 958 504 | 0.995 940 760 | 0.587 953 019 | 2 | 411.278 | 696.700 0 | 0.590 323 0 | 0.994 953 782 | 1.000 948 831 | 0.995 897 825 | 0.587 934 844 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | 411.276 0 | 696.700 0 | 0.590 320 1 | 0.994 982 307 | 1.000 954 716 | 0.995 932 232 | 0.587 952 268 | Avg |
| N or N _i Pulses | NKF P / Bbl | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.277 | 696.700 0 | 0.590 321 5 | 0.995 006 077 | 1.000 956 812 | 0.995 958 111 | 0.587 968 940 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.273 | 696.700 0 | 0.590 315 8 | 0.994 987 061 | 1.000 958 504 | 0.995 940 760 | 0.587 953 019 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.278 | 696.700 0 | 0.590 323 0 | 0.994 953 782 | 1.000 948 831 | 0.995 897 825 | 0.587 934 844 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.276 0 | 696.700 0 | 0.590 320 1 | 0.994 982 307 | 1.000 954 716 | 0.995 932 232 | 0.587 952 268 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>Iteration Results</th> <th>CTS_{FP}</th> <th>CPS_{FP}</th> <th>CTL_{FP}</th> <th>CPL_{FP}</th> <th>CTPL_{FP}</th> <th>CPV_{run} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>Crude Oil, JP-4</td><td>1.000 323 282</td><td>1.000 063 284</td><td>0.994 968 045</td><td>1.000 967 228</td><td>0.995 930 406</td><td>0.590 143 371</td><td>1</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 322 748</td><td>1.000 063 369</td><td>0.994 958 536</td><td>1.000 968 596</td><td>0.995 922 249</td><td>0.590 132 489</td><td>2</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 322 926</td><td>1.000 063 011</td><td>0.994 982 307</td><td>1.000 962 964</td><td>0.995 940 439</td><td>0.590 103 575</td><td>3</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>4</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>6</td></tr> <tr> <td></td> <td>1.000 322 985</td> <td>1.000 063 221</td> <td>0.994 969 629</td> <td>1.000 966 263</td> <td>0.995 931 031</td> <td>0.590 126 478</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | | | Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} Bbls | Run | Crude Oil, JP-4 | 1.000 323 282 | 1.000 063 284 | 0.994 968 045 | 1.000 967 228 | 0.995 930 406 | 0.590 143 371 | 1 | Crude Oil, JP-4 | 1.000 322 748 | 1.000 063 369 | 0.994 958 536 | 1.000 968 596 | 0.995 922 249 | 0.590 132 489 | 2 | Crude Oil, JP-4 | 1.000 322 926 | 1.000 063 011 | 0.994 982 307 | 1.000 962 964 | 0.995 940 439 | 0.590 103 575 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | | 1.000 322 985 | 1.000 063 221 | 0.994 969 629 | 1.000 966 263 | 0.995 931 031 | 0.590 126 478 | Avg |
| Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 323 282 | 1.000 063 284 | 0.994 968 045 | 1.000 967 228 | 0.995 930 406 | 0.590 143 371 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 322 748 | 1.000 063 369 | 0.994 958 536 | 1.000 968 596 | 0.995 922 249 | 0.590 132 489 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 322 926 | 1.000 063 011 | 0.994 982 307 | 1.000 962 964 | 0.995 940 439 | 0.590 103 575 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 322 985 | 1.000 063 221 | 0.994 969 629 | 1.000 966 263 | 0.995 931 031 | 0.590 126 478 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th>1 means ΔCPV Passed</th> <th>ΔP_{B_SET} kg/m³</th> <th>ΔT_{P_SET} °F</th> <th>ΔP_{P_SET} psig</th> <th>ΔQ_{MM_SET} %</th> <th>r% ICPV_{run}</th> <th>CPV_{set}</th> <th>CPV_{set} Bbls</th> <th></th> </tr> </thead> <tbody> <tr> <td>Runs 1-3</td> <td>1</td> <td>0.000</td> <td>0.050</td> <td>1.05</td> <td>0.0</td> <td>0.007</td> <td>Pass</td> <td>0.590 126 478</td> <td>Runs 1-3</td> </tr> <tr> <td>Runs 2-4</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>-</td> <td>Runs 2-4</td> </tr> <tr> <td>Runs 3-5</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>-</td> <td>Runs 3-5</td> </tr> <tr> <td>Runs 4-6</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>-</td> <td>Runs 4-6</td> </tr> </tbody> </table> | | | | | | | | | | 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{MM_SET} % | r% ICPV _{run} | CPV _{set} | CPV _{set} Bbls | | Runs 1-3 | 1 | 0.000 | 0.050 | 1.05 | 0.0 | 0.007 | Pass | 0.590 126 478 | Runs 1-3 | Runs 2-4 | NA | NA | NA | NA | NA | - | - | - | Runs 2-4 | Runs 3-5 | NA | NA | NA | NA | NA | - | - | - | Runs 3-5 | Runs 4-6 | NA | NA | NA | NA | NA | - | - | - | Runs 4-6 | | | | | | | | | | | | | | | |
| 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{MM_SET} % | r% ICPV _{run} | CPV _{set} | CPV _{set} Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 | 1 | 0.000 | 0.050 | 1.05 | 0.0 | 0.007 | Pass | 0.590 126 478 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 2-4 | NA | NA | NA | NA | NA | - | - | - | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 3-5 | NA | NA | NA | NA | NA | - | - | - | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 4-6 | NA | NA | NA | NA | NA | - | - | - | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 40%;">Signature</th> <th style="width: 20%;">Date</th> <th style="width: 40%;">Company</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td style="text-align: center;">API Midstream Representative</td> </tr> <tr><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td></tr> </tbody> </table> | | | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example B.2 - Calibration Set II - 2 of 2

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|---|-------------------------------|-------------------------|--|--------------------------------|-------------------------|---|-------------------------------------|---|--|--|-------|------|--|------------|---------|--------|--|------|-----------|-----------|--|------|------------|-------------|--|-----------|---------------|---------------|-----|------------------|-------|-------|--|-------------------|------|------|------|-----------------|---------|---------|-------------------|-------------------|------|------|------|-----------------|---------|---------|-------------------|-------------------|------|------|------|-----------------|---------|---------|-------------------|---------------------------|---------|---------|-----|---------------------|--------|--------|----|---------------------|-------|-------|------|---------------|---|---|--|------------|----------|----------|--|-------------------|-------|-------|---|---------------|-------|-------|---|---------------|------|------|--|-----|-------------|-------------|--|------|----|-------|---|------------------|----|-------|---|----------------|----|------|--|
| BPV Determination using Master Meter - Calibration Set III | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| General Data Operator: API Midstream Station Name: Headquarters Fluid or Batch: Crude Ch 11.1: Crude T _B : 60.0 °F P _B : 0.0 psig | | | Field Prover Prover Manufacturer: API Prover Design: Displacement Flow Design: Unidirectional Wall Design: Single Detector: External Displacer: Captive Displacer Wall Material: 316SS Rod Material: Invar G _{Lp} : 0.000 008 90 per °F G _{Ld} : 0.000 008 90 per °F E _p : 028 000 000 per psig ID _p : 17.400 0 inch WT _p : 1.825 0 inch Serial No.: Uni-USC-004 Switches: 9204 to 9234 | | | Report Summary <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th style="background-color: #d9ead3;">Start</th> <th style="background-color: #d9ead3;">Stop</th> <th></th> </tr> </thead> <tbody> <tr> <td>Report No.</td> <td>Start 3</td> <td>Stop 3</td> <td></td> </tr> <tr> <td>Date</td> <td>14-Feb-24</td> <td>14-Feb-24</td> <td></td> </tr> <tr> <td>Time</td> <td>8:21:18 AM</td> <td>11:21:18 AM</td> <td></td> </tr> <tr> <td>Totalizer</td> <td>2,342,501.020</td> <td>2,343,601.020</td> <td>Bbl</td> </tr> <tr> <td>Fluid, Batch No.</td> <td>Crude</td> <td>Crude</td> <td></td> </tr> <tr> <td>API₆₀</td> <td>35.1</td> <td>35.1</td> <td>°API</td> </tr> <tr> <td>ρ₆₀</td> <td>848.427</td> <td>848.387</td> <td>kg/m³</td> </tr> <tr> <td>API₁₅</td> <td>35.1</td> <td>35.1</td> <td>°API</td> </tr> <tr> <td>ρ₁₅</td> <td>848.829</td> <td>848.789</td> <td>kg/m³</td> </tr> <tr> <td>API₂₀</td> <td>35.6</td> <td>35.6</td> <td>°API</td> </tr> <tr> <td>ρ₂₀</td> <td>845.206</td> <td>845.166</td> <td>kg/m³</td> </tr> <tr> <td>Flowrate, Q_{av}</td> <td>882.146</td> <td>881.970</td> <td>BPH</td> </tr> <tr> <td>T_{MP_AVG}</td> <td>73.100</td> <td>73.240</td> <td>°F</td> </tr> <tr> <td>P_{MP_AVG}</td> <td>187.7</td> <td>188.3</td> <td>psig</td> </tr> <tr> <td>Trips per Run</td> <td>1</td> <td>1</td> <td></td> </tr> <tr> <td>Roundtrips</td> <td>Runs 1-5</td> <td>Runs 1-5</td> <td></td> </tr> <tr> <td>Repeatability (r)</td> <td>0.008</td> <td>0.014</td> <td>%</td> </tr> <tr> <td>Allowable (r)</td> <td>0.020</td> <td>0.020</td> <td>%</td> </tr> <tr> <td>(r) Pass/Fail</td> <td>Pass</td> <td>Pass</td> <td></td> </tr> <tr> <td>MMF</td> <td>0.999 845 2</td> <td>0.999 865 5</td> <td></td> </tr> <tr> <td>ΔMMF</td> <td>NA</td> <td>0.002</td> <td>%</td> </tr> <tr> <td>Allowable ± ΔMMF</td> <td>NA</td> <td>0.020</td> <td>%</td> </tr> <tr> <td>ΔMMF Pass/Fail</td> <td>NA</td> <td>Pass</td> <td></td> </tr> </tbody> </table> | | | | | Start | Stop | | Report No. | Start 3 | Stop 3 | | Date | 14-Feb-24 | 14-Feb-24 | | Time | 8:21:18 AM | 11:21:18 AM | | Totalizer | 2,342,501.020 | 2,343,601.020 | Bbl | Fluid, Batch No. | Crude | Crude | | API ₆₀ | 35.1 | 35.1 | °API | ρ ₆₀ | 848.427 | 848.387 | kg/m ³ | API ₁₅ | 35.1 | 35.1 | °API | ρ ₁₅ | 848.829 | 848.789 | kg/m ³ | API ₂₀ | 35.6 | 35.6 | °API | ρ ₂₀ | 845.206 | 845.166 | kg/m ³ | Flowrate, Q _{av} | 882.146 | 881.970 | BPH | T _{MP_AVG} | 73.100 | 73.240 | °F | P _{MP_AVG} | 187.7 | 188.3 | psig | Trips per Run | 1 | 1 | | Roundtrips | Runs 1-5 | Runs 1-5 | | Repeatability (r) | 0.008 | 0.014 | % | Allowable (r) | 0.020 | 0.020 | % | (r) Pass/Fail | Pass | Pass | | MMF | 0.999 845 2 | 0.999 865 5 | | ΔMMF | NA | 0.002 | % | Allowable ± ΔMMF | NA | 0.020 | % | ΔMMF Pass/Fail | NA | Pass | |
| | Start | Stop | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Report No. | Start 3 | Stop 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Date | 14-Feb-24 | 14-Feb-24 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Time | 8:21:18 AM | 11:21:18 AM | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Totalizer | 2,342,501.020 | 2,343,601.020 | Bbl | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Fluid, Batch No. | Crude | Crude | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₆₀ | 35.1 | 35.1 | °API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ ₆₀ | 848.427 | 848.387 | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₁₅ | 35.1 | 35.1 | °API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ ₁₅ | 848.829 | 848.789 | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API ₂₀ | 35.6 | 35.6 | °API | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ ₂₀ | 845.206 | 845.166 | kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Flowrate, Q _{av} | 882.146 | 881.970 | BPH | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| T _{MP_AVG} | 73.100 | 73.240 | °F | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| P _{MP_AVG} | 187.7 | 188.3 | psig | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Trips per Run | 1 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrips | Runs 1-5 | Runs 1-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Repeatability (r) | 0.008 | 0.014 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Allowable (r) | 0.020 | 0.020 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (r) Pass/Fail | Pass | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| MMF | 0.999 845 2 | 0.999 865 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF | NA | 0.002 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Allowable ± ΔMMF | NA | 0.020 | % | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ΔMMF Pass/Fail | NA | Pass | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Master Meter Flowmeter ID: 400 Manufacturer: API Model: Turbine Nominal Size: 3 inch Type: PD Proving Result: MMF T _F Comp: No P _F Comp: No NKF: 696.700 0 P / Bbl Cartridge No.: API-0011 | | | Density Method ρ _{obs} Method: Spot Sample ρ _{obs} Device: Online Density DMF: 0.000 0 HYC Factor: No | | | Calibration Set Criteria ΔMMF _{SET} ≤ 0.02 % (r) ICPV _{RUN} ≤ 0.02 % (r) CPV _{RUN} ≤ 0.02 % Spot Sample ρ _{60_START} : 848.426 922 906 387 kg/m ³ ρ _{60_STOP} : 848.386 903 945 631 kg/m ³ ρ _{60_SET} : 848.406 913 426 009 kg/m ³ MMF _{SET} : 0.999 855 4 - | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, r% ≤ 0.02, for 3 Consecutive CPVs Crude Oil - Tables 5A/6A | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | Base Density | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| ρ _{obs} kg/m ³ | T _{dm} °F | P _{dm} psig | T _{FP_INLET} °F | T _{FP_OUTLET} °F | T _{MM} °F | T _{FD} °F | ρ _B kg/m ³ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | 73.070 | 73.200 | 73.390 | 75.120 | 848.407 | Run 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | 73.050 | 73.120 | 73.390 | 75.020 | 848.407 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | 73.080 | 73.140 | 73.400 | 75.140 | 848.407 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | 73.070 | 73.150 | 73.390 | 75.090 | 848.407 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Roundtrip Measurements | | | | | | | | T_{FP} and P_{FP} Values | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Ch 11.1 Iteration Results | N or N _i Pulses | Q _{MM} BPH | P _{FP_INLET} psig | P _{FP_OUTLET} psig | P _{MM} psig | T _{FP} °F | P _{FP} psig | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 411.407 | 882.125 | 176.1 | 173.8 | 185.4 | 73.135 0 | 174.95 | Run 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 411.413 | 882.131 | 176.7 | 174.0 | 185.9 | 73.085 0 | 175.35 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 411.408 | 882.129 | 176.2 | 174.0 | 186.4 | 73.110 0 | 175.10 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | 4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 411.409 3 | 882.128 | 176.3 | 173.9 | 185.9 | 73.110 0 | 175.10 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Example B.2 - Calibration Set III - 1 of 2

This document is not an API Standard; it is under consideration within an API technical committee but has not received all approvals required to become an API Standard. It shall not be reproduced or circulated or quoted, in whole or in part, outside of API committee activities except with the approval of the Chairman of the committee having jurisdiction and staff of the API Standards Dept. Copyright API. All rights reserved.

| Washington, D.C., USA | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|--|------------------------------|---|---------------------------|------------------------|----------------------------|--|---------------|----------|--------------------------------|--|---------------------------|-----------------------------|---------------------------|------------------------------|----------------------------|----------------------------|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|-------|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|----|-----------------|---------------|---------------|---------------|---------------|---------------|---------------|----|----|----|----|---|---|---|----------|----------|----|----|----|----|----|---|---|---|----------|--|--|--|--|--|--|---|-----------|---------------|---------------|---------------|---------------|---------------|---------------|-----|
| BPV Determination using Master Meter - Calibration Set III | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| API Chapter 12.4.2 USC_60 Measurement Units Sampling Method - Spot BPV - Standard Method Fixed Range Method, $r\% \leq 0.02$, for 3 Consecutive CPVs Crude Oil - Tables 5A/6A | | | <div style="display: flex; justify-content: space-between;"> <div> ΔMMF_{SET} Pass $(r) ICPV_{SET}$ Pass $(r) CPV_{SET}$ Pass </div> <div style="border-left: 1px solid black; padding-left: 5px;">-</div> </div> | | | | Report Summary <div style="display: flex; justify-content: space-between;"> <div> Prior Report No. Start Date Start 3 Time 00:00:00 Fluid, Batch No. 2342501.02 </div> <div> Current Stop Stop 3 00:00:00 2343601.02 </div> </div> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr style="background-color: #f4a460;"> <th>N or N_i Pulses</th> <th>NKF P / Bbl</th> <th>IV_{MM}</th> <th>CTL_{MM}</th> <th>CPL_{MM}</th> <th>CTPL_{MM}</th> <th>GSV_{MM} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>411.407</td><td>696.700 0</td><td>0.590 508 1</td><td>0.993 641 209</td><td>1.000 973 983</td><td>0.994 609 000</td><td>0.587 239 743</td><td>1</td></tr> <tr><td>411.413</td><td>696.700 0</td><td>0.590 516 7</td><td>0.993 641 209</td><td>1.000 976 613</td><td>0.994 611 612</td><td>0.587 249 838</td><td>2</td></tr> <tr><td>411.408</td><td>696.700 0</td><td>0.590 509 5</td><td>0.993 636 452</td><td>1.000 979 275</td><td>0.994 609 495</td><td>0.587 241 428</td><td>3</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>4</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>6</td></tr> <tr style="background-color: #f4a460;"> <td>411.409 3</td> <td>696.700 0</td> <td>0.590 511 4</td> <td>0.993 639 624</td> <td>1.000 976 624</td> <td>0.994 610 036</td> <td>0.587 243 670</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | | | N or N _i Pulses | NKF P / Bbl | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} Bbls | Run | 411.407 | 696.700 0 | 0.590 508 1 | 0.993 641 209 | 1.000 973 983 | 0.994 609 000 | 0.587 239 743 | 1 | 411.413 | 696.700 0 | 0.590 516 7 | 0.993 641 209 | 1.000 976 613 | 0.994 611 612 | 0.587 249 838 | 2 | 411.408 | 696.700 0 | 0.590 509 5 | 0.993 636 452 | 1.000 979 275 | 0.994 609 495 | 0.587 241 428 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | 411.409 3 | 696.700 0 | 0.590 511 4 | 0.993 639 624 | 1.000 976 624 | 0.994 610 036 | 0.587 243 670 | Avg |
| N or N _i Pulses | NKF P / Bbl | IV _{MM} | CTL _{MM} | CPL _{MM} | CTPL _{MM} | GSV _{MM} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.407 | 696.700 0 | 0.590 508 1 | 0.993 641 209 | 1.000 973 983 | 0.994 609 000 | 0.587 239 743 | 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.413 | 696.700 0 | 0.590 516 7 | 0.993 641 209 | 1.000 976 613 | 0.994 611 612 | 0.587 249 838 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 411.408 | 696.700 0 | 0.590 509 5 | 0.993 636 452 | 1.000 979 275 | 0.994 609 495 | 0.587 241 428 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| 411.409 3 | 696.700 0 | 0.590 511 4 | 0.993 639 624 | 1.000 976 624 | 0.994 610 036 | 0.587 243 670 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr style="background-color: #f4a460;"> <th>Iteration Results</th> <th>CTS_{FP}</th> <th>CPS_{FP}</th> <th>CTL_{FP}</th> <th>CPL_{FP}</th> <th>CTPL_{FP}</th> <th>CPV_{run} Bbls</th> <th>Run</th> </tr> </thead> <tbody> <tr><td>Crude Oil, JP-4</td><td>1.000 368 416</td><td>1.000 059 572</td><td>0.993 762 527</td><td>1.000 918 245</td><td>0.994 675 045</td><td>0.590 130 927</td><td>1</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 366 636</td><td>1.000 059 708</td><td>0.993 786 313</td><td>1.000 920 192</td><td>0.994 700 787</td><td>0.590 126 769</td><td>2</td></tr> <tr><td>Crude Oil, JP-4</td><td>1.000 368 149</td><td>1.000 059 623</td><td>0.993 774 420</td><td>1.000 918 956</td><td>0.994 687 655</td><td>0.590 125 266</td><td>3</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>4</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td></tr> <tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>6</td></tr> <tr style="background-color: #f4a460;"> <td></td> <td>1.000 367 734</td> <td>1.000 059 634</td> <td>0.993 774 420</td> <td>1.000 919 131</td> <td>0.994 687 829</td> <td>0.590 127 654</td> <td>Avg</td> </tr> </tbody> </table> | | | | | | | | | | Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} Bbls | Run | Crude Oil, JP-4 | 1.000 368 416 | 1.000 059 572 | 0.993 762 527 | 1.000 918 245 | 0.994 675 045 | 0.590 130 927 | 1 | Crude Oil, JP-4 | 1.000 366 636 | 1.000 059 708 | 0.993 786 313 | 1.000 920 192 | 0.994 700 787 | 0.590 126 769 | 2 | Crude Oil, JP-4 | 1.000 368 149 | 1.000 059 623 | 0.993 774 420 | 1.000 918 956 | 0.994 687 655 | 0.590 125 266 | 3 | | | | | | | | 4 | | | | | | | | 5 | | | | | | | | 6 | | 1.000 367 734 | 1.000 059 634 | 0.993 774 420 | 1.000 919 131 | 0.994 687 829 | 0.590 127 654 | Avg |
| Iteration Results | CTS _{FP} | CPS _{FP} | CTL _{FP} | CPL _{FP} | CTPL _{FP} | CPV _{run} Bbls | Run | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| Crude Oil, JP-4 | 1.000 366 636 | 1.000 059 708 | 0.993 786 313 | 1.000 920 192 | 0.994 700 787 | 0.590 126 769 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Crude Oil, JP-4 | 1.000 368 149 | 1.000 059 623 | 0.993 774 420 | 1.000 918 956 | 0.994 687 655 | 0.590 125 266 | 3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| | | | | | | | 6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | 1.000 367 734 | 1.000 059 634 | 0.993 774 420 | 1.000 919 131 | 0.994 687 829 | 0.590 127 654 | Avg | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse; text-align: center;"> <thead> <tr style="background-color: #f4a460;"> <th>1 means ΔCPV Passed</th> <th>ΔP_{B_SET} kg/m³</th> <th>ΔT_{P_SET} °F</th> <th>ΔP_{P_SET} psig</th> <th>ΔQ_{MM_SET} %</th> <th>r% ICPV_{run}</th> <th>CPV_{set}</th> <th>CPV_{set} Bbls</th> <th></th> </tr> </thead> <tbody> <tr> <td>Runs 1-3</td> <td>1</td> <td>0.000</td> <td>0.050</td> <td>0.40</td> <td>0.0</td> <td>0.001</td> <td>Pass</td> <td>0.590 127 654</td> <td>Runs 1-3</td> </tr> <tr> <td>Runs 2-4</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>-</td> <td>Runs 2-4</td> </tr> <tr> <td>Runs 3-5</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>-</td> <td>Runs 3-5</td> </tr> <tr> <td>Runs 4-6</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>NA</td> <td>-</td> <td>-</td> <td>-</td> <td>Runs 4-6</td> </tr> </tbody> </table> | | | | | | | | | | 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{MM_SET} % | r% ICPV _{run} | CPV _{set} | CPV _{set} Bbls | | Runs 1-3 | 1 | 0.000 | 0.050 | 0.40 | 0.0 | 0.001 | Pass | 0.590 127 654 | Runs 1-3 | Runs 2-4 | NA | NA | NA | NA | NA | - | - | - | Runs 2-4 | Runs 3-5 | NA | NA | NA | NA | NA | - | - | - | Runs 3-5 | Runs 4-6 | NA | NA | NA | NA | NA | - | - | - | Runs 4-6 | | | | | | | | | | | | | | | |
| 1 means ΔCPV Passed | ΔP_{B_SET} kg/m ³ | ΔT_{P_SET} °F | ΔP_{P_SET} psig | ΔQ_{MM_SET} % | r% ICPV _{run} | CPV _{set} | CPV _{set} Bbls | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 1-3 | 1 | 0.000 | 0.050 | 0.40 | 0.0 | 0.001 | Pass | 0.590 127 654 | Runs 1-3 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 2-4 | NA | NA | NA | NA | NA | - | - | - | Runs 2-4 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 3-5 | NA | NA | NA | NA | NA | - | - | - | Runs 3-5 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Runs 4-6 | NA | NA | NA | NA | NA | - | - | - | Runs 4-6 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr style="background-color: #f4a460;"> <th style="width: 40%;">Signature</th> <th style="width: 20%;">Date</th> <th style="width: 40%;">Company</th> </tr> </thead> <tbody> <tr> <td></td> <td></td> <td>API Midstream Representative</td> </tr> <tr><td> </td><td></td><td></td></tr> <tr><td> </td><td></td><td></td></tr> <tr><td> </td><td></td><td></td></tr> </tbody> </table> | | | | | | | | | | Signature | Date | Company | | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Signature | Date | Company | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | API Midstream Representative | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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Example B.2 - Calibration Set III - 2 of 2

Annex C
(informative)
Equations for the Master Meter Volumetric Method

Figure C.1 - Standard Method Using Continuous Sampling

Figure C.2 - Standard Method Equations Using Spot Sampling

Figure C.3 - Alternate Method 'A' Using Continuous Sampling

Figure C.4 - Alternate Method 'A' Using Spot Sampling

Figure C.5 - Alternate Method 'B' Using Continuous Sampling

Figure C.6 - Alternate Method 'B' Using Spot Sampling

DRAFT

| Density Correlations using API MPMS Chapter 11.1 | | |
|--|--|--|
| The density correlations in accordance with API MPMS Chapter 11.1 for atmospherically stable fluids (P _{E,at,Tfluid} = 0.0 psig, 0.0 kPag): | | |
| CTPL = CTL x CPL = ρ _{TP} / ρ _B | | |
| ρ _{TP} = CTPL x ρ _B = CTL x CPL x ρ _B | | |
| And, | | |
| CTL ~ f (ρ _B , T _{Fluid}) | | |
| CPL ~ f (ρ _B , T _{Fluid} , P _{Fluid} , F _{Fluid}) | | |
| F _{Fluid} ~ f (ρ _B , T _{Fluid}) | | |
| For Continuous Sampling, | | |
| ρ _B and ρ _{B_RUN} ~ (ρ _{obs} , T _{dm} , P _{dm}) | | |
| And, | | |
| ρ _{B_SET} = Σ ³ (ρ _{B_RUN}) / 3 | | |
| ICPV Equations | | |
| Master Meter | CTL _{MM} ~ f (ρ _{B_START} , T _{MM}) | |
| | F _{MM} ~ f (ρ _{B_START} , T _{MM}) | |
| | CPL _{MM} = 1 / [1 - (P _{MM} x F _{MM})] | |
| | GSV _{MM} = [(Σ N) / NKf x CTL _{MM} x CPL _{MM}] x MMF _{START} | |
| Field Displacement Prover | CTS _{FP} | |
| | CTS _{FP} = { 1 + [(T _{FP} - T _B) x GL _{FP}] } ³ | |
| | CTS _{FP} = { 1 + [(T _{FP} - T _B) x GL _{FP}] } ² x { 1 + [(T _{fd} - T _B) x GL _{fd}] } | |
| | CPS _{FP} = { 1 + [(P _{FP} x ID _{FP}) / (E _{FP} x WT _{FP})] } | |
| | CTL _{FP} ~ f (ρ _{B_START} , T _{FP}) | |
| | F _{FP} ~ f (ρ _{B_START} , T _{FP}) | |
| | CPL _{FP} = 1 / [1 - (P _{FP} x F _{FP})] | |
| | ICPV _{RUN} = GSV _{MM} / (CTS _{FP} x CPS _{FP} x CTL _{FP} x CPL _{FP}) | |
| Field Open Tank Prover | CTS _{FP} = { 1 + [(T _{FP} - T _B) x GL _{FP}] } ³ | |
| | CPS _{FP} = 1.000 000 | |
| | CPS _{MP} = { 1 + [(P _{MP} x ID _{MP}) / (E _{MP} x WT _{MP})] } | |
| | CTL _{FP} ~ f (ρ _{B_START} , T _{FP}) | |
| | CPL _{FP} = 1.000 000 | |
| | ICPV _{RUN} = GSV _{MM} / (CTS _{FP} x CPS _{FP} x CTL _{FP} x CPL _{FP}) | |
| CPV Equations | | |
| Master Meter | CTL _{MM} ~ f (ρ _{B_RUN} , T _{MM}) | |
| | F _{MM} ~ f (ρ _{B_RUN} , T _{MM}) | |
| | CPL _{MM} = 1 / [1 - (P _{MM} x F _{MM})] | |
| | MMF _{SET} = [MMF _{START} + MMF _{STOP}] / 2 | |
| GSV _{MM_RUN} = [(Σ N) / NKf x CTL _{MM} x CPL _{MM}] x MMF _{SET} | | |
| Field Displacement Prover | CTS _{FP} | |
| | CTS _{FP} = { 1 + [(T _{FP} - T _B) x GL _{FP}] } ³ | |
| | CTS _{FP} = { 1 + [(T _{FP} - T _B) x GL _{FP}] } ² x { 1 + [(T _{fd} - T _B) x GL _{fd}] } | |
| | CPS _{FP} = { 1 + [(P _{FP} x ID _{FP}) / (E _{FP} x WT _{FP})] } | |
| | CTL _{FP} ~ f (ρ _{B_RUN} , T _{FP}) | |
| | F _{FP} ~ f (ρ _{B_RUN} , T _{FP}) | |
| | CPL _{FP} = 1 / [1 - (P _{FP} x F _{FP})] | |
| | CPV _{RUN} = GSV _{MM_RUN} / (CTS _{FP} x CPS _{FP} x CTL _{FP} x CPL _{FP}) | |
| CPV _{SET} = (Σ ³ CPV _{RUN}) / 3 | | |
| Field Open Tank Prover | CTS _{FP} = { 1 + [(T _{FP} - T _B) x GL _{FP}] } ³ | |
| | CPS _{FP} = 1.000 000 | |
| | CPS _{MP} = { 1 + [(P _{MP} x ID _{MP}) / (E _{MP} x WT _{MP})] } | |
| | CTL _{FP} ~ f (ρ _{B_RUN} , T _{FP}) | |
| | CPL _{FP} = 1.000 000 | |
| | CPV _{RUN} = GSV _{MM_RUN} / (CTS _{FP} x CPS _{FP} x CTL _{FP} x CPL _{FP}) | |
| CPV _{SET} = (Σ ³ CPV _{RUN}) / 3 | | |

Figure C.1 - Standard Method Using Continuous Sampling

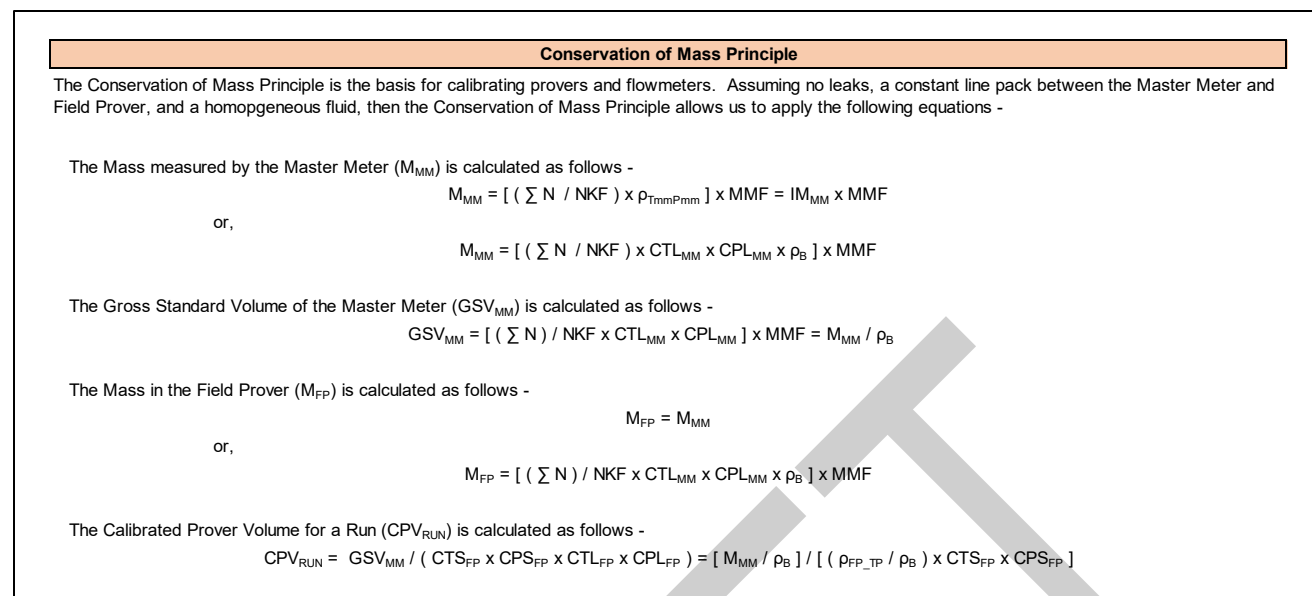


Figure C.1 - Standard Method Using Continuous Sampling (continued)

| Density Correlations using API MPM Chapter 11.1 | | |
|--|--|---|
| The density correlations in accordance with API MPMS Chapter 11.1 for atmospherically stable fluids ($P_{E_at_Tfluid} = 0.0$ psig, 0.0 kPag): | | |
| $CTPL = CTL \times CPL = \rho_{TP} / \rho_B$ | | |
| $\rho_{TP} = CTPL \times \rho_B = CTL \times CPL \times \rho_B$ | | |
| And, | $CTL \sim f(\rho_B, T_{Fluid})$ $CPL \sim f(\rho_B, T_{Fluid}, P_{Fluid}, F_{Fluid})$ $F_{Fluid} \sim f(\rho_B, T_{Fluid})$ | |
| And, | $\rho_{B_SET} = (\rho_{B_START} + \rho_{B_STOP}) / 2$ | |
| For Spot Sampling, | | |
| ρ_B and $\rho_{B_RUN} \sim (\rho_{obs}, T_{obs}, P_{obs})$ | | |
| ICPV Equations | | |
| Master Meter | $CTL_{MM} \sim f(\rho_{B_START}, T_{MM})$ $F_{MM} \sim f(\rho_{B_START}, T_{MM})$ $CPL_{MM} = 1 / [1 - (P_{MM} \times F_{MM})]$ $GSV_{MM} = [(\sum N) / NKF \times CTL_{MM} \times CPL_{MM}] \times MMF_{START}$ | |
| Field Displacement Prover | CTS_{FP} $CTS_{FP} = \{1 + [(T_{FP} - T_B) \times GL_{FP}]\}^3$ $CTS_{FP} = \{1 + [(T_{FP} - T_B) \times GL_{FP}]\}^2 \times \{1 + [(T_{Id} - T_B) \times GL_{Id}]\}$ $CPS_{FP} = \{1 + [(P_{FP} \times ID_{FP}) / (E_{FP} \times WT_{FP})]\}$ $CTL_{FP} \sim f(\rho_{B_START}, T_{FP})$ $F_{FP} \sim f(\rho_{B_START}, T_{FP})$ $CPL_{FP} = 1 / [1 - (P_{FP} \times F_{FP})]$ $ICPV_{RUN} = GSV_{MM} / (CTS_{FP} \times CPS_{FP} \times CTL_{FP} \times CPL_{FP})$ | free displacer design captive displacer design single wall design |
| Field Open Tank Prover | $CTS_{FP} = \{1 + [(T_{FP} - T_B) \times GL_{FP}]\}^3$ $CPS_{FP} = 1.000\ 000$ $CPS_{MP} = \{1 + [(P_{MP} \times ID_{MP}) / (E_{MP} \times WT_{MP})]\}$ $CTL_{FP} \sim f(\rho_{B_START}, T_{FP})$ $CPL_{FP} = 1.000\ 000$ $ICPV_{RUN} = GSV_{MM} / (CTS_{FP} \times CPS_{FP} \times CTL_{FP} \times CPL_{FP})$ | |
| CPV Equations | | |
| Master Meter | $CTL_{MM} \sim f(\rho_{B_SET}, T_{MM})$ $F_{MM} \sim f(\rho_{B_SET}, T_{MM})$ $CPL_{MM} = 1 / [1 - (P_{MM} \times F_{MM})]$ $MMF_{SET} = [MMF_{START} + MMF_{STOP}] / 2$ $GSV_{MM_RUN} = [(\sum N) / NKF \times CTL_{MM} \times CPL_{MM}] \times MMF_{SET}$ | |
| Field Displacement Prover | CTS_{FP} $CTS_{FP} = \{1 + [(T_{FP} - T_B) \times GL_{FP}]\}^3$ $CTS_{FP} = \{1 + [(T_{FP} - T_B) \times GL_{FP}]\}^2 \times \{1 + [(T_{Id} - T_B) \times GL_{Id}]\}$ $CPS_{FP} = \{1 + [(P_{FP} \times ID_{FP}) / (E_{FP} \times WT_{FP})]\}$ $CTL_{FP} \sim f(\rho_{B_SET}, T_{FP})$ $F_{FP} \sim f(\rho_{B_SET}, T_{FP})$ $CPL_{FP} = 1 / [1 - (P_{FP} \times F_{FP})]$ $CPV_{RUN} = GSV_{MM_RUN} / (CTS_{FP} \times CPS_{FP} \times CTL_{FP} \times CPL_{FP})$ $CPV_{SET} = (\sum^3 CPV_{RUN}) / 3$ | free displacer design captive displacer design single wall design |
| Field Open Tank Prover | $CTS_{FP} = \{1 + [(T_{FP} - T_B) \times GL_{FP}]\}^3$ $CPS_{FP} = 1.000\ 000$ $CPS_{MP} = \{1 + [(P_{MP} \times ID_{MP}) / (E_{MP} \times WT_{MP})]\}$ $CTL_{FP} \sim f(\rho_{B_SET}, T_{FP})$ $CPL_{FP} = 1.000\ 000$ $CPV_{RUN} = GSV_{MM_RUN} / (CTS_{FP} \times CPS_{FP} \times CTL_{FP} \times CPL_{FP})$ $CPV_{SET} = (\sum^3 CPV_{RUN}) / 3$ | |

Figure C.2 - Standard Method Equations Using Spot Sampling

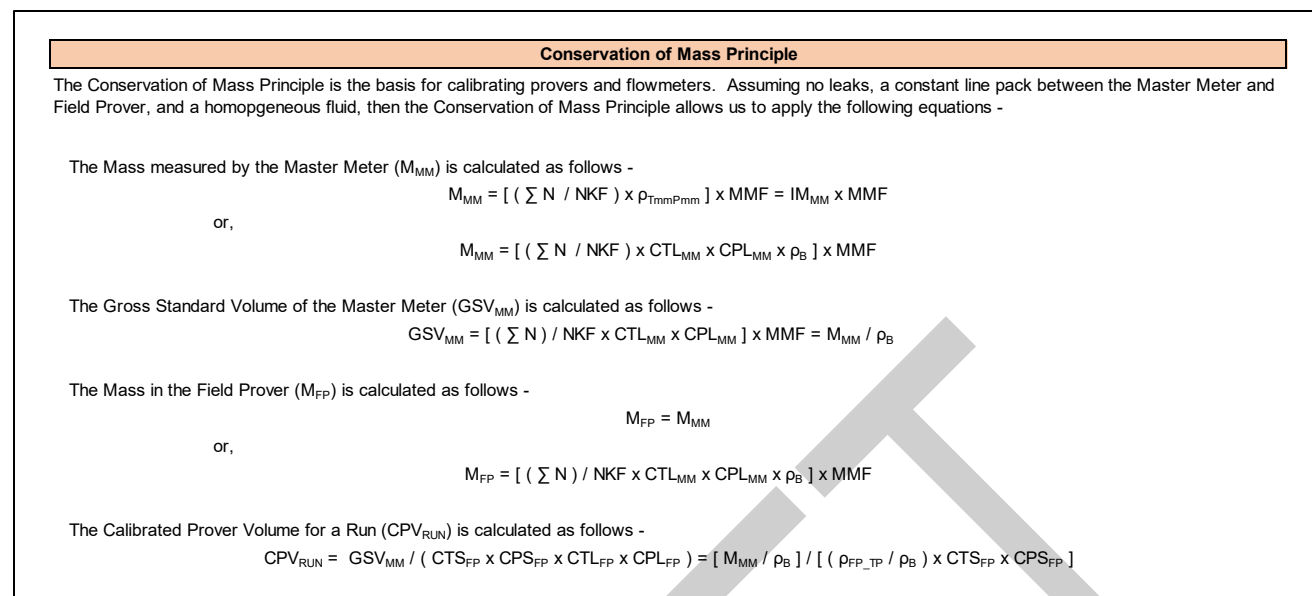


Figure C.2 - Standard Method Equations Using Spot Sampling (continued)

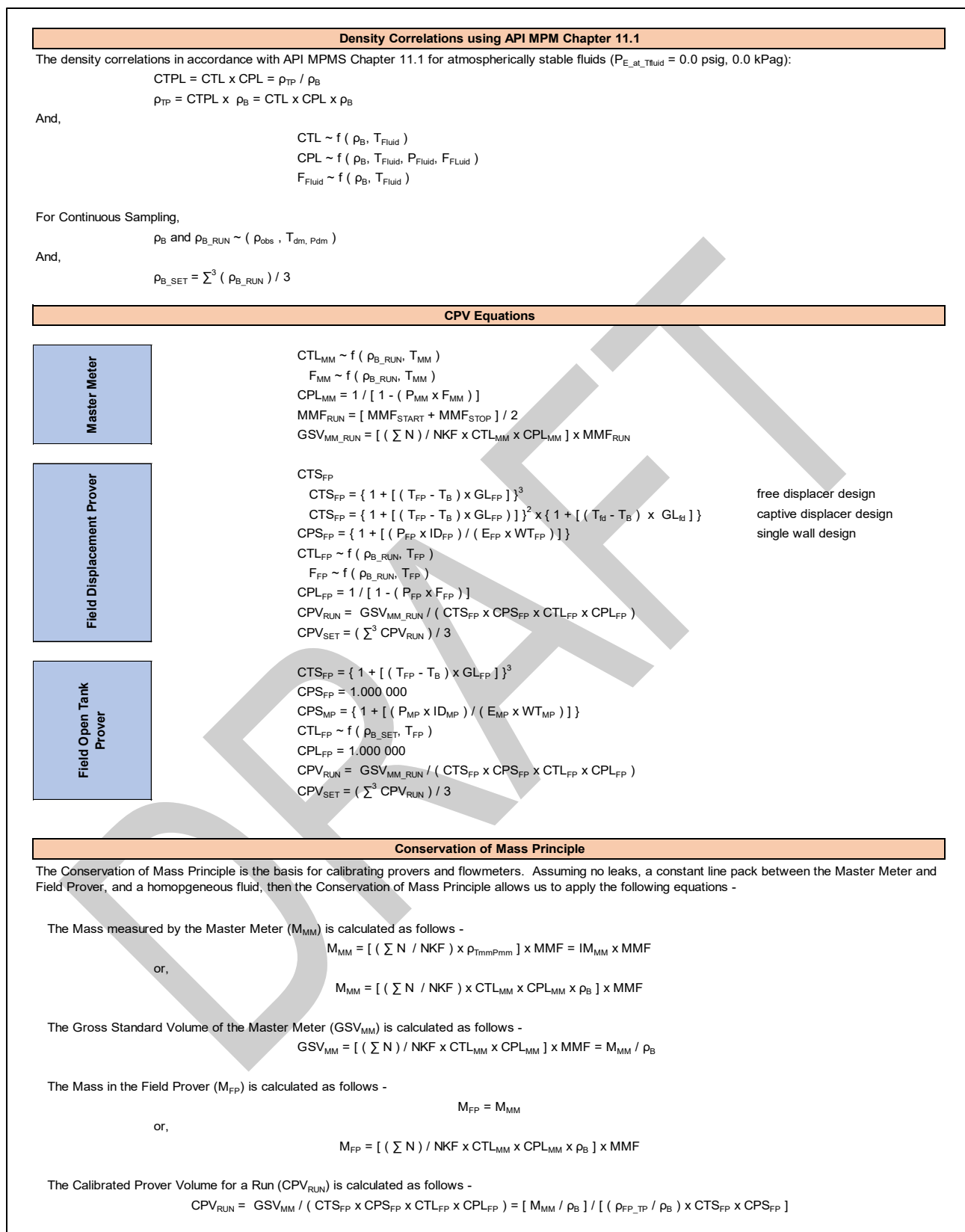


Figure C.3 - Alternate Method 'A' Using Continuous Sampling

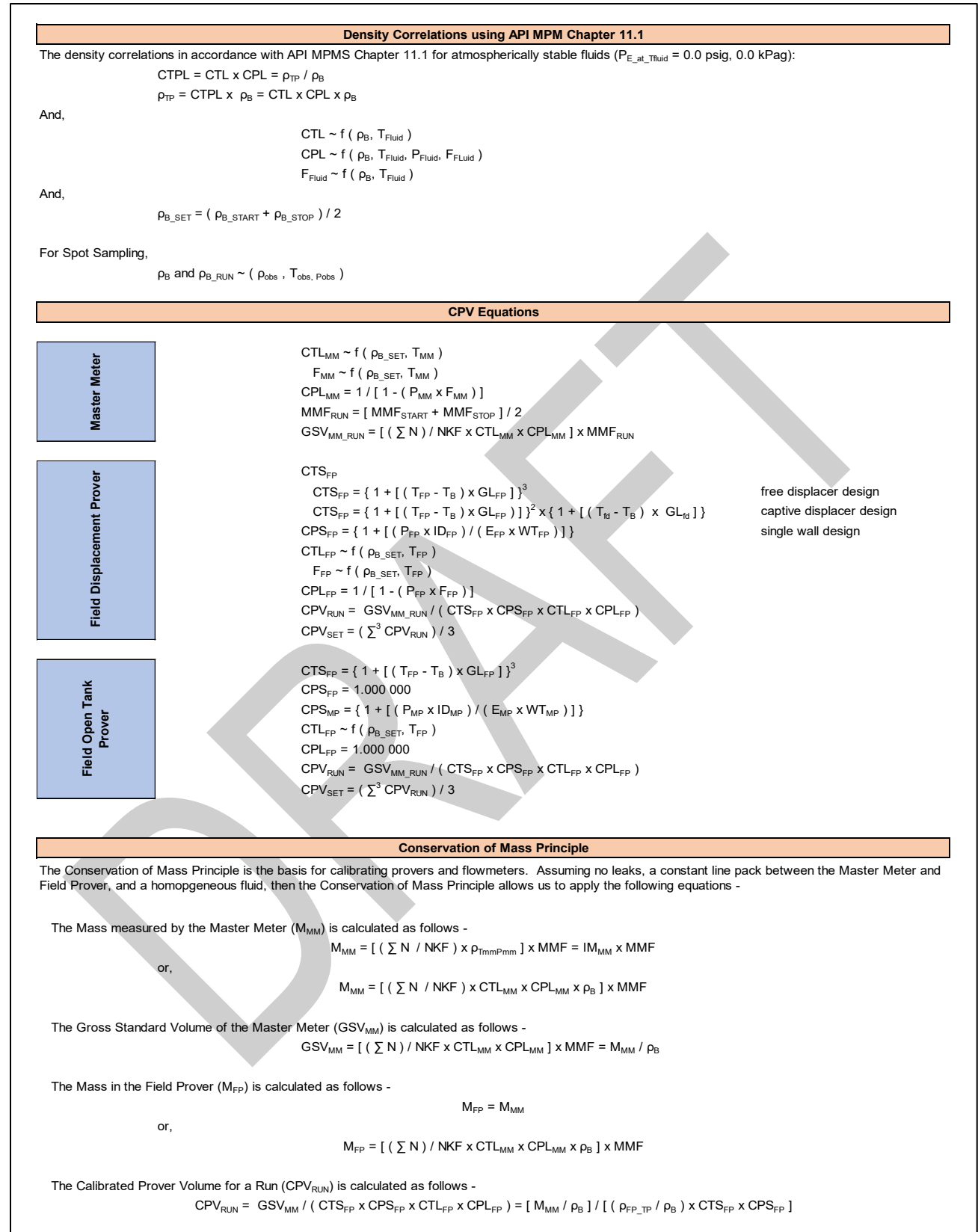


Figure C.4 - Alternate Method 'A' Using Spot Sampling

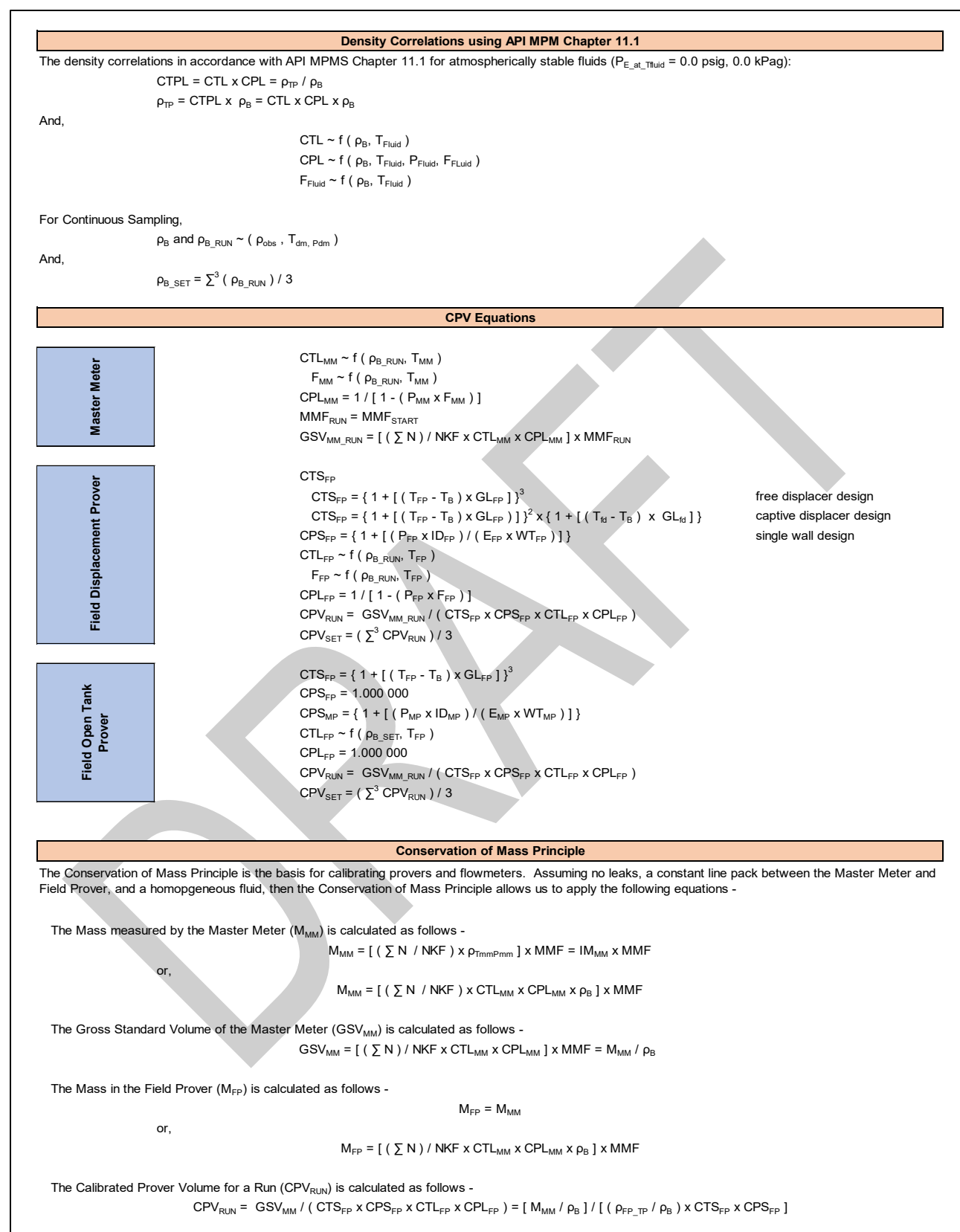


Figure C.5 - Alternate Method 'B' Using Continuous Sampling

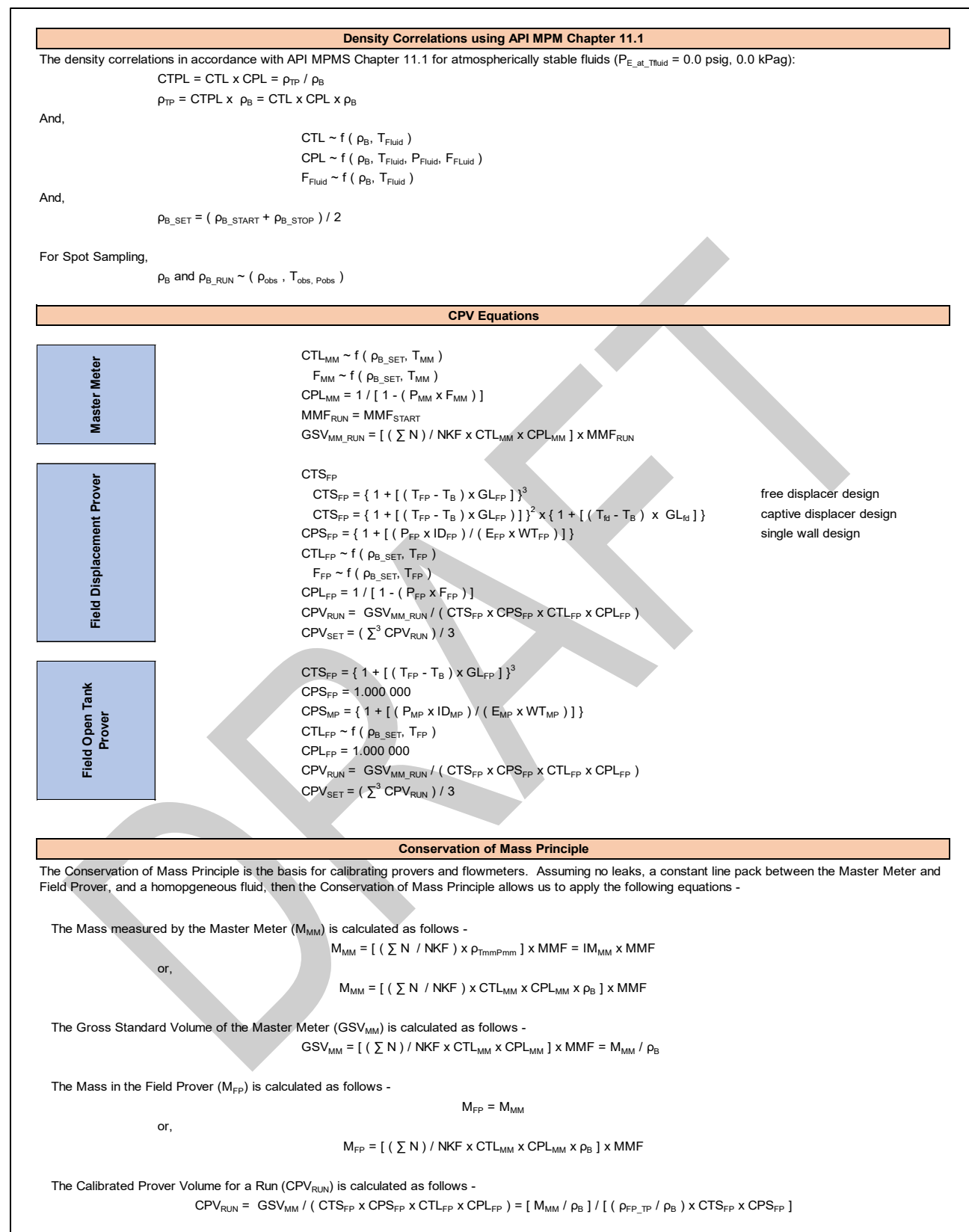


Figure C.6 - Alternate Method 'B' Using Spot Sampling

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